Eidgenössische Technische Hochschule Zürich
Swiss Federal Institute of Technology Zurich

Conceptualization and Multi-Objective Optimization of the Electric System of an Airborne Wind Turbine

J. W. Kolar et al.

Swiss Federal Institute of Technology (ETH) Zurich
Power Electronic Systems Laboratory
www.pes.ee.ethz.ch

Eidgenössische Technische Hochschule Zürich
Swiss Federal Institute of Technology Zurich

Pareto-Optimal Design of Airborne Wind Turbine Power Electronics

J. W. Kolar, T. Friedli, F. Krismer, A. Looser, M. Schweizer, P. Steimer, J. Bevirt

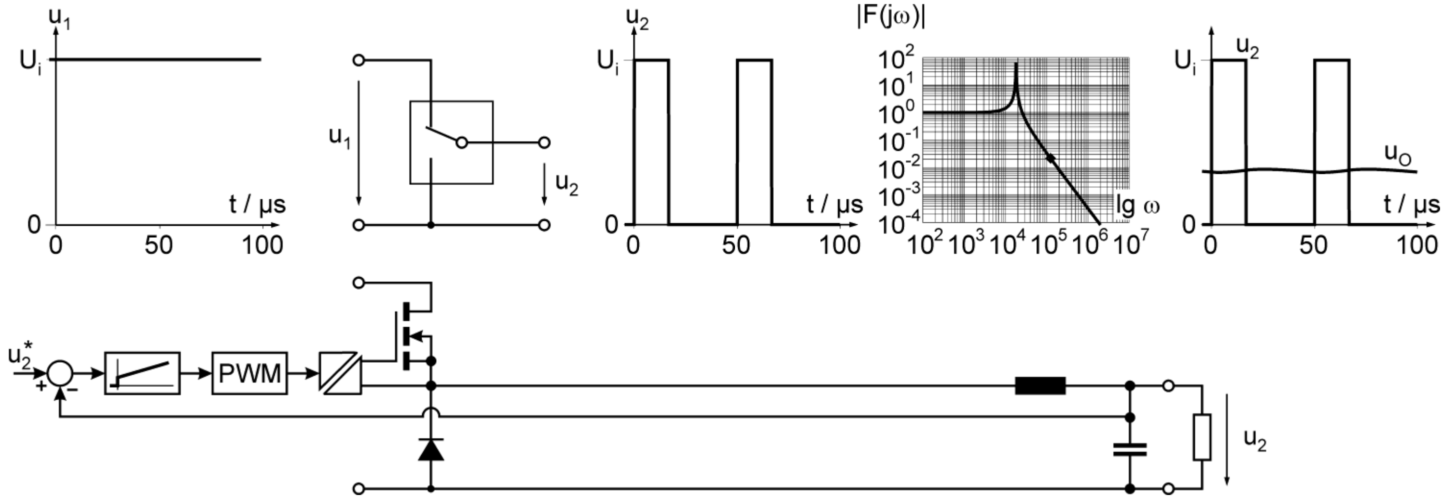
Power and productivity for a better world™ ABB   JOBY ENERGY

Swiss Federal Institute of Technology (ETH) Zurich
Power Electronic Systems Laboratory
www.pes.ee.ethz.ch

Basics

Electronic Power Processing
Power Electronics Performance Trends
Design Process
Multi-Objective Optimization

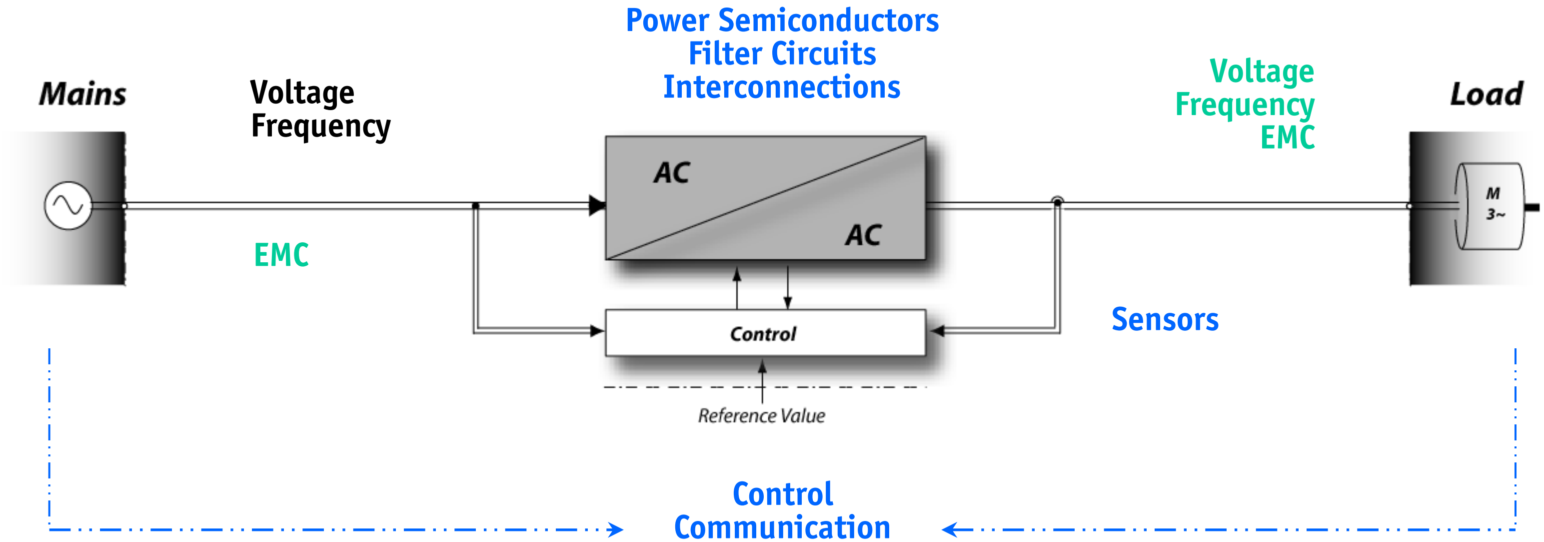
Basic Electronic Power Processing System



- Electronic Switches / Power Semiconductors
- Filter Circuits / Inductors, Capacitors
- Heat Management / Heatsink
- Sensor Circuits
- Digital Signal Processing

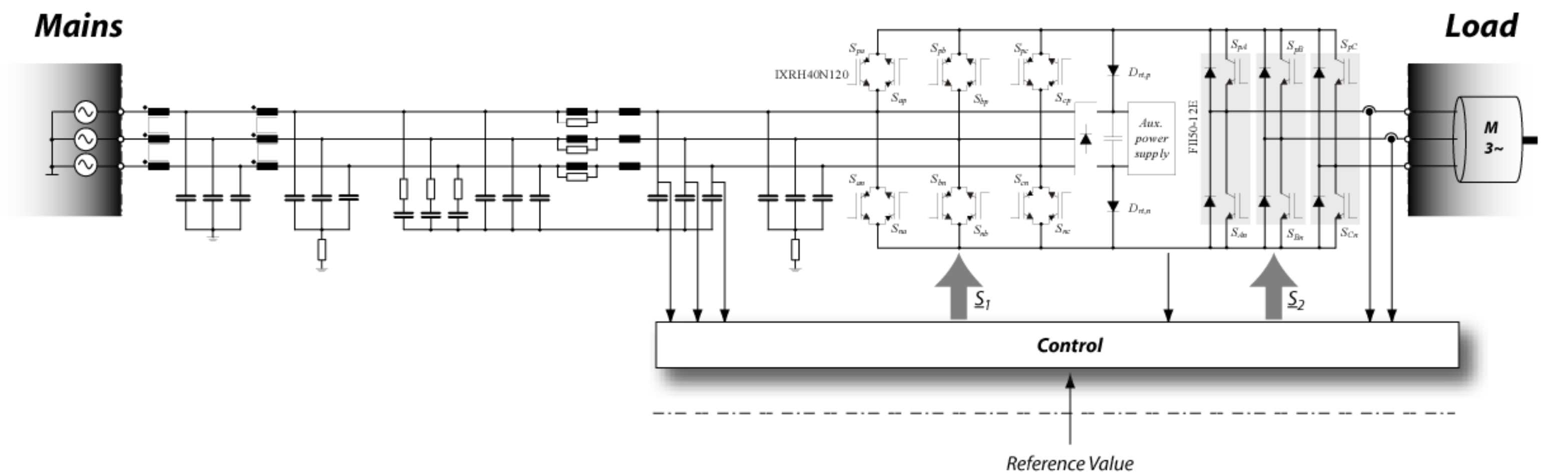
Basic Electronic Power Processing System

- Highest Efficiency
- Highest Dynamics
- Highest Compactness
- Highest Compatibility
- Highest Reliability



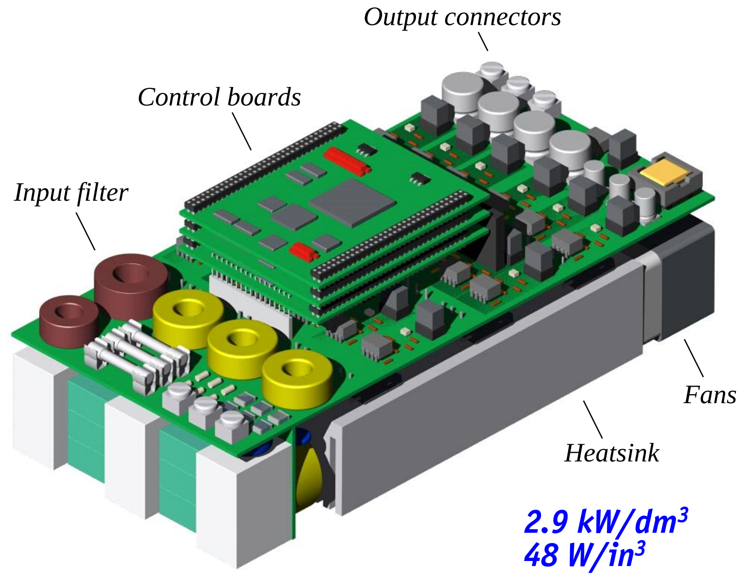
Basic Electronic Power Processing System

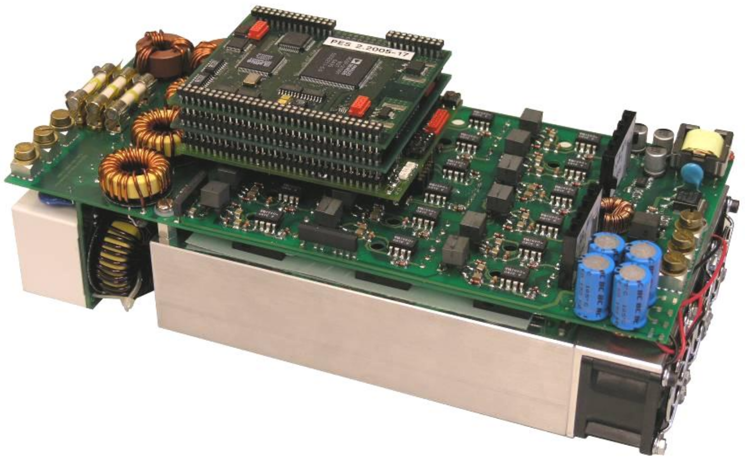
- Highest Efficiency
- Highest Dynamics
- Highest Compactness
- Highest Compatibility
- Highest Reliability



▶ Example of a Three-Phase AC/AC Matrix Converter

Three-Phase AC/AC Matrix Converter Prototype





2.9 kW/dm³
48 W/in³

Efficiency 95.5%

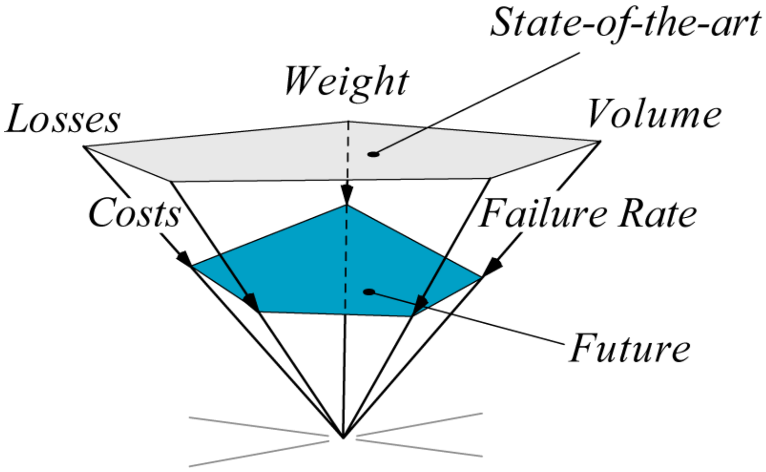
Input RMS voltage	*400V*
Output Power	*6.8 kVA*
Rectifier Switching Frequency	*12.5 kHz*
Inverter Switching Frequency	*25 kHz*

Power Electronics Performance Trends

- **Performance Indices**

— Power Density [kW/dm³]
— Power per Unit Weight [kW/kg]
— Relative Costs [kW/$]
— Relative Losses [%]
— Failure Rate [h^{-1}]

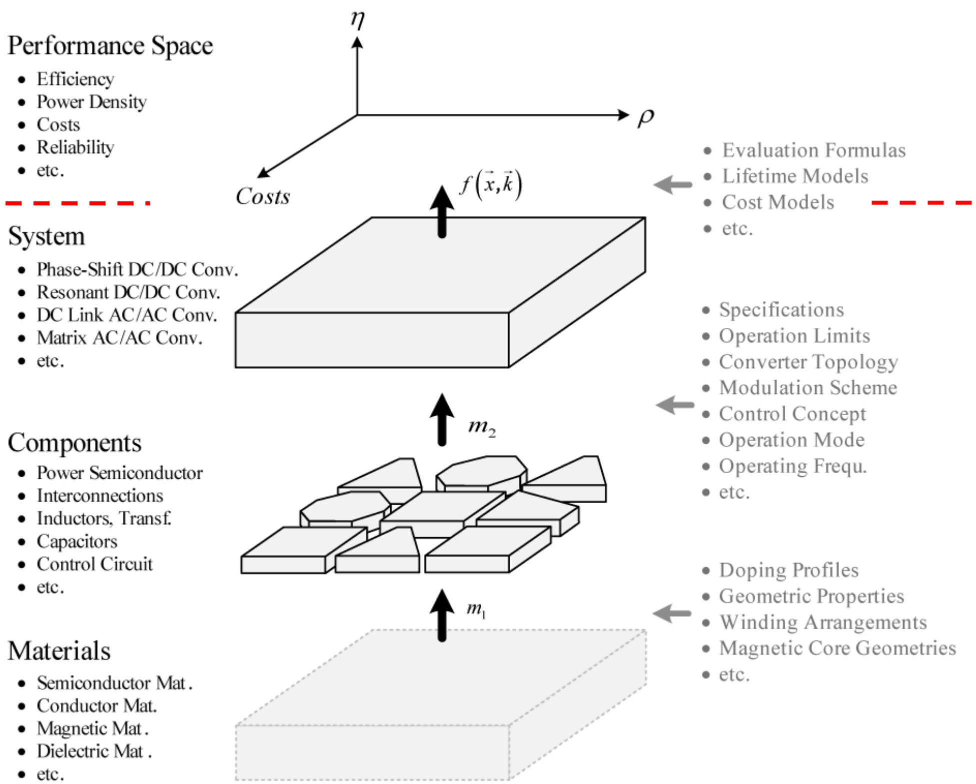
▶ Understand the Mutual Coupling of Performance Indices



Abstraction of Power Converter Design Process

Performance Space

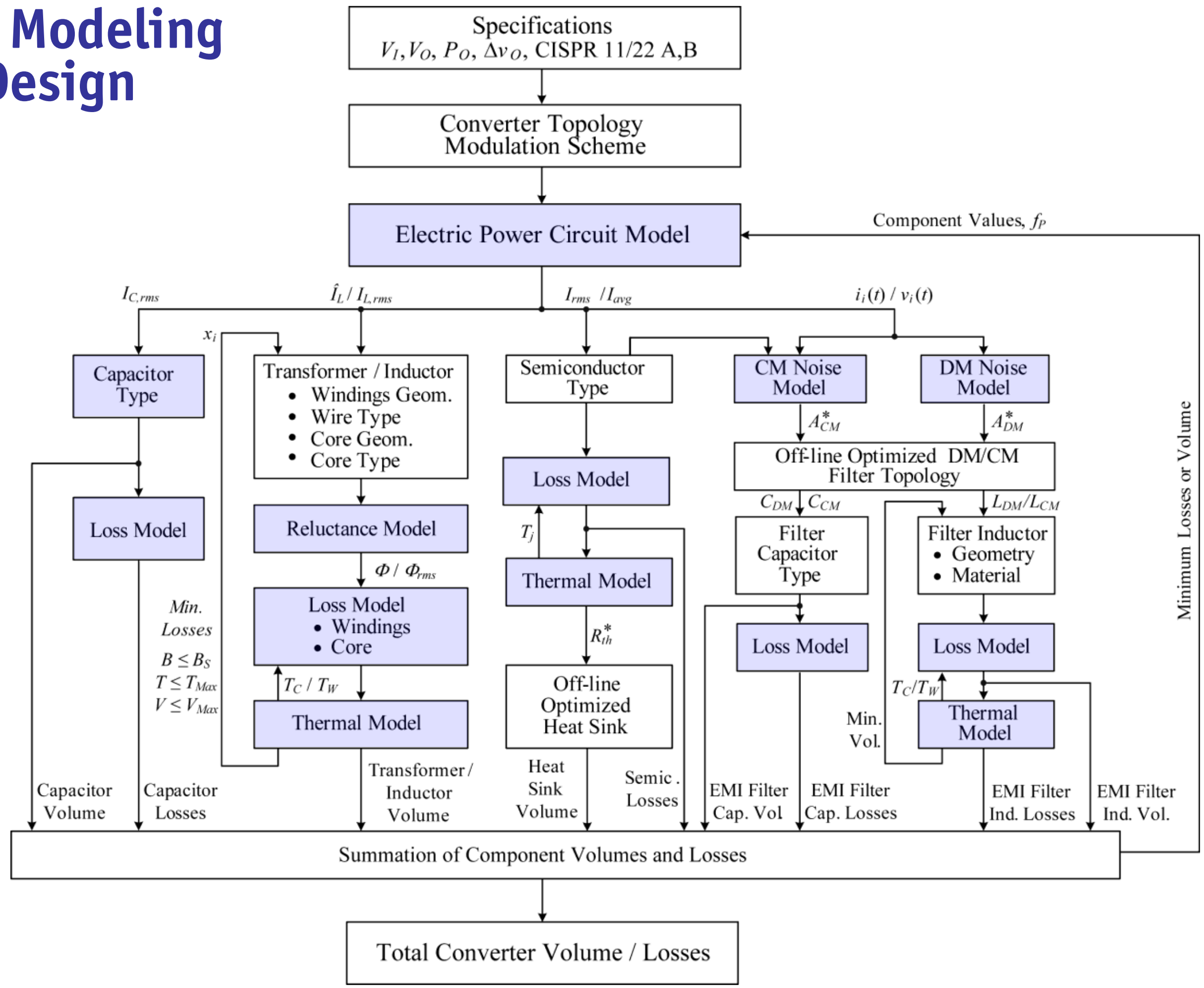
Design Space



▶ *Mapping of Design Space into System Performance Space*

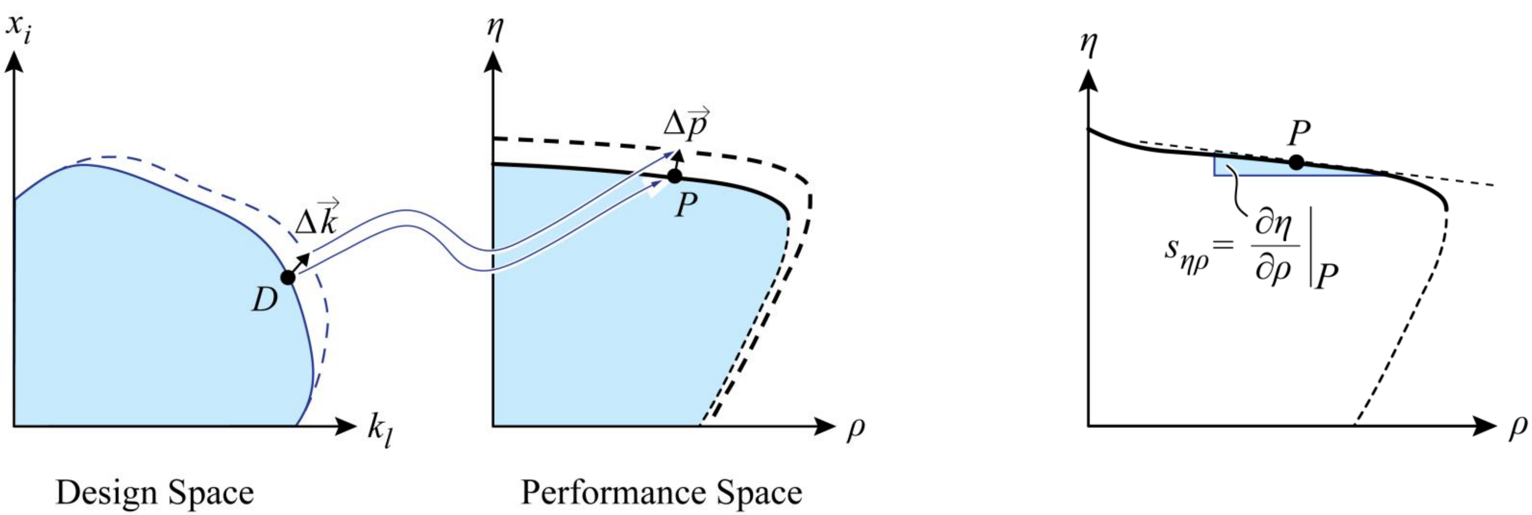
Mathematical Modeling of Converter Design

- **Multi-Objective Optimization**



Multi-Objective Design Optimization/ PARETO-Front

- ► Sensitivity to Technology Advancements
- ► Trade-off Analysis



Example → Efficiency / Volume Trade-off of Inductors

Operating Conditions and Parameters

$$L, f_P, I \qquad \Phi \propto L\, I$$

- **Scaling of Core Losses**

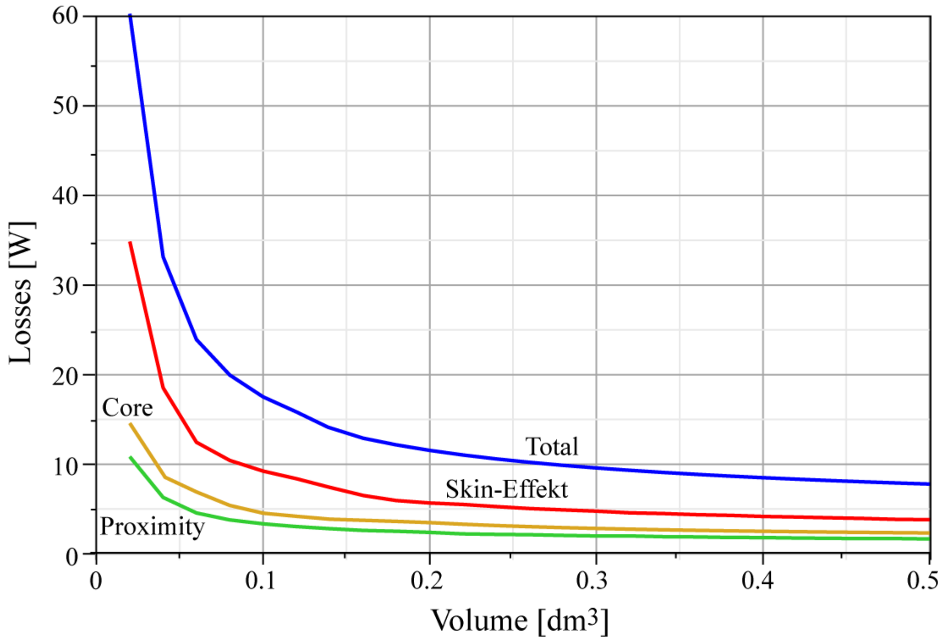
$$P_{Core} \propto f_P \left(\frac{\Phi}{A}\right)^2 V$$

$$P_{Core} \propto \left(\frac{1}{l^2}\right)^2 l^3 \propto \frac{1}{l}$$

- **Scaling of Winding Losses**

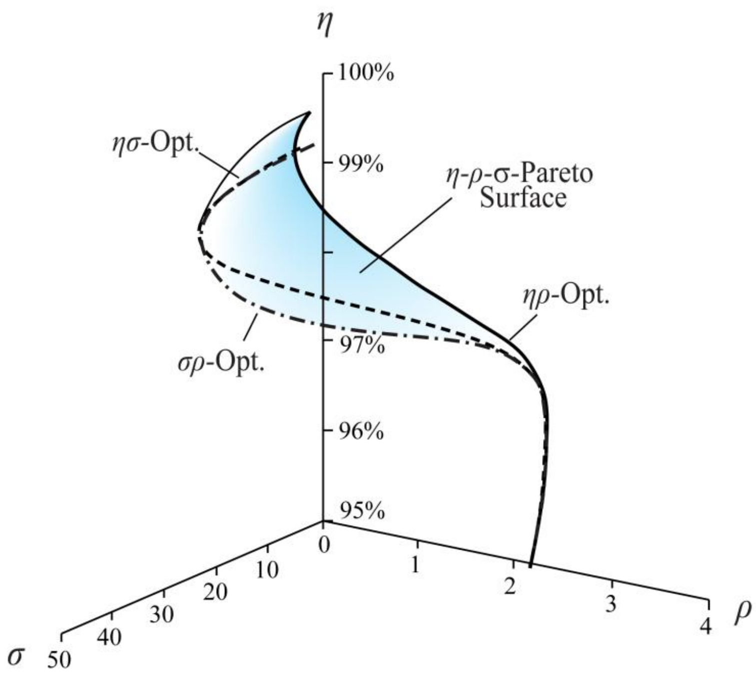
$$P_{Wdg} \propto I^2 R \propto I^2 \frac{l_{Wdg}}{\kappa A_{Wdg}}$$

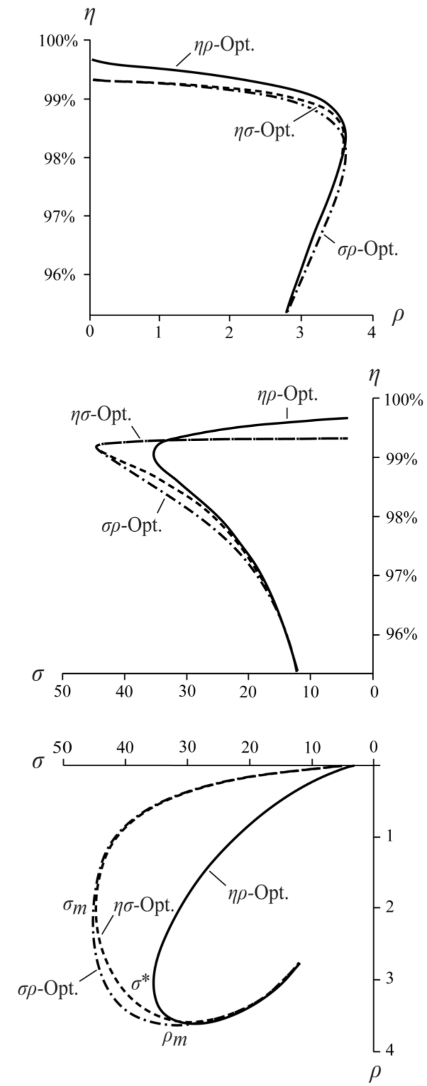
$$P_{Wdg} \propto \frac{1}{l}$$



Converter Performance Evaluation Based on η-ρ-σ-PARETO Surface

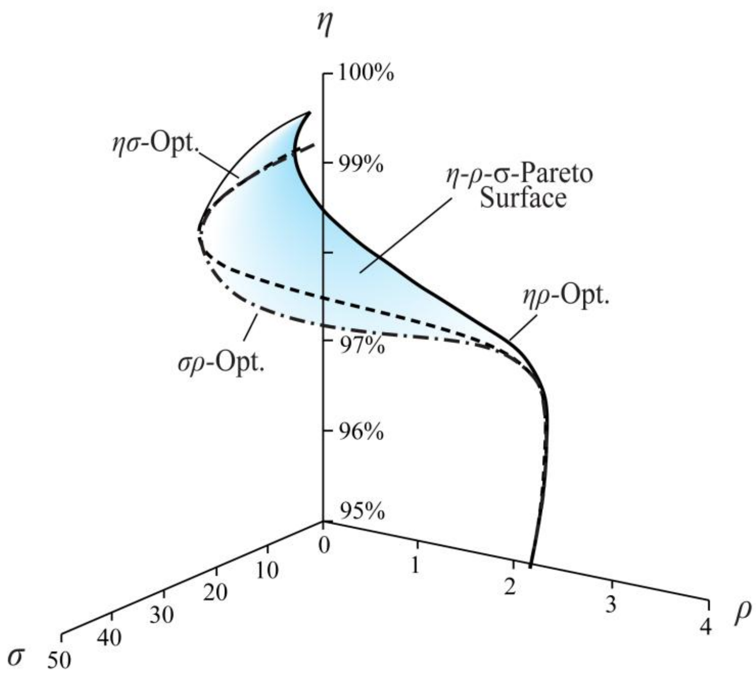
- σ: kW/$

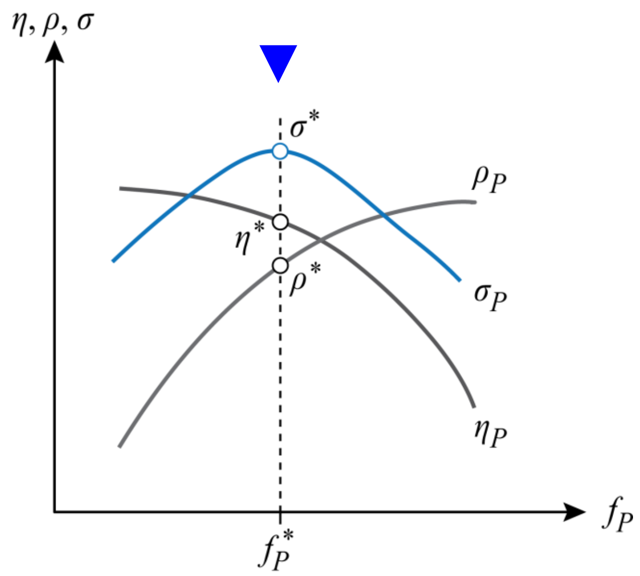




Converter Performance Evaluation Based on η-ρ-σ-PARETO Surface

► *´ Technology Node´*



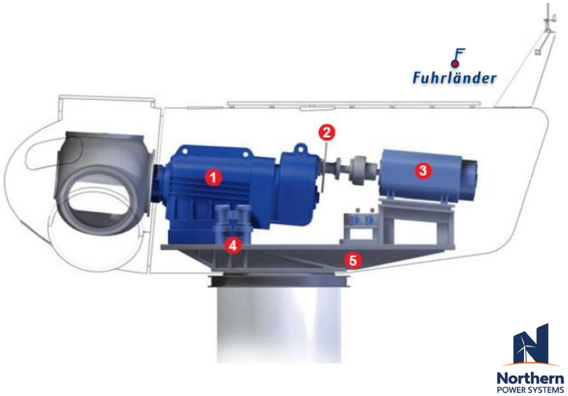


Technology Node: $(\sigma^*, \eta^*, \rho^*, f_P^*)$

"Out-of-the-Box"
Wind Turbine Concepts

Power Kite & *Ground-Based* EE-Generation
Power Kite & *On-Board* EE-Generation

Conventional 100kW Wind Turbine



▶ Characteristics

- Tower 35m/18 tons
- Rotor 21m / 2.3tons
- Nacelle 4.4 tons

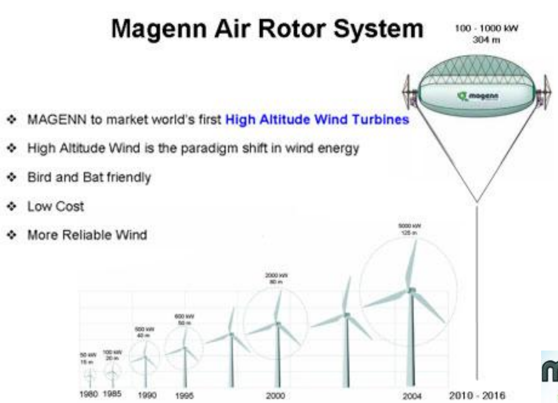
▼

$$v_{\mathrm{W}}(h) = v_{\mathrm{W}}^{*} \left(\frac{h}{h^{*}} \right)^{\alpha_{\mathrm{H}}}$$

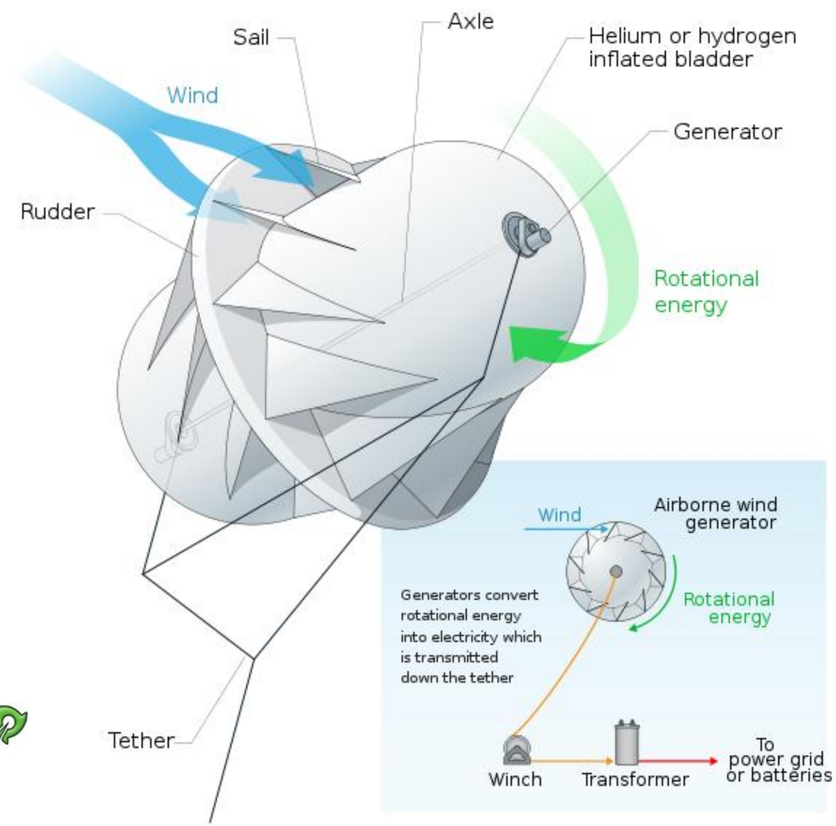
- Large Fraction of Mechanically Supporting Parts / High Costs

Air Rotor Wind Generator

- Helium or Hydrogen Inflated
- Magnus Effect - Additional Lift



magenn
wind power anywhere



Revolutionize Wind Power Generation Using Kites / Tethered Airfoils

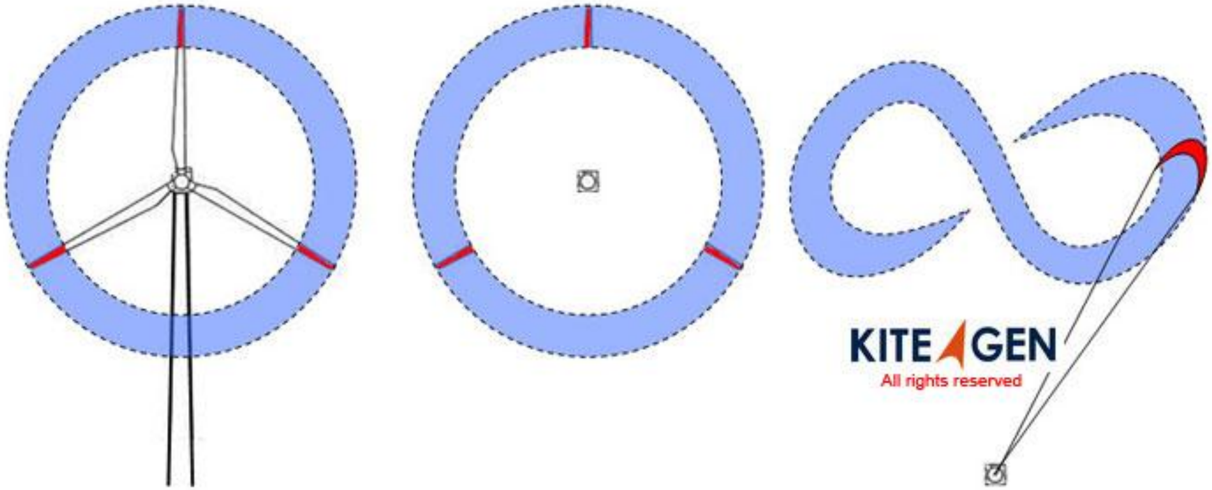
[2] M. Loyd, 1980

- Wing Tips / Highest Speed Regions are the Main Power Generating Parts of a Wind Turbine

Controlled Power Kites for Capturing Wind Power

- ► Replace Blades by Power Kites
- ► Minimum Base Foundation etc. Required
- ► Operative Height Adjustable to Wind Conditions

M. Loyd, 1980

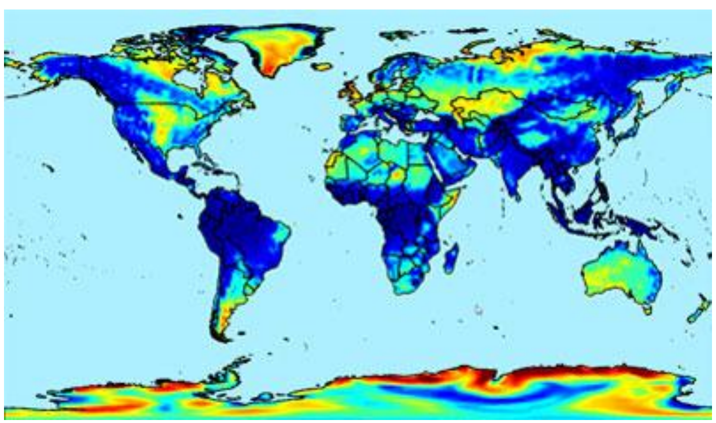


- ■ Wing Tips / Highest Speed Regions are the Main Power Generating Parts of a Wind Turbine

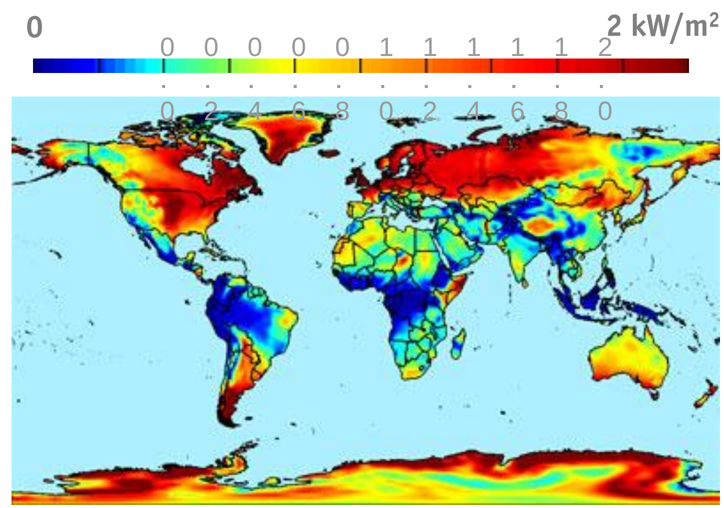
Controlled Power Kites for Capturing Wind Power

- Wind at High Altitudes is Faster and More Consistent
- Operate Kites at High Altitudes or Even in the Jet Stream

Source: JOBY ENERGY



120m



700m

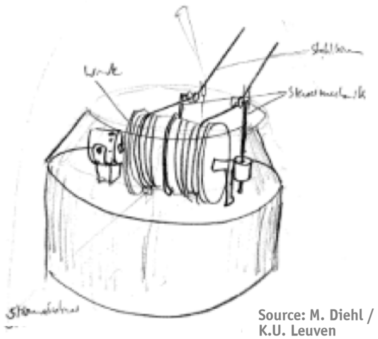
Controlled Power Kites for Capturing Wind Power

- Wind at High Altitudes is Faster and More Consistent
- Operate Kites at High Altitudes or Even in the Jet Stream

STANFORD UNIVERSITY

AIRBORNE 2010 WIND ENERGY CONFERENCE

Pumping Power Kites



Source: M. Diehl / K.U. Leuven

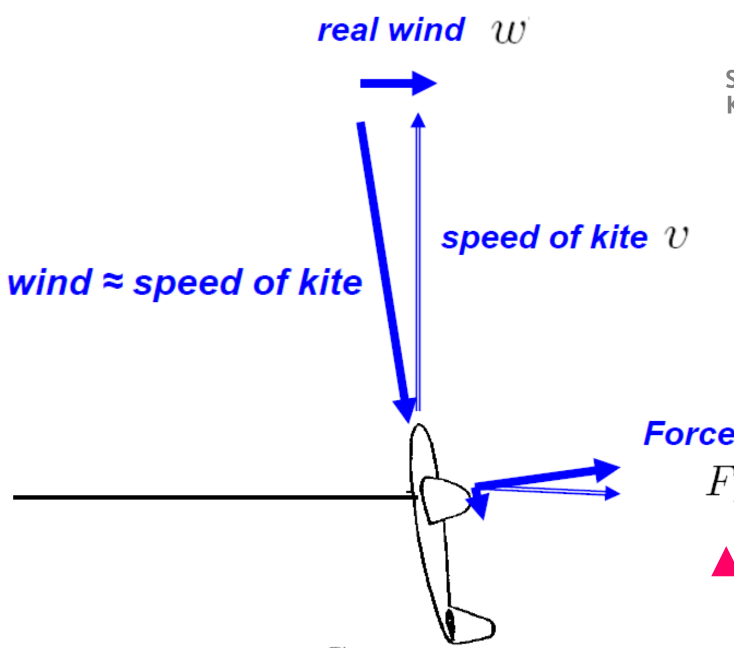
Ground-Based EE-Generation

Basics of Power Kites

- Kite´s Aerodynamic Surface Converts Wind Energy into Kite Motion

Source: M. Diehl / K.U. Leuven

- *effective wind ≈ speed of kite*



$$F_L = \frac{1}{2}\rho A C_{\mathrm{L}} v^2$$

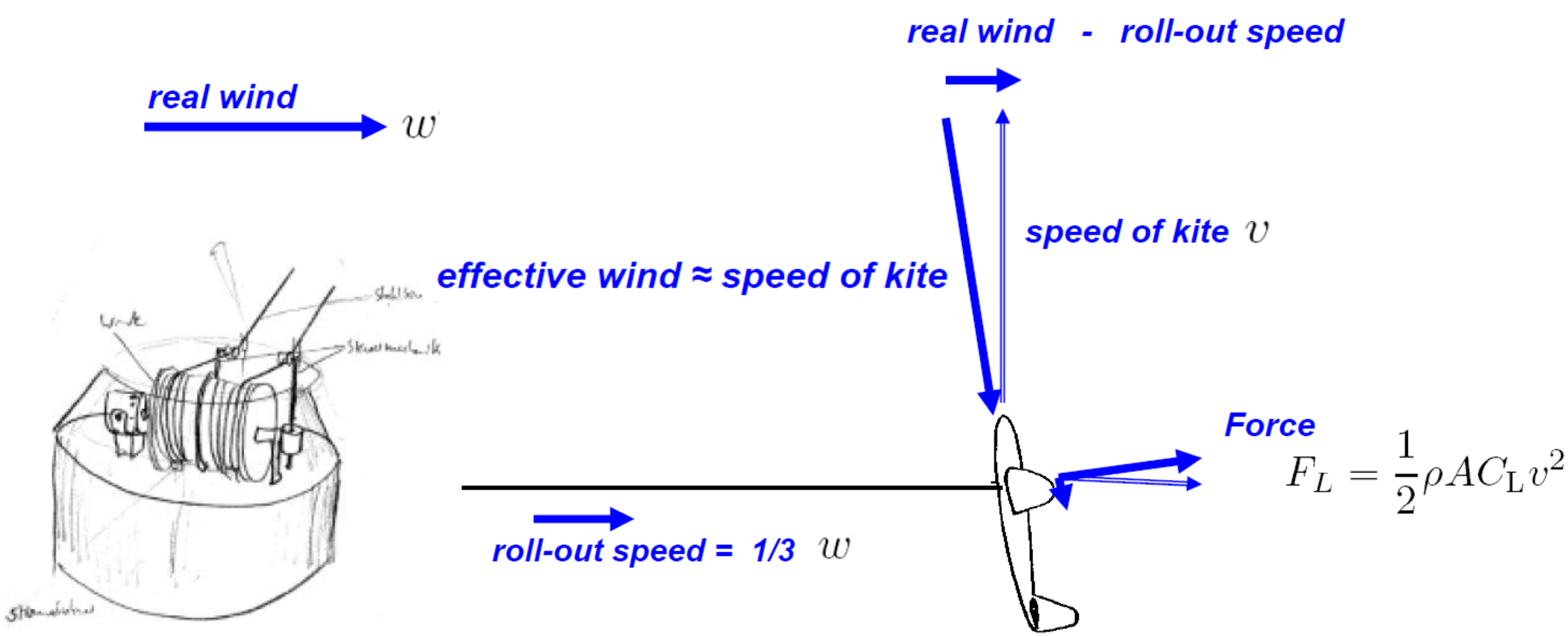
- Generated Force Could be Converted into Useful Power by Pulling a Load / Driving Turbines via a Tether

Kite moves $\frac{C_{\mathrm{L}}}{C_{\mathrm{D}}}$ *x faster than real wind!*

Pumping Power Kites

- **Maximum Power** $$P = \frac{2}{27}\rho A w^3 C_\mathrm{L} \left(\frac{C_\mathrm{L}}{C_\mathrm{D}}\right)^2$$ M. Loyd, 1980

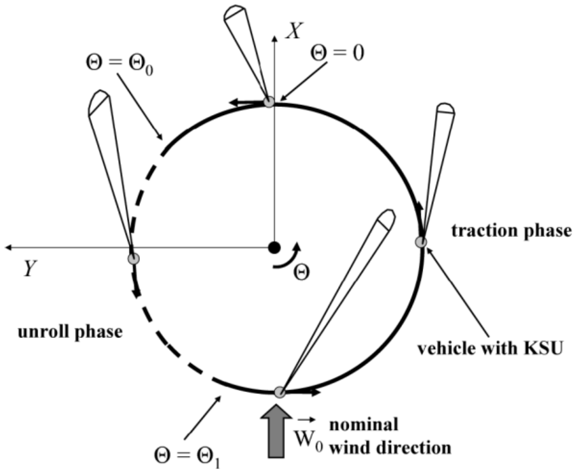
Source: M. Diehl / K.U. Leuven

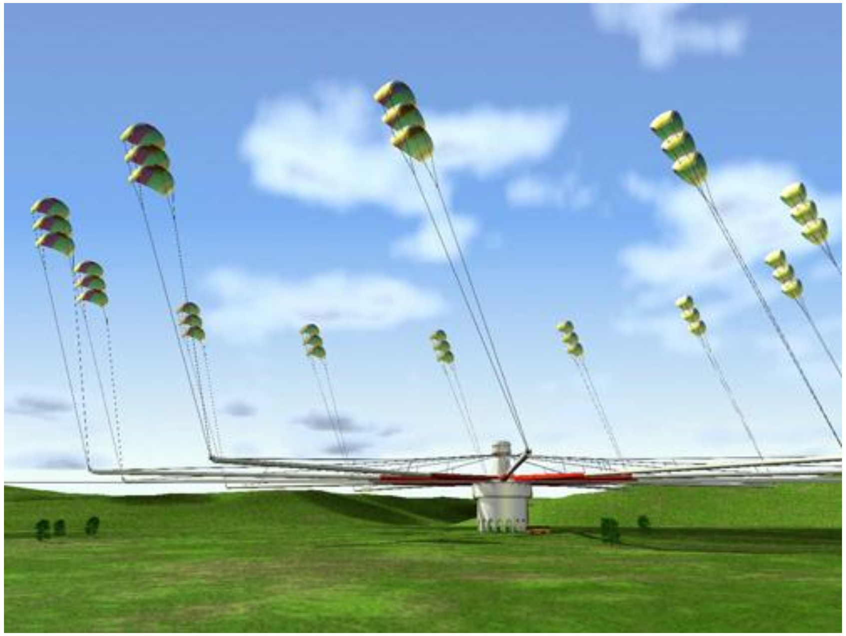


Pumping Power Kites for Capturing High Altitude Wind Power

- Lower Electricity Production Costs than Current Wind Farms
- Generate up to 250 MW/km^2, vs. the Current 3 MW/km^2
- Research at the POLITECNICO DI TORINO

KITE GEN

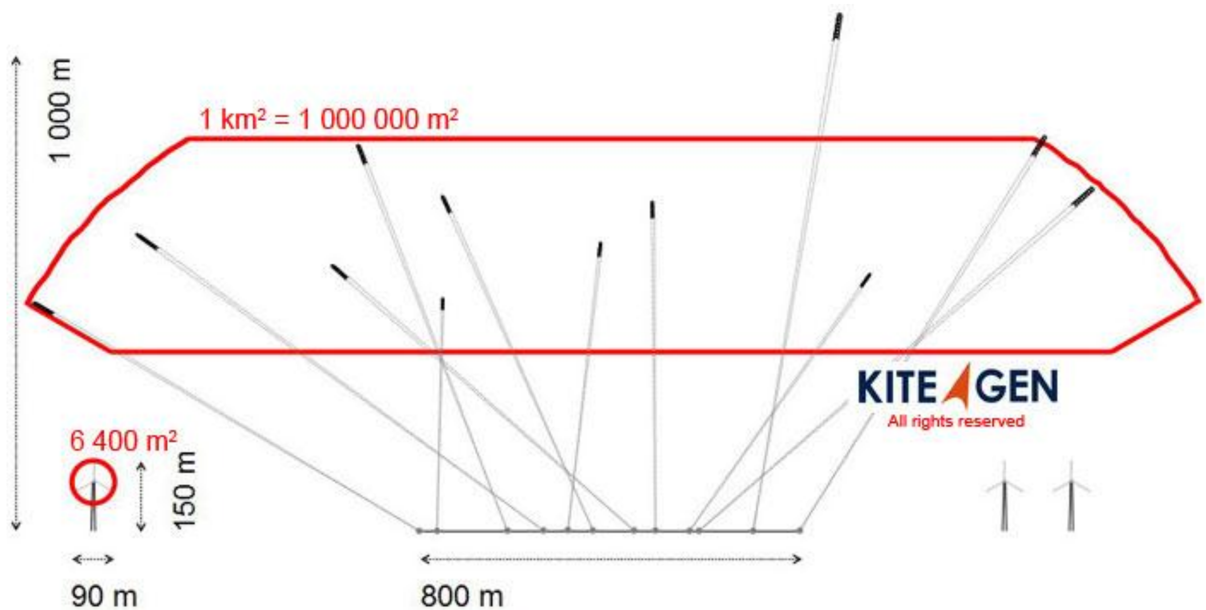




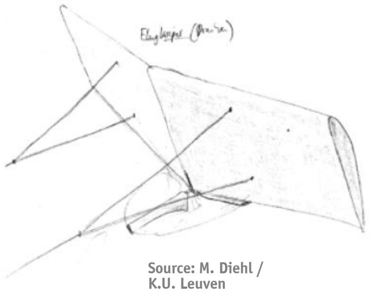
Pumping Power Kites for Capturing High Altitude Wind Power

- Lower Electricity Production Costs than Current Wind Farms
- Generate up to 250 MW/km², vs. the Current 3 MW/km²
- Research at the POLITECNICO DI TORINO

Carousel Configuration



Airborne Wind Turbine



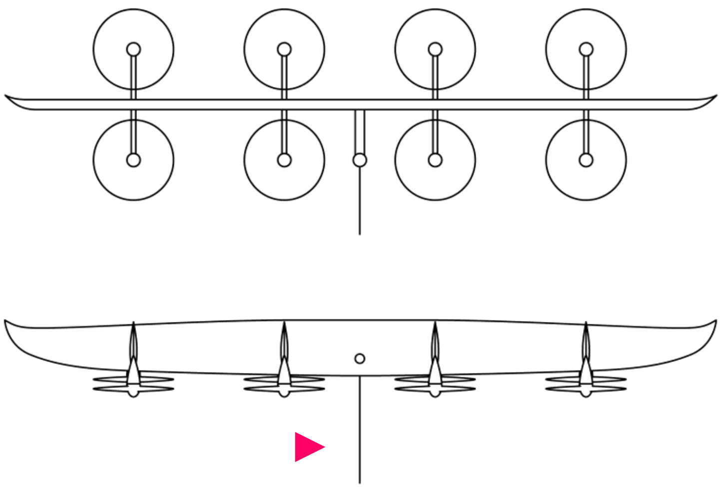
Source: M. Diehl / K.U. Leuven

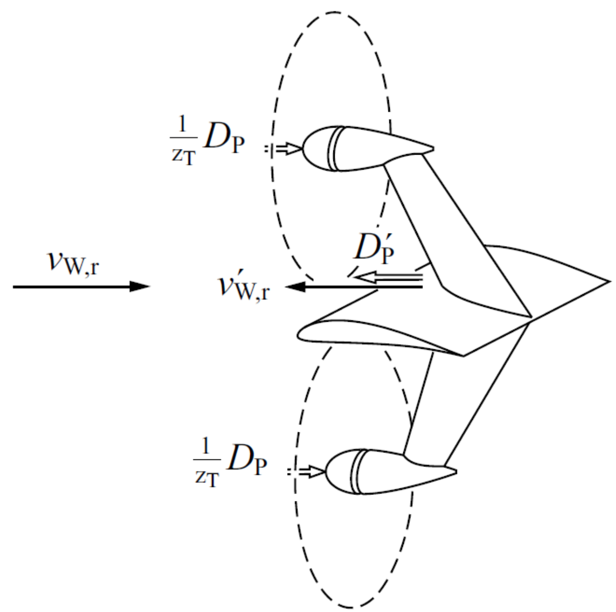
On-Board EE-Generation

Alternative Concept – Airborne Wind Turbine

- Power Kite Equipped with Turbine / Generator / Power Electronics
- Power Transmitted to Ground Electrically

M. Loyd, 1980



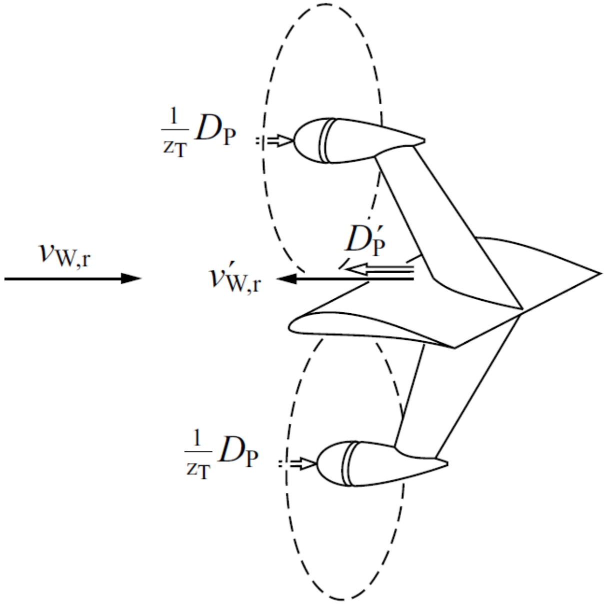


Alternative Concept – Airborne Wind Turbine

- Power Kite Equipped with Turbine / Generator / Power Electronics
- Power Transmitted to Ground Electrically

M. Loyd, 1980

Source: JOBY ENERGY

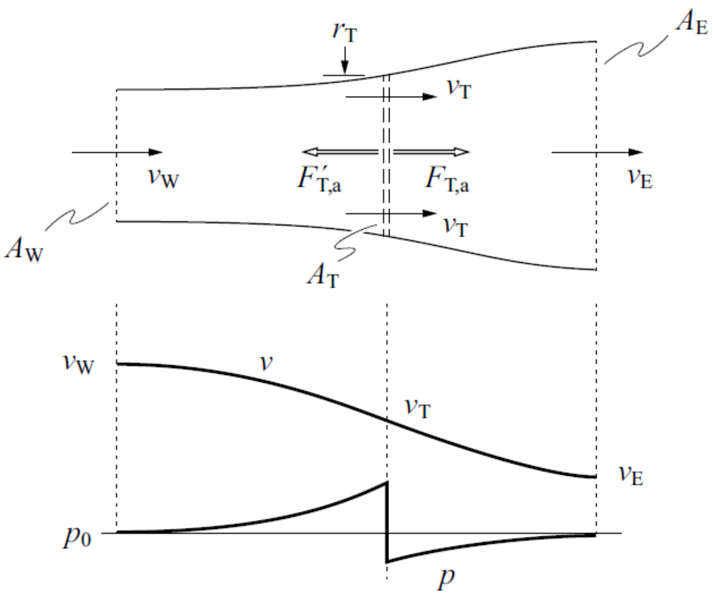


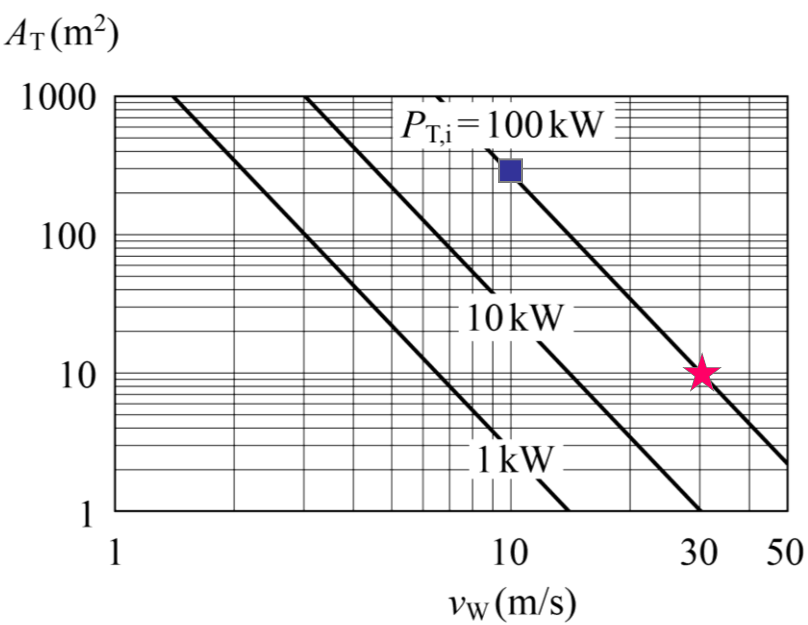
Basic Physics of Wind Turbines

- Maximum Achievable acc. to Lanchester / Betz
- High Crosswind Kite Speed → Very Small Turbine Area

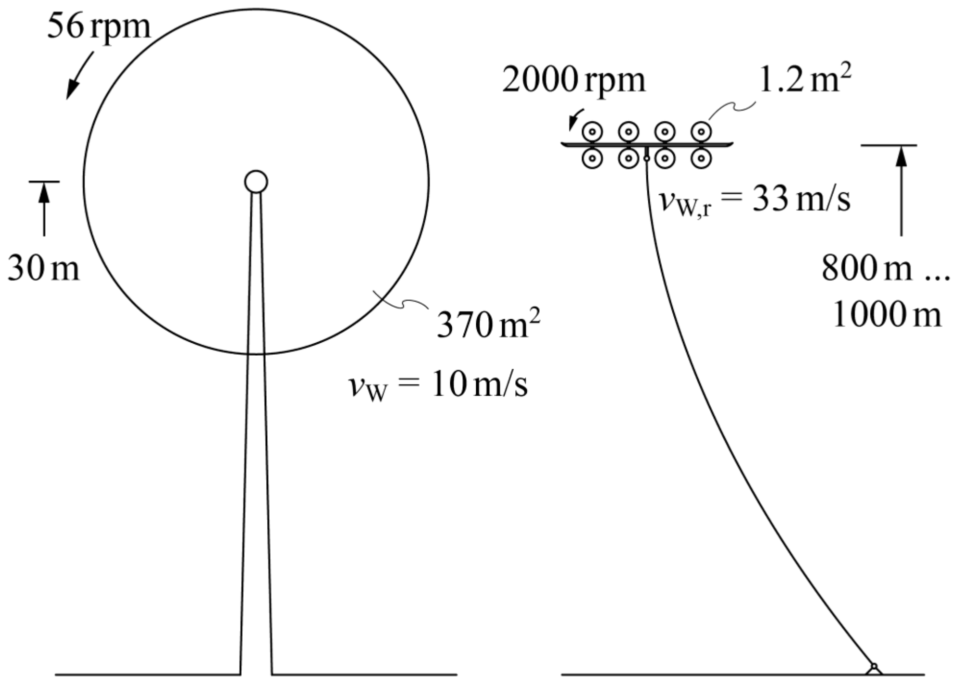
$$P_{T,i} = c_{P,i} \frac{1}{2} \rho A_T v_W^3$$

$$c_{P,i} = \frac{16}{27} \approx 0.59$$





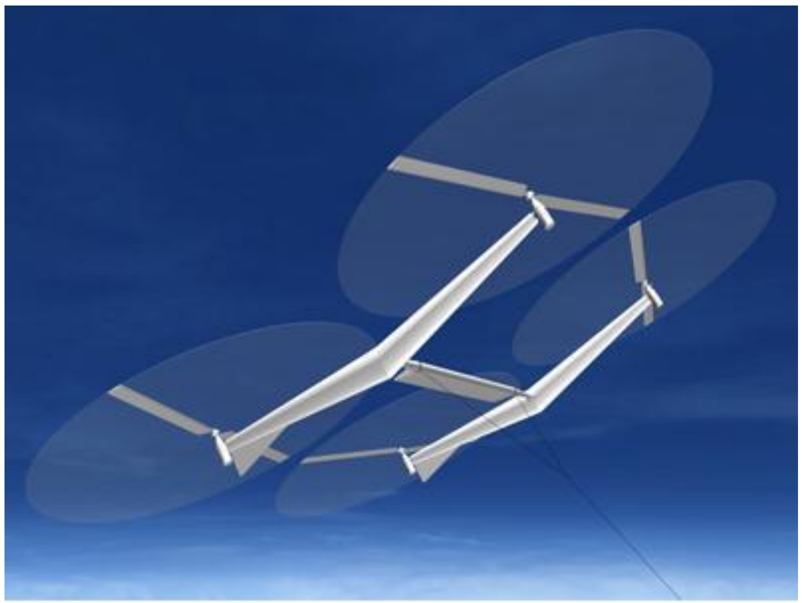
Comparison of Conventional / Airborne Wind Turbine



- Numerical Values Given for 100kW Rated Power

SkyWindPower AWT Concept

- Tethered Rotorcraft – Quadrupole Rotor Arrangement
- Inclined Rotors Generate Lift & Force Rotation / Electricity Generation



SKY WINDPOWER

Artist´s Drawing of
240kW / 10m Rotor System

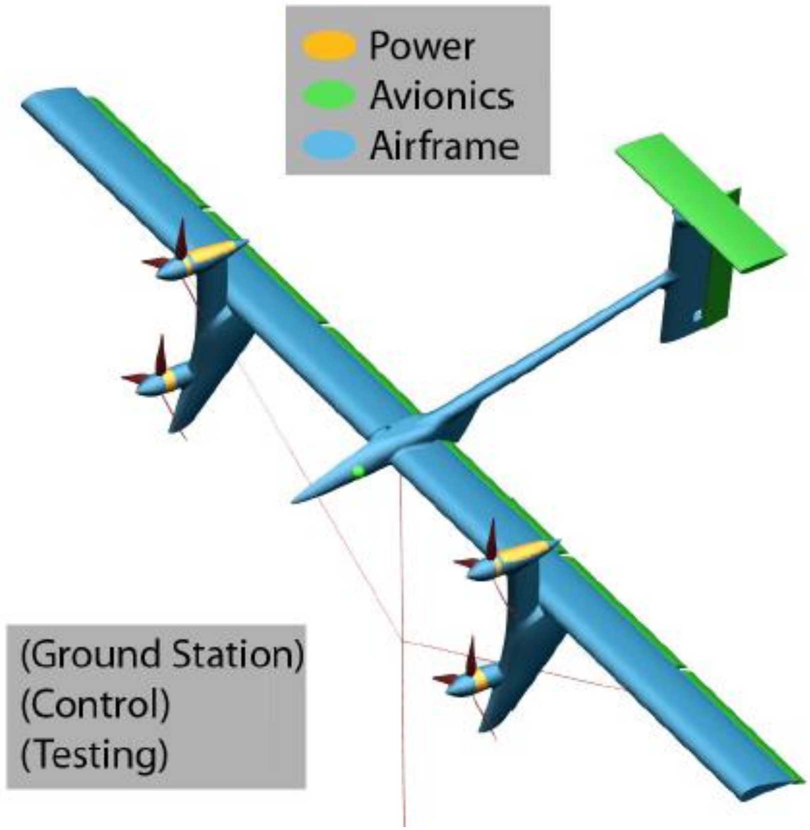
- Named as One of the 50 Top Inventions in 2008 by TIME Magazine

JOBY ENERGY AWT Concept

- Reinforced Tether Transfers MV-Electricity to Ground
- Composite Tether also Provides Mechanical Connection to Ground

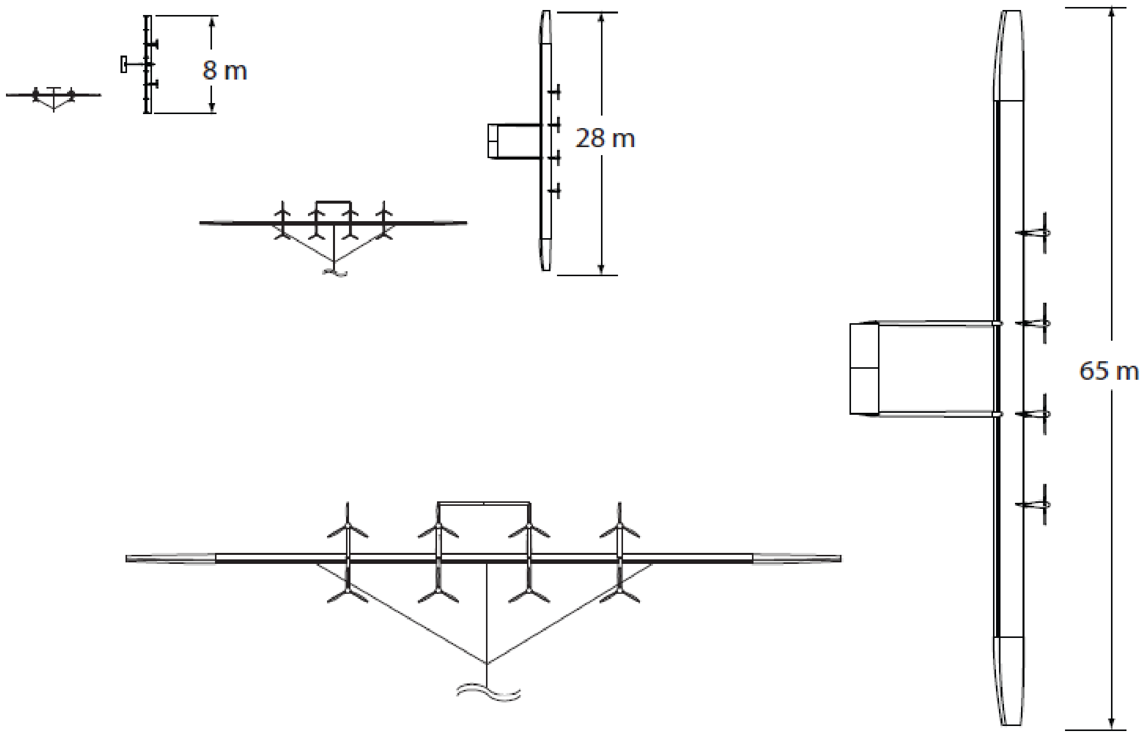
MAKANI POWER

AWT Concept



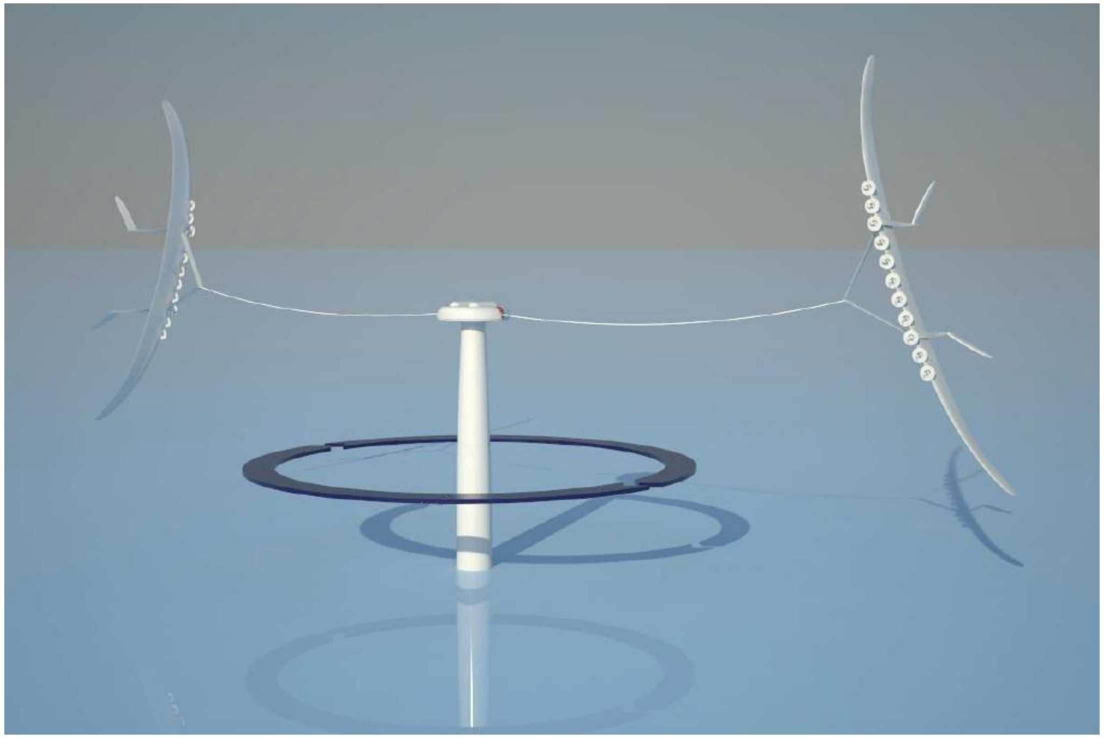
MAKANI POWER Demonstration Plan

W7 30 KW	M600 600 kW	M5 5 MW



MAKANI POWER Flight Modes / Parked

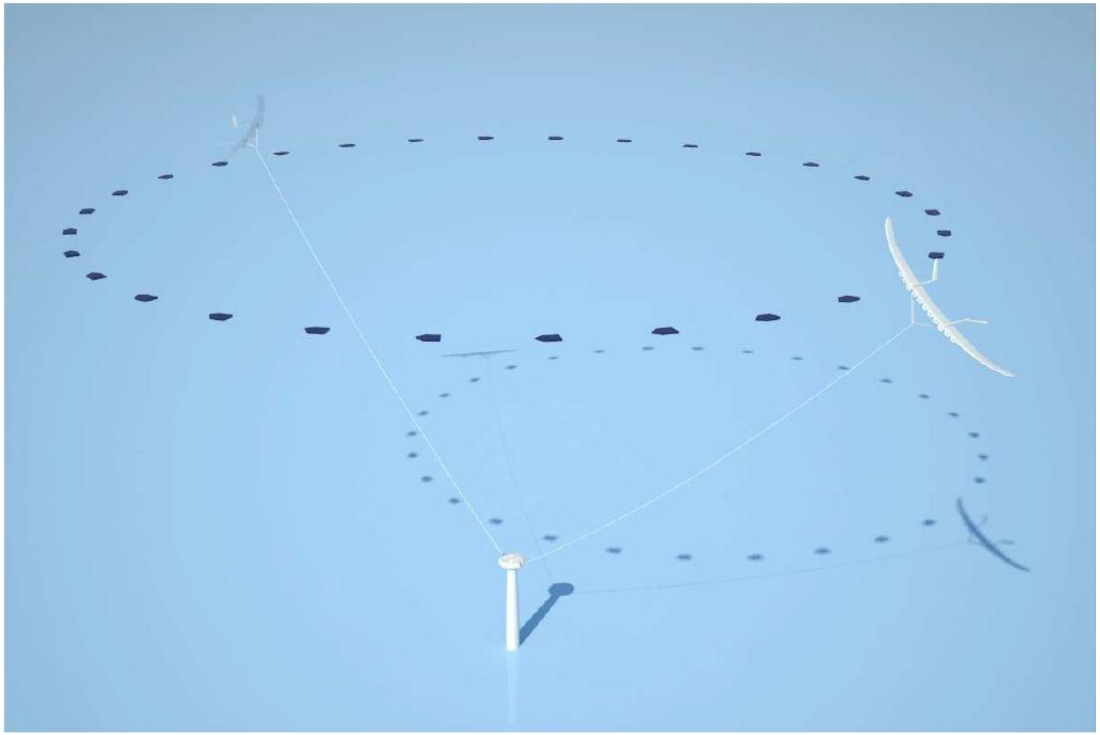
Future Prospects



Source: M. Diehl / K.U. Leuven

- Example for Thinking "Out-of-the-Box" !

Future Prospects



Source: M. Diehl / K.U. Leuven

- Example for Thinking “Out-of-the-Box” !

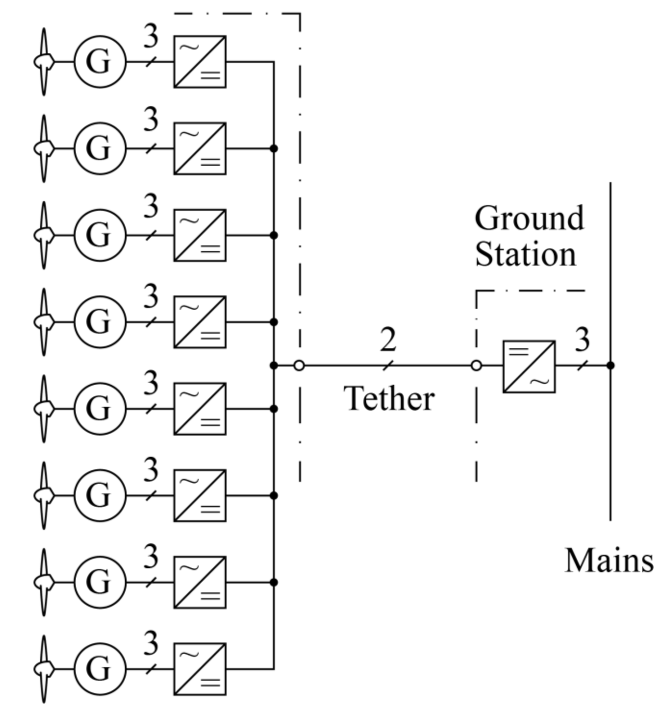
Technical Feasibility of AWT Electrical System

- AWT Electrical System Structure
- Multi-Objective Optimization (*Weight vs. Efficiency*)
- Controls Aspects

AWT Basic Electrical System Structure

▶ Rated Power	100kW
▶ Operating Height	800...1000m
▶ Ambient Temp.	40°C
▶ Power Flow	Motor & Generator

Airborne Wind Turbine



Turbines, Generators, and Power Electronics

■ El. System Target Weight	100kg
■ Efficiency (incl. Tether)	90%
■ Turbine /Motor	2000/3000rpm

Design of Electrical Power System

- Clarify Practical Feasibility of AWT Concept
- Clarify Weight/Efficiency Trade-off / Multi-Objective Optimization / PARETO-Front

Tether Design

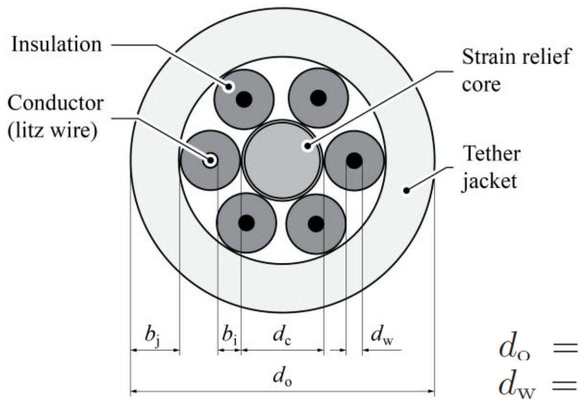
DC Voltage Level
η-γ-PARETO Front

Tether DC Transmission Voltage Level

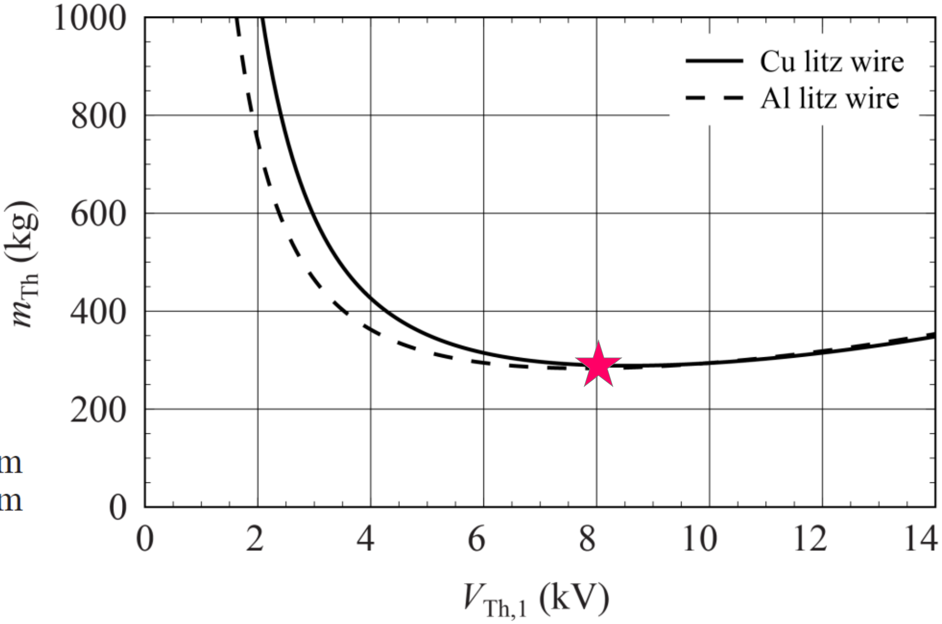
- $P_{th,1}$ = 100kW / l_{th} = 1000m
- Strain Relief Core – Kevlar (F_{th} = 70kN, d=5mm)
- Cu or Al Helical Conductors - ½ U_{th} Isolated
- Outer Protection Jacket (3mm)

$$\eta_{Th} = 98.5\%$$

$$b_i = 0.0144 \frac{mm}{kV^2} \cdot V_i^2 + 0.1694 \frac{mm}{kV} \cdot V_i + 0.40\,mm$$

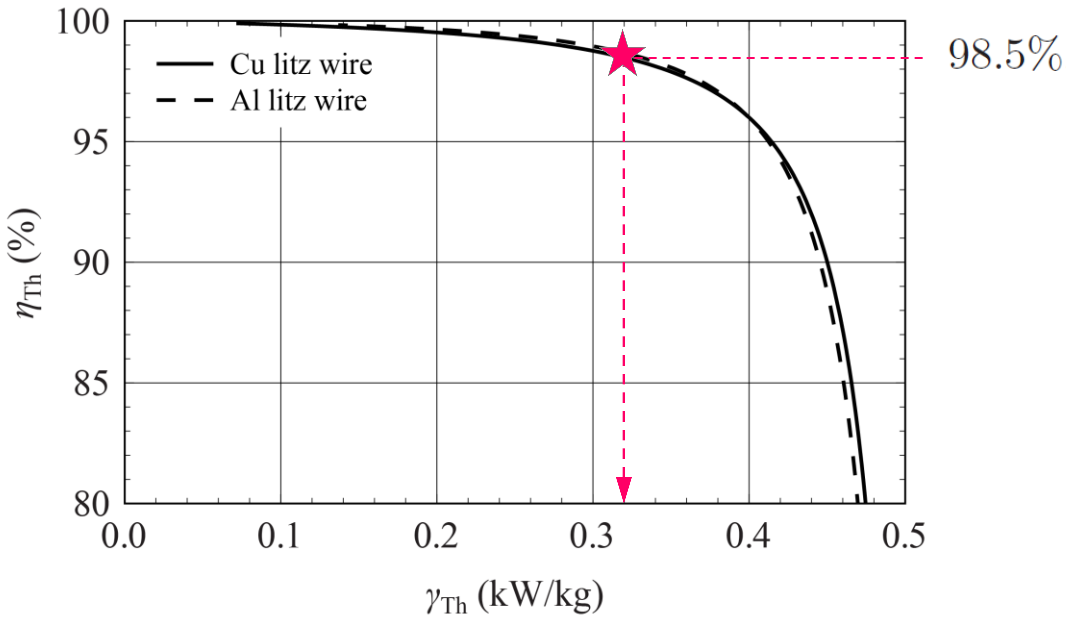


$$d_o = 19\,mm$$
$$d_w = 1.5\,mm$$



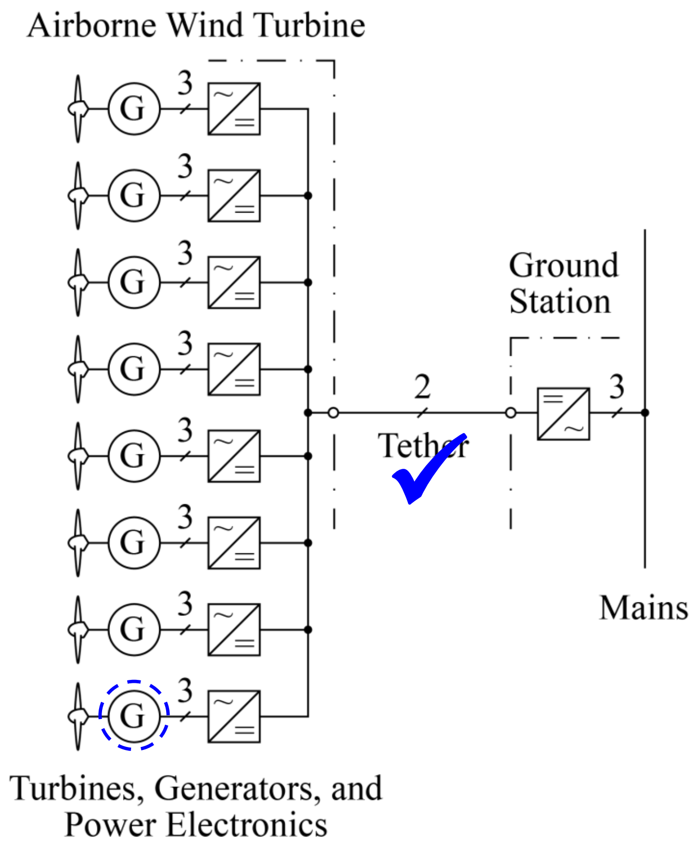
Tether η-γ-PARETO Front

- **Tether Voltage $V_{th,1}$ = 8kV**



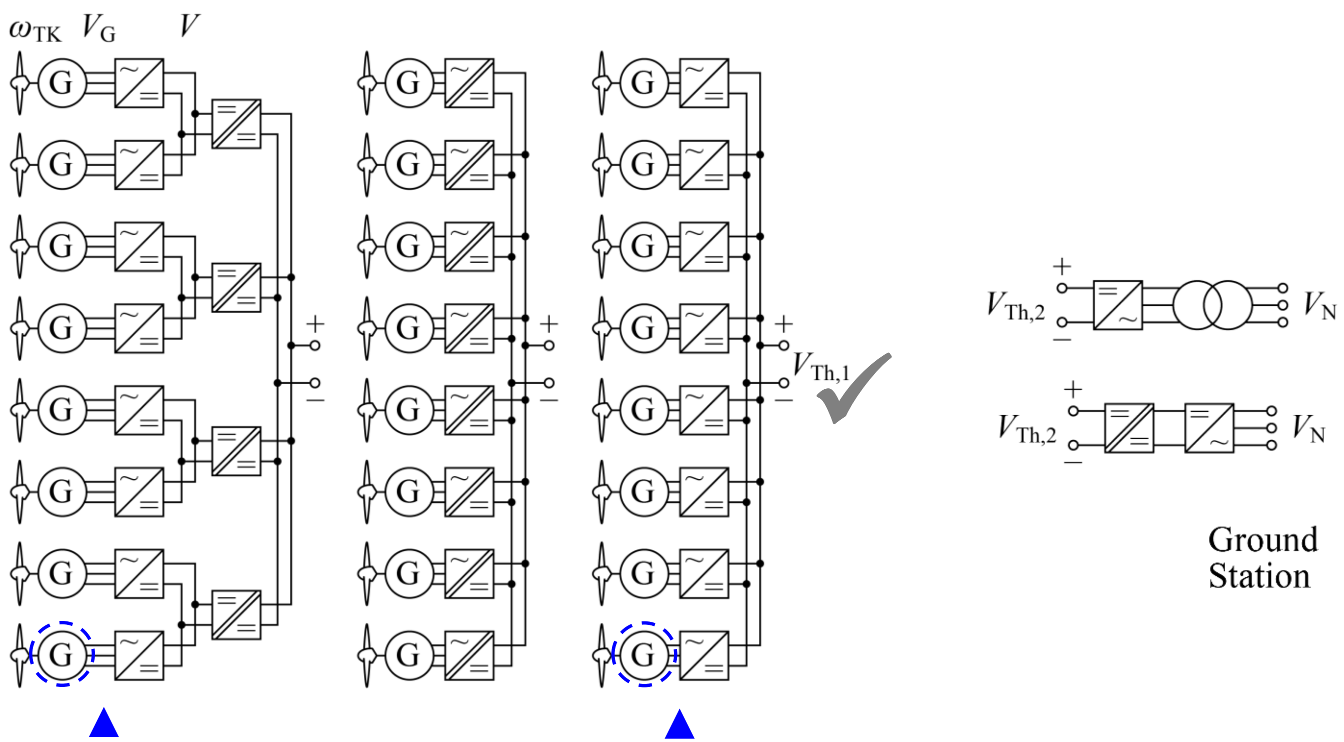
- **Total Weight of Tether: 320kg**

System Overview



Possible AWT Electrical System Structures

- ▶ Low-Voltage or Medium-Voltage Generators / Power Electronics
- ▶ Decision Based on Weight/Efficiency/Complexity



Generator / Motor Design

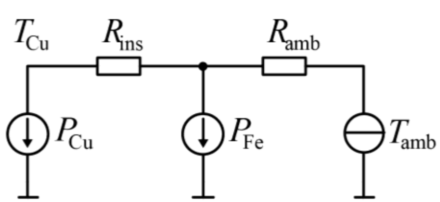
Dimensions
Number of Pole Pairs
η-γ-PARETO Front

Generator / Motor η-γ-PARETO Front

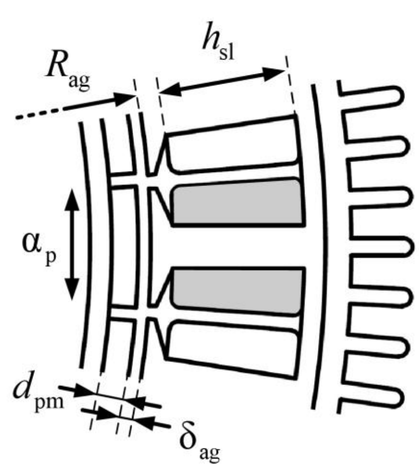
► Medium Voltage vs. Low Voltage Machine $V_{th,1}$ = 8kV

- PMSM – Radial Flux – Internal Rotor - Slotted Stator / Concentrated Windings – Air Cooling
- Analytical EM and Thermal Models for Weight / Efficiency Optimization
- P = 16kW / 2000rpm

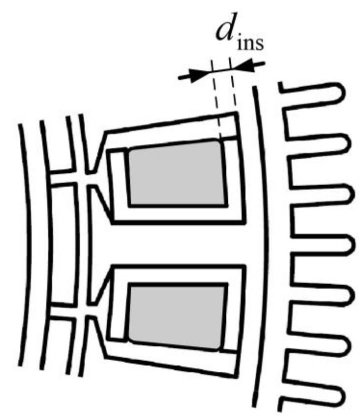
$$\eta_{mot} = \frac{P_{mech}}{P_{mech} + P_v}$$



Thermal Model



LV Machine



HV Machine

■ LVG: Diameter 17cm (excl. Cooling Fins) / Width 6.0cm / p = 20 / η = 95.4% / Weight 5.1kg

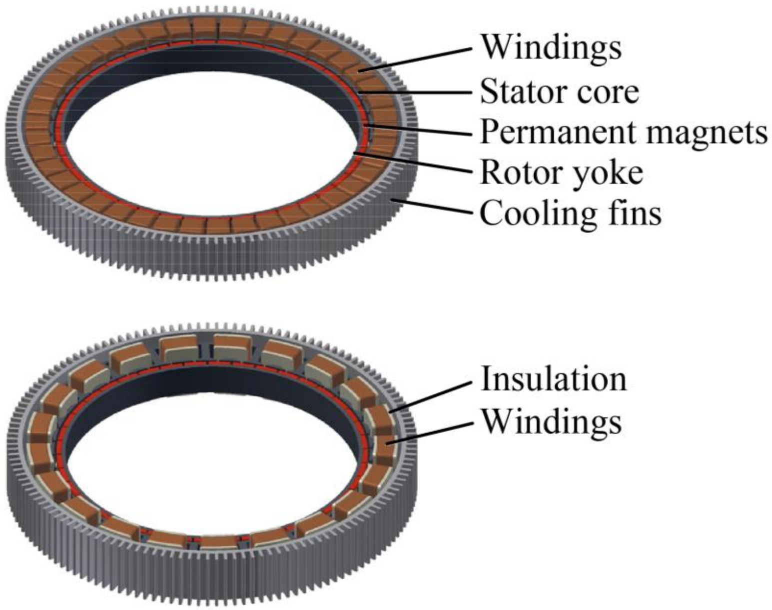
CAD Drawing of LV and MV Machine

▶ Fixed Parameters and Degrees of Freedom

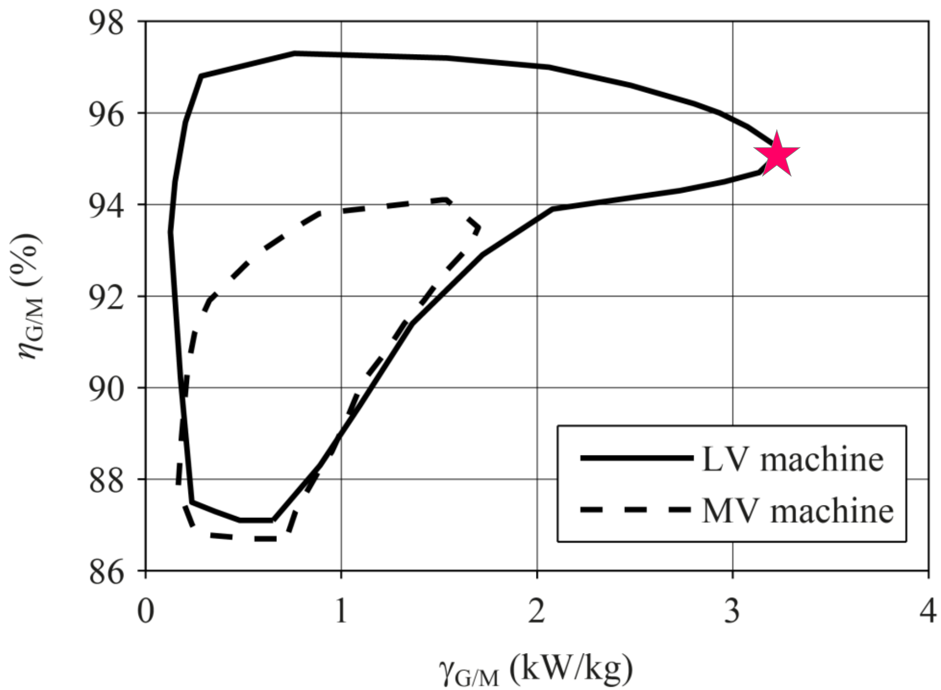
MACHINE OPTIMIZATION PARAMETERS AND FIXED PARAMETERS

Optimization parameters	Symbol	Range
Air-gap radius	R_{ag}	$50 \ldots 250$ mm
Active length	L	$10 \ldots 60$ mm
Slot depth	h_{sl}	$5 \ldots 20$ mm
Permanent magnet thickness	d_{pm}	$2 \ldots 8$ mm
Pole coverage factor	α_p	$0.8 \ldots 1$
Number of pole pairs	p	$5 \ldots 30$

Fixed parameters	Symbol	Value
Air gap	δ_{ag}	1.5 mm
Copper filling factor	k_{Cu}	0.45
Permanent magnet remanence	B_{rem}	1.3 T
Iron saturation flux density	B_{sat}	2.2 T
Insulation thickness (MV machine only)	d_{ins}	2 mm



Generator / Motor η-γ-PARETO Front



▶ **Selected Design**
η = 95.4%
γ = 3.1 kW/kg

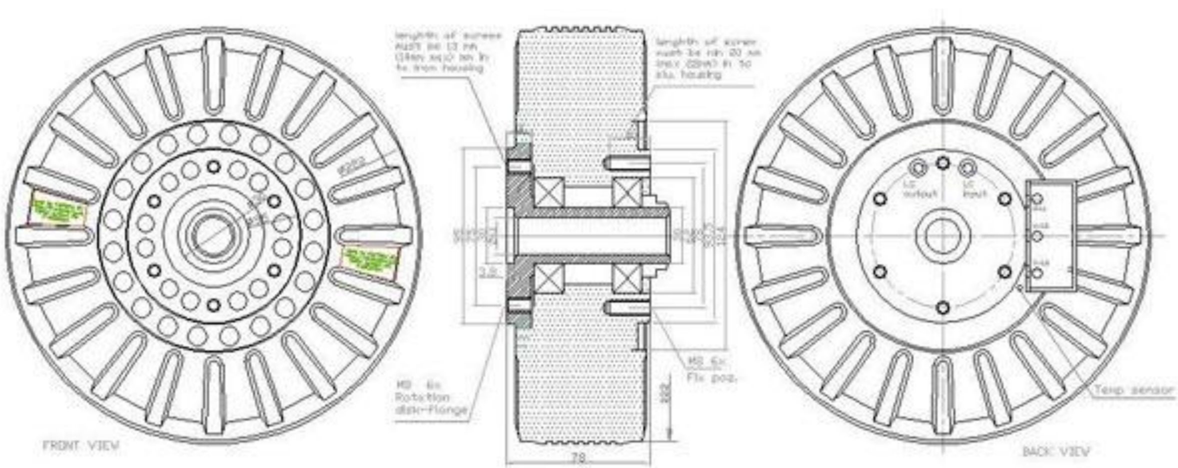
■ **Medium Voltage Machine Not Considered Further**

Comparison to Commercial Motors

- **Motors Employed for Electric Propulsion of Glider Airplane**

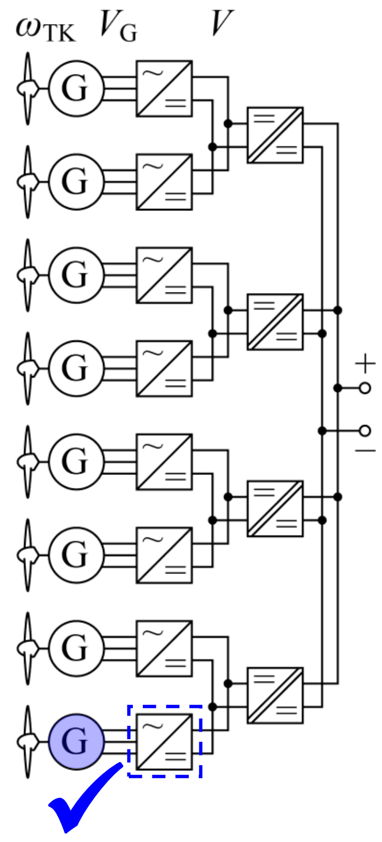
ENSTROJ
electric motor innovation
established in 1991

Power P = 10kW
Speed n = 2200rpm
Cooling v_L = 25m/s



- Diameter 22cm
  Width 8.6cm
  Weight 12kg
  Pole Pairs 10
  Efficiency 91%

System Overview



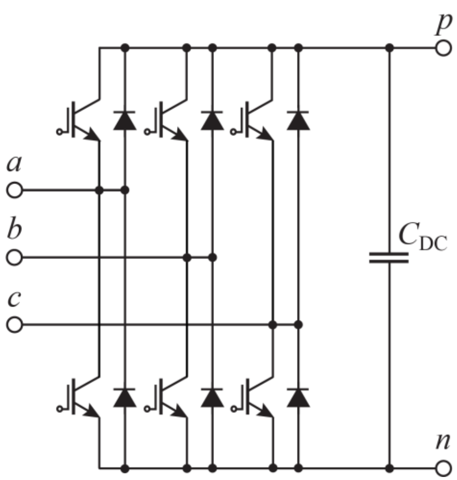
Rectifier / Inverter Design

Chip Area
Heatsink Volume
η-γ-PARETO Front

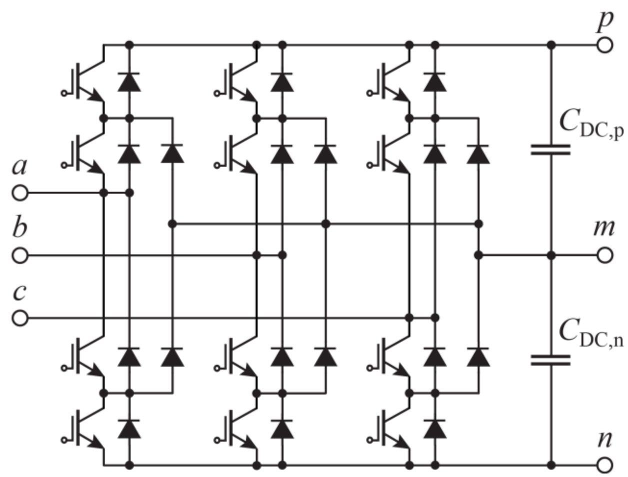
Rectifier / Inverter Design

▶ 2-Level or 3-Level Bidirectional Voltage Source Rectifier

- S = 19.3kVA
- V_{DC} = 750V
- $f_{S,min}$ = 24kHz
- T_J = 125°C
- Foil Capacitor DC Link



1200V T&FS Si IGBT4s /
1200V SiC Diodes

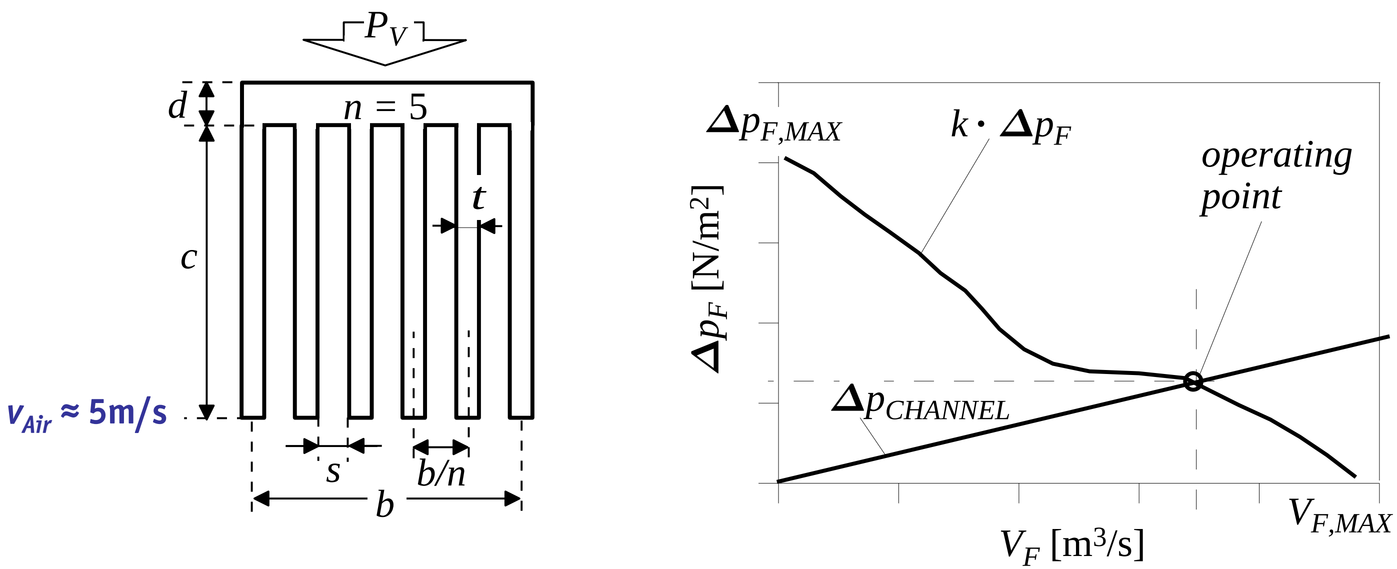


600V T&FS Si IGBT3s /
600V Si EmCon3 Diodes

■ Maximization of Heatsink Thermal Conductance / Weight (Volume) - Max. CSPI

Heatsink Optimization

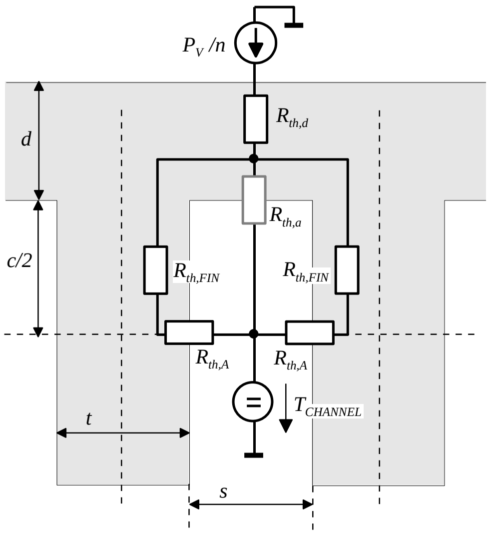
► Maximize Thermal Conductance / Weight (Volume)

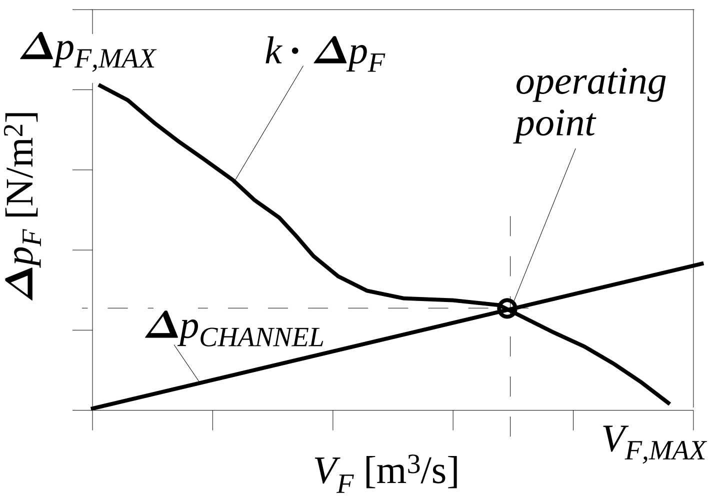


- Highest Performance Fan
- Fin Thickness / Channel Width Optimization

Heatsink Optimization

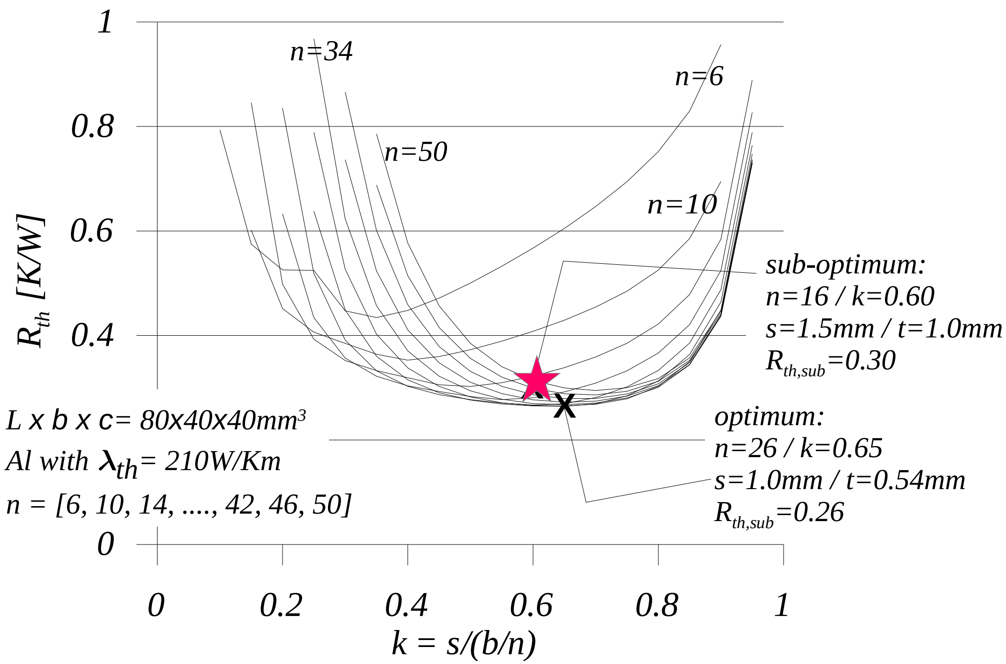
▶ Maximize Thermal Conductance / Weight (Volume)





- Highest Performance Fan
- Fin Thickness / Channel Width Optimization

Heatsink Optimization



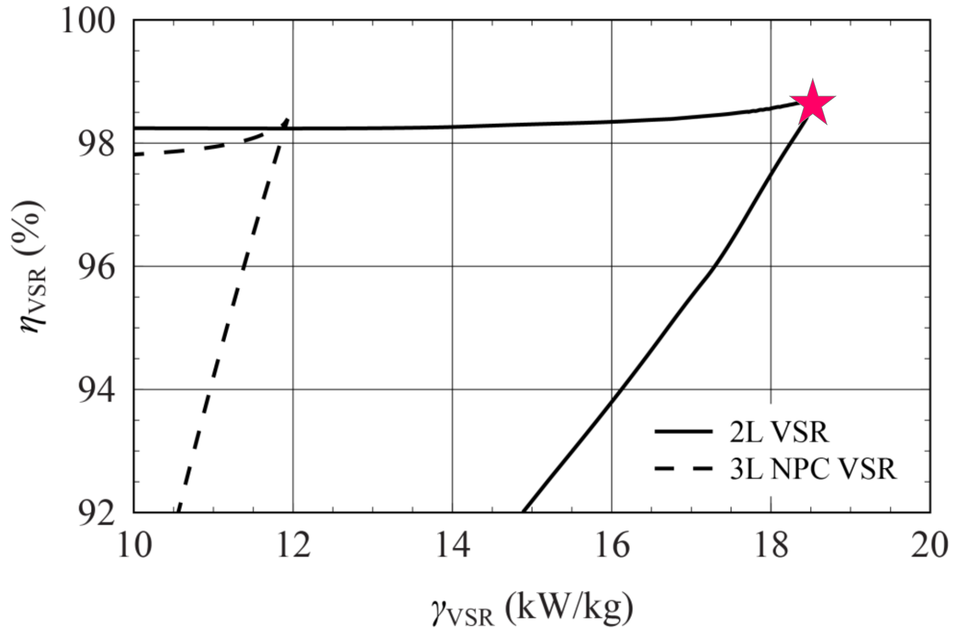
- **Optimum**

$$CSPI_{\mathrm{m}} = 15.0\frac{\mathrm{W}}{\mathrm{K\,kg}}$$

- Highest Performance Fan
- Fin Thickness / Channel Width Optimization

Rectifier / Inverter η-γ-PARETO Front

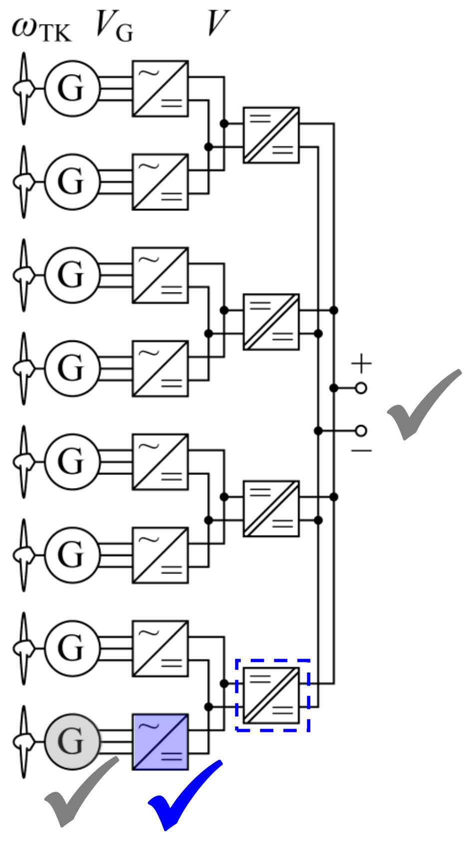
- Switching Frequency Range 24...70 kHz
- Heatsink Temperature Range 55...100 °C (T_{amb} = 40°C)



▶ **Selected Design**
η = 98.5%
γ = 19 kW/kg

■ 3-Level Topology Does Not Show a Benefit

System Overview



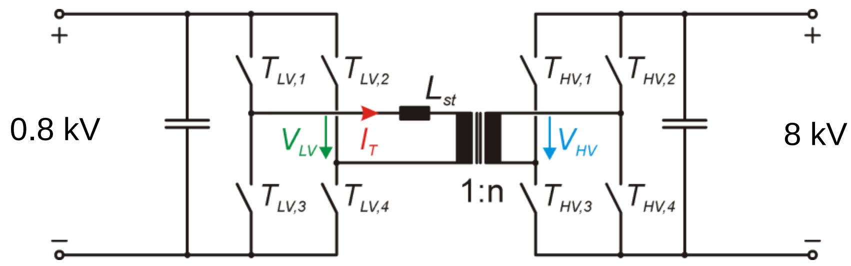
$8kV_{DC}/750V_{DC}$ DAB Converter Design

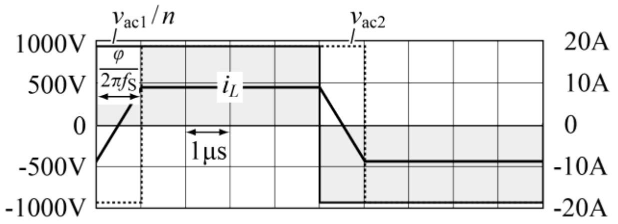
Switches / Topology
Transformer
η-γ-PARETO Front

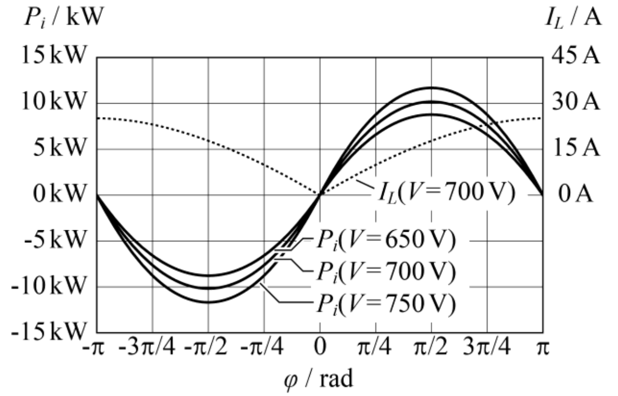
DC/DC Converter Topology

▶ **Bidirectional Energy Transfer - Dual Active Bridge**

- Weight ≤ 25kg
- f_S = 50...125kHz → $f_{S,m}$ = 100kHz
- Phase-Shift Control (φ = $\pi/4$)





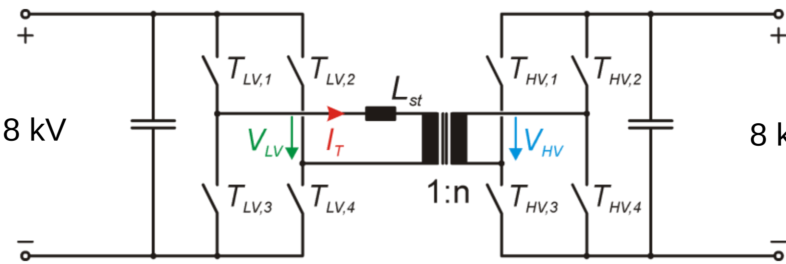


■ **Implementation of Electronic Switches - SiC**

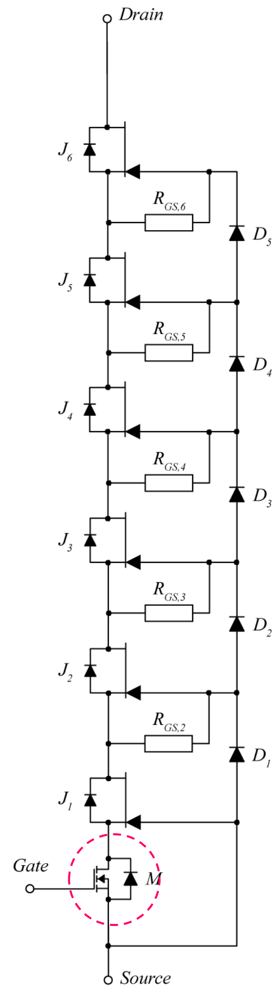
DC/DC Converter Topology

▶ **Bidirectional Energy Transfer - Dual Active Bridge**

- Weight ≤ 25kg
- f_S = 50…125kHz → $f_{S,m}$ = 100kHz
- Phase-Shift Control (φ = $\pi/4$)



▶ **10kV Si/SiC SuperCascode Switch**



■ Implementation of Electronic Switches - SiC

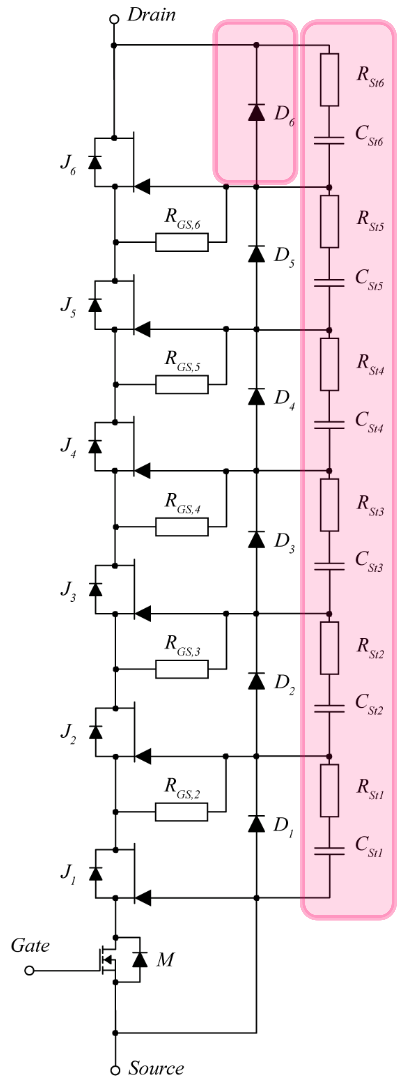
Si/SiC Super Cascode Switch

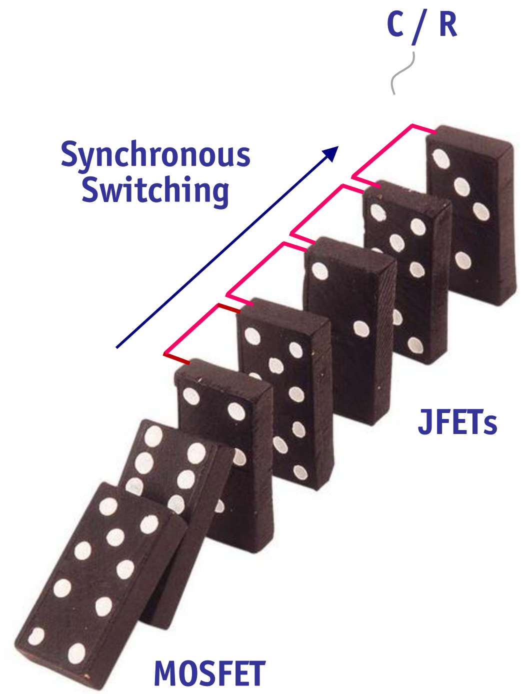
➔ HV-Switch Controllable via Si-MOSFET

- * 1 LV Si MOSFET
- * 6 HV 1.7kV SiC JFETs
- * Avalanche Rated Diodes

➔ Ultra Fast Switching
➔ Low Losses
➔ Parasitics

- * Passive Elements for Simultaneous Turn-on and Turn-off
- * Stabilization of Turn-off State Voltage Distribution





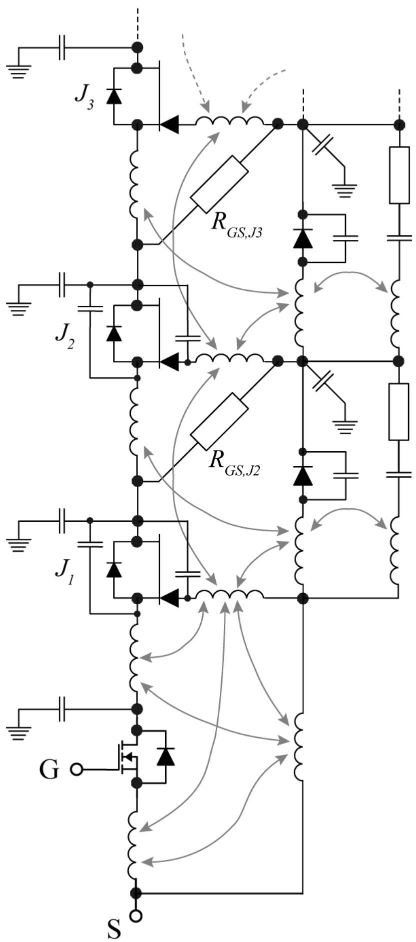
Si/SiC Super Cascode Switch

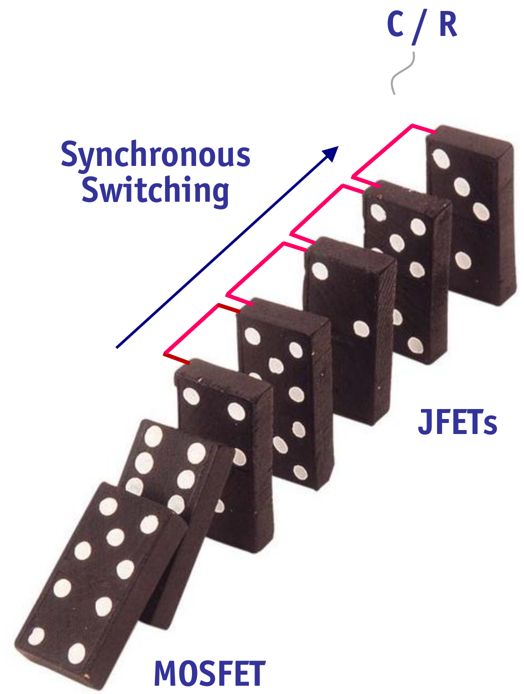
➔ HV-Switch Controllable via Si-MOSFET

* 1 LV Si MOSFET
* 6 HV 1.7kV SiC JFETs
* Avalanche Rated Diodes

➔ Ultra Fast Switching
➔ Low Losses
➔ Parasitics

* Passive Elements for Simultaneous Turn-on and Turn-off
* Stabilization of Turn-off State Voltage Distribution

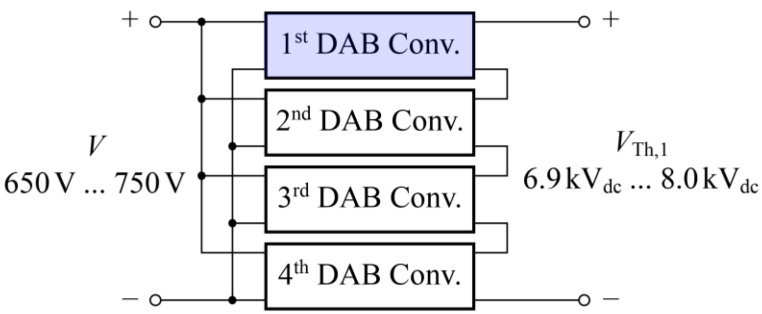


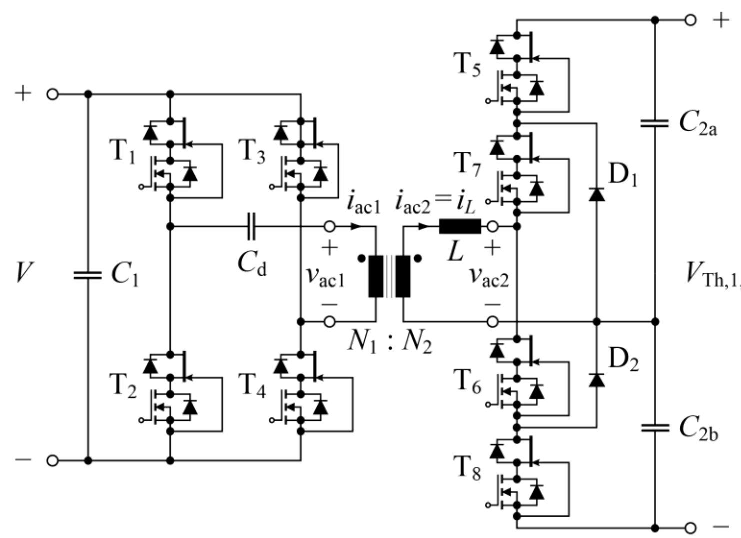


Selected Multi-Cell Converter Topology

► **MV-Side Series-Connection / LV-Side Parallel-Connection**

$P_i = 6.25\text{kW}$
$V_{th,1,i} = 2\text{kV}$

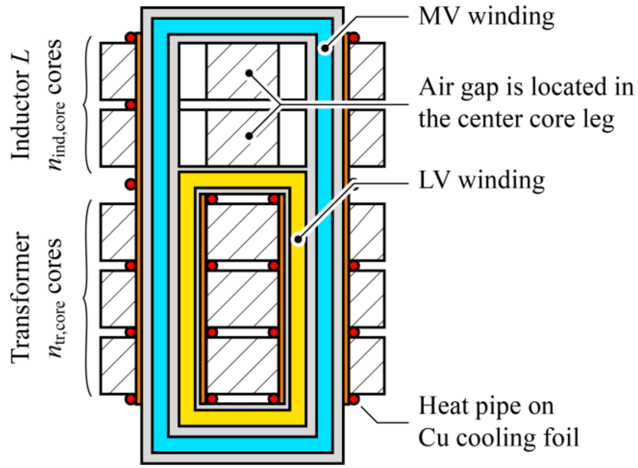


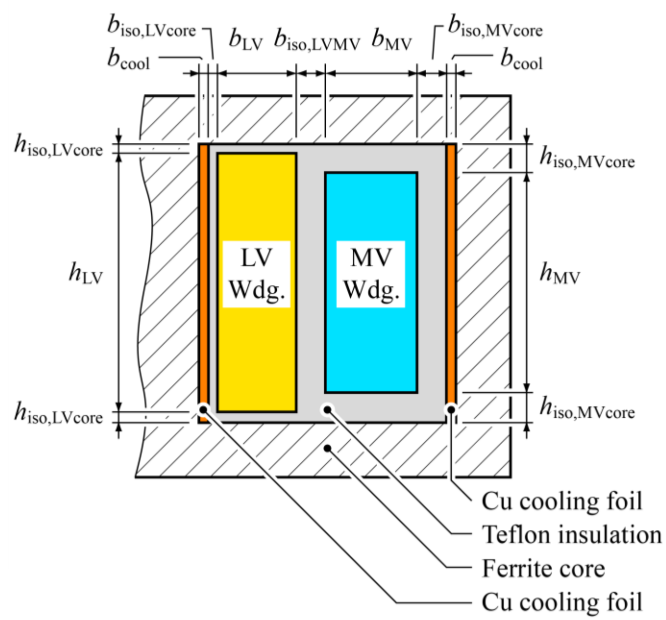


■ **Winding Arrangement & Efficiency / Weight Optimization of Transformer**

Transformer Design

- ▶ MV-Winding Arranged Around Inductor Cores
- ▶ Cooling Provided by Heatpipes
- ▶ Stacked Cores - Scalable Arrangement



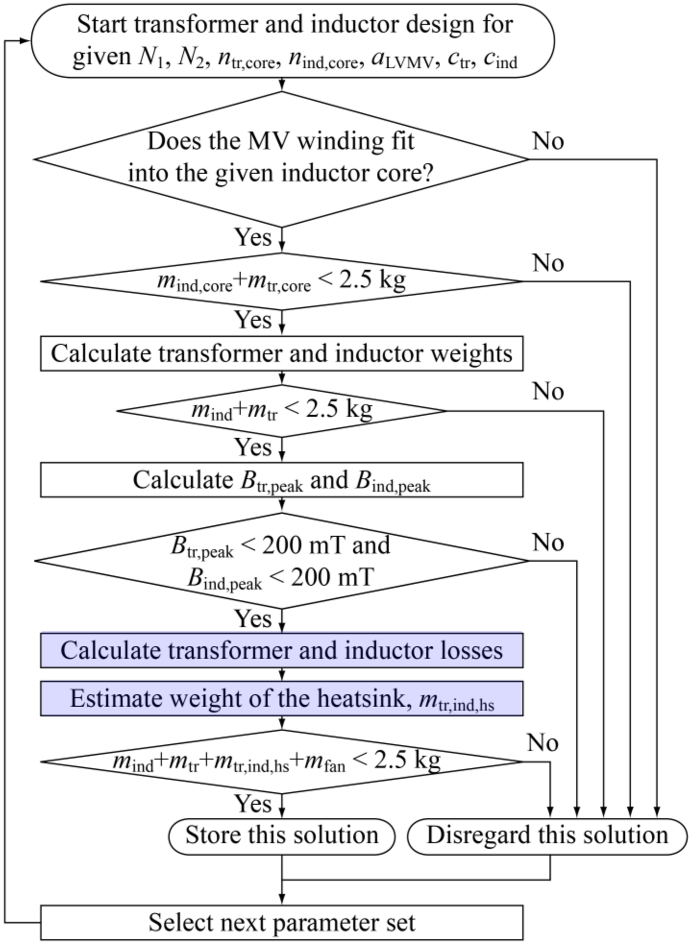


- ■ Optimization - Weight / Efficiency Trade-off

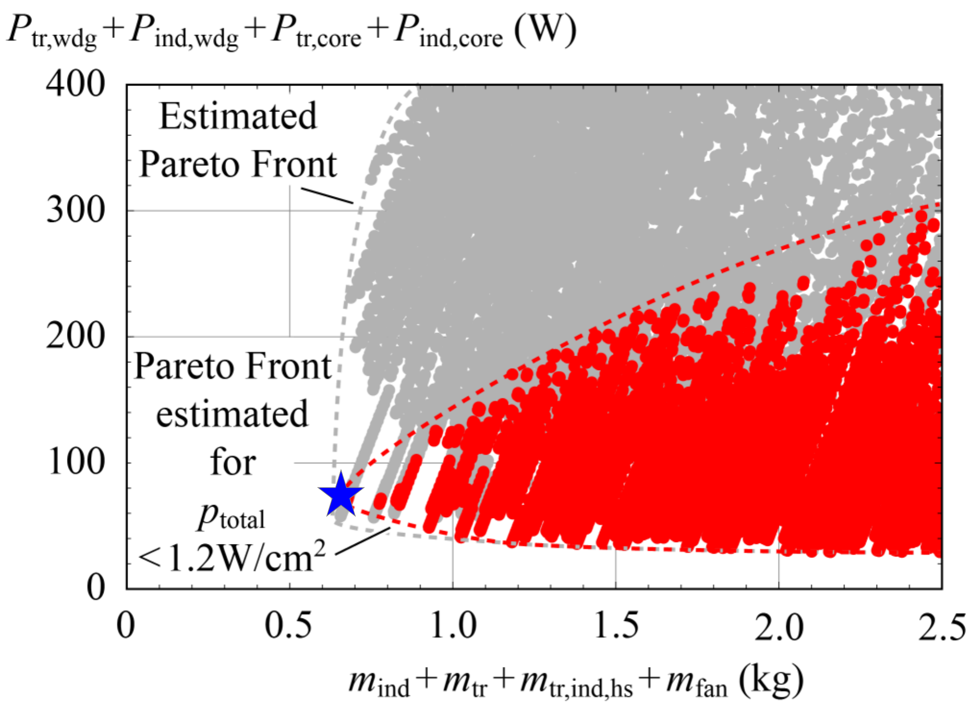
Transformer Optimization

- **Degrees of Freedom / Parameter Ranges**

$$\vec{N}_1 = [5\ 6\ 7\ 8\ 9\ 10\ 11\ \dots\ 39\ 40]^T,$$
$$\vec{N}_2 = \mathrm{round}(\vec{N}_1 \cdot 1\,\mathrm{kV}/750\,\mathrm{V}),$$
$$\vec{n}_{\mathrm{tr,core}} = [1\ 2\ 3\ 4\ 5\ 6\ 8\ 10\ 12\ 14\ 16\ 18\ 20]^T,$$
$$\vec{n}_{\mathrm{ind,core}} = [1\ 2\ 3\ 4\ 5\ 7\ 10]^T,$$
$$\vec{a}_{\mathrm{LVMV}} = [0.75\ 1.0\ 1.25]^T,$$
$$\vec{c}_{\mathrm{tr}} = [\mathrm{E30/15/7}\ \ \mathrm{E32/16/9}\ \ \mathrm{E42/21/20}\ \ \mathrm{E55/28/21}\ \ \mathrm{E65/32/27}\ \ \mathrm{E70/33/32}\ \ \mathrm{UI93/76/30}\ \ \mathrm{UU93/76/30}]^T$$
$$\vec{c}_{\mathrm{ind}} = \vec{c}_{\mathrm{tr}}$$



Transformer η-γ-PARETO Front

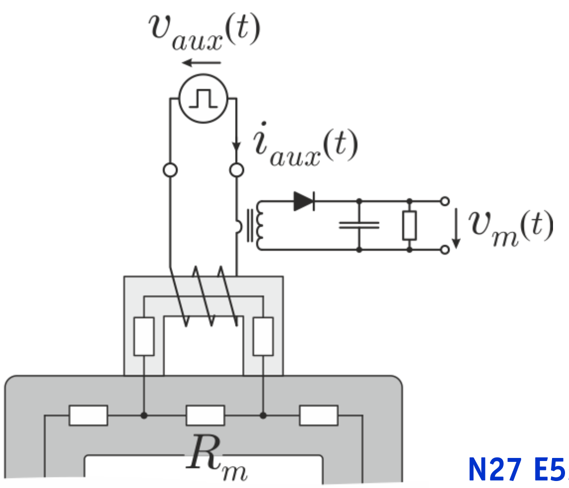


▶ **Selected Design**
η = 97%
γ = 4.5 kW/kg

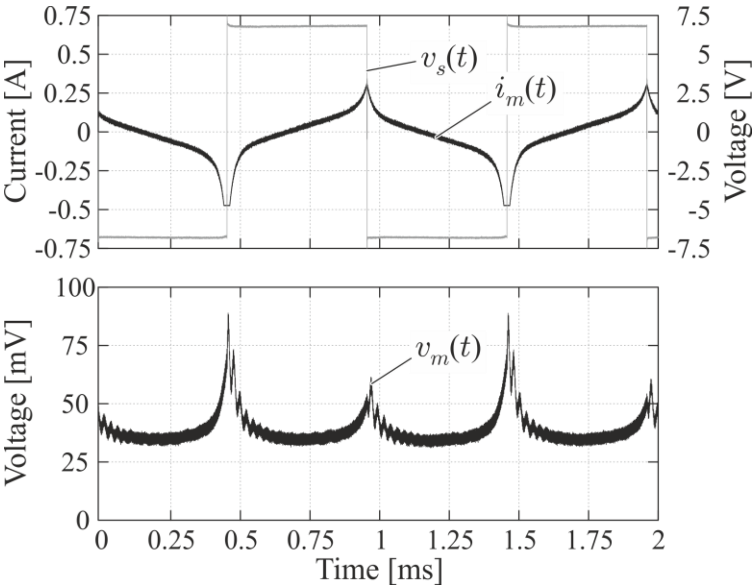
■ **Transformer Volt-Second Balancing - Series Capacitor or "Magnetic Ear" Control**

Transformer Volt-Second Balancing – "Magnetic Ear"

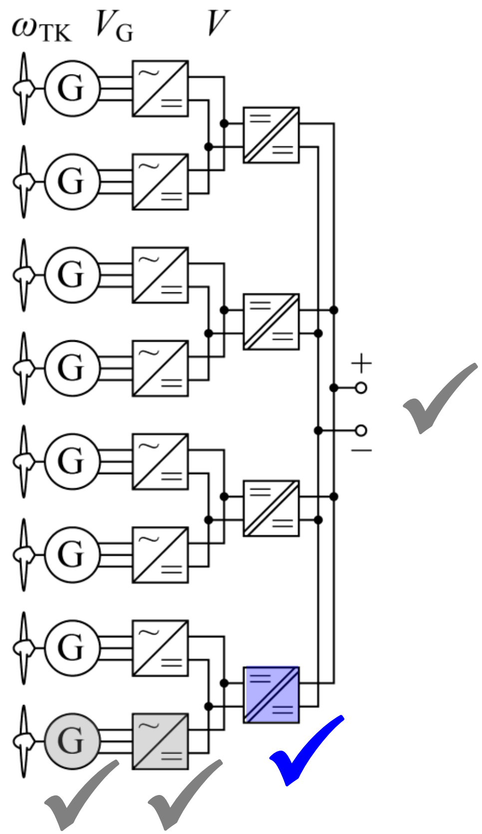
- Magnetic Ear Magnetized with 50% Duty Cycle Rectangular Voltage Winding
- Measured Aux. Current i_{aux} / Voltage v_m Indicates Flux Level
- Enables Closed-Loop Flux Control



N27 E55 Ferrite



System Overview

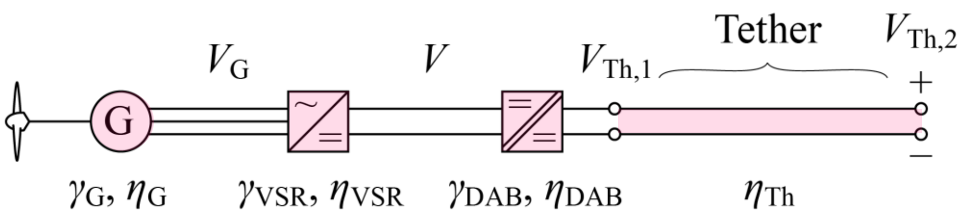


Overall System Consideration

Total Weight
Overall Efficiency
η-γ-PARETO Front

Determination of Overall System Performance

▶ **Consideration of the η-γ-Characteristics of the Partial Systems**



$$m_G = \frac{\frac{P_D}{P_R} P_{out}}{\eta_{VSR}\,\eta_{DAB}\,\eta_{Th}} \frac{1}{\gamma_G(\eta_G)}$$

$$m_{VSR} = \frac{\frac{P_D}{P_R} P_{out}}{\eta_{DAB}\,\eta_{Th}} \frac{1}{\gamma_{VSR}(\eta_{VSR})}$$

$$m_{DAB} = \frac{P_{out}/\eta_{Th}}{\gamma_{DAB}(\eta_{DAB})}$$

$$m = m_G + m_{VSR} + m_{DAB}$$

▶ **Overall η-γ-Characteristic**

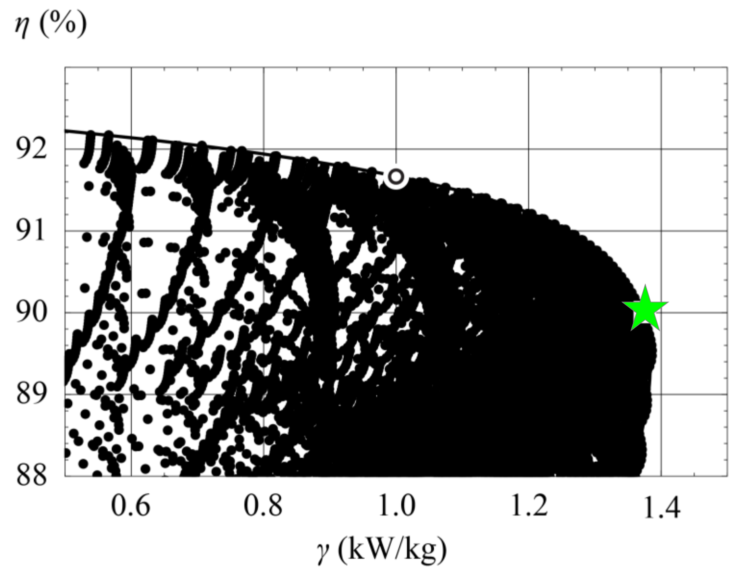
$$\gamma = \frac{P_{out}}{m}$$

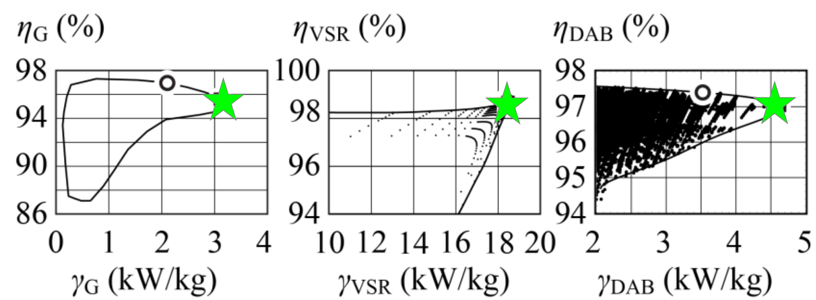
- **Efficiencies of the Partial Systems Need to be Taken into Account**
- **P_D/P_R = Overrating Ratio (8x16kW/100kW)**

Overall System Performance

EFFICIENCIES AND POWER-TO-WEIGHT RATIOS AT THE 2 DESIGN POINTS MARKED IN FIG. 24(A) (CALCULATED FOR NOMINAL OPERATION).

Total system	Generator, VSR, and DAB converter		
$\gamma = 1.37\,\mathrm{kW/kg}$ $\eta = 90.0\%$	Generator:	$\gamma_{\mathrm{G}} = 3.11\,\mathrm{kW/kg}$,	$\eta_{\mathrm{G}} = 95.4\%$
	VSR:	$\gamma_{\mathrm{VSR}} = 18.3\,\mathrm{kW/kg}$,	$\eta_{\mathrm{VSR}} = 98.6\%$
	DAB:	$\gamma_{\mathrm{DAB}} = 4.60\,\mathrm{kW/kg}$,	$\eta_{\mathrm{DAB}} = 97.1\%$
$\gamma = 1.00\,\mathrm{kW/kg}$ $\eta = 91.7\%$	Generator:	$\gamma_{\mathrm{G}} = 2.14\,\mathrm{kW/kg}$,	$\eta_{\mathrm{G}} = 96.9\%$
	VSR:	$\gamma_{\mathrm{VSR}} = 18.3\,\mathrm{kW/kg}$,	$\eta_{\mathrm{VSR}} = 98.6\%$
	DAB:	$\gamma_{\mathrm{DAB}} = 3.53\,\mathrm{kW/kg}$,	$\eta_{\mathrm{DAB}} = 97.4\%$





- **Final Step: System Control Consideration**

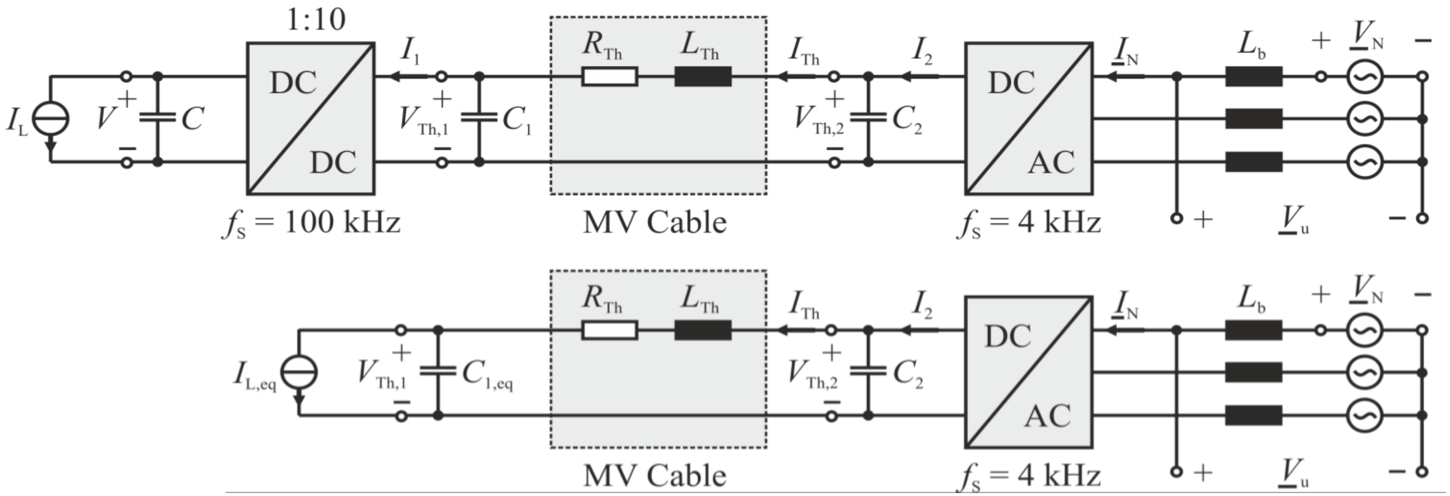
Electric System Control

Stability
Reference Response
Disturbance Response

System Control

- ▶ Control of Flight Trajectory / Max. Energy Generation
- ▶ Generator (Motor) Speed / Torque Control
- ▶ etc.

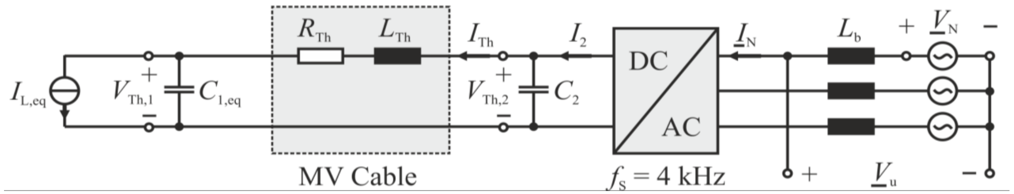
- ▶ Control of DC Voltage Levels is Mandatory !

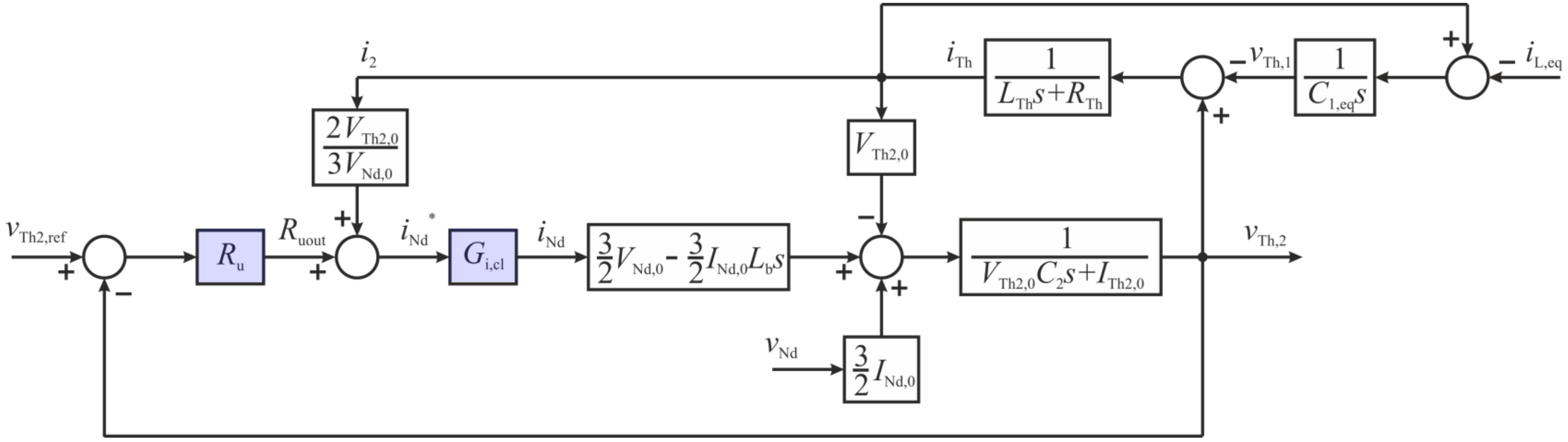


■ Simplified Control-Oriented Block Diagram of the Electric System

Control Block Diagram

- ▶ Ground Station Controls the Tether Voltage
- ▶ Control Objectives: LV DC Bus 650...750V; MV (Tether) < 8kV



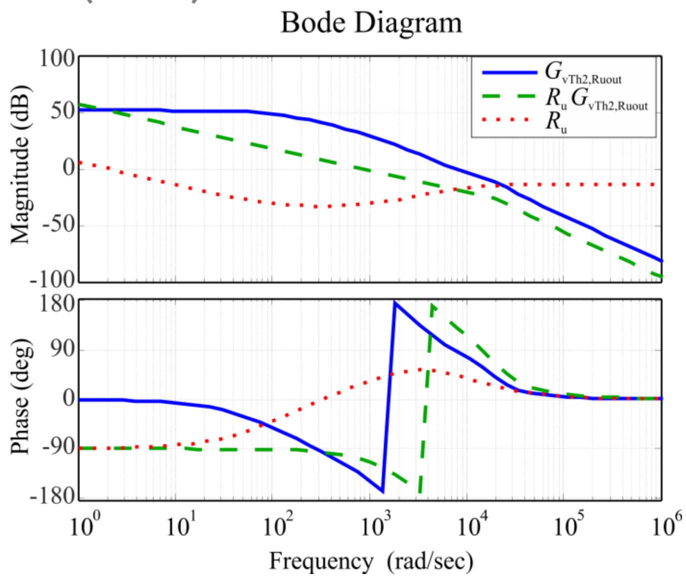


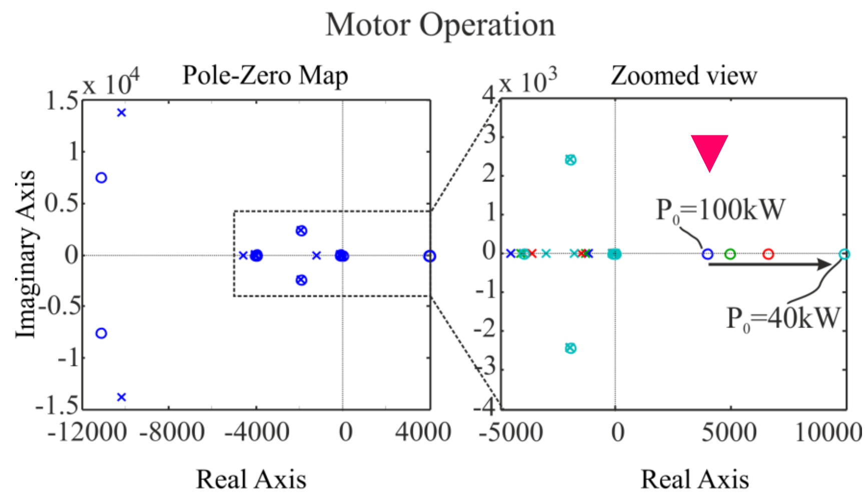
- Only Tether Voltage at Ground Station is Measured (I_{Th} Feedforward)
- Motor AND Generator Operation Must be Considered

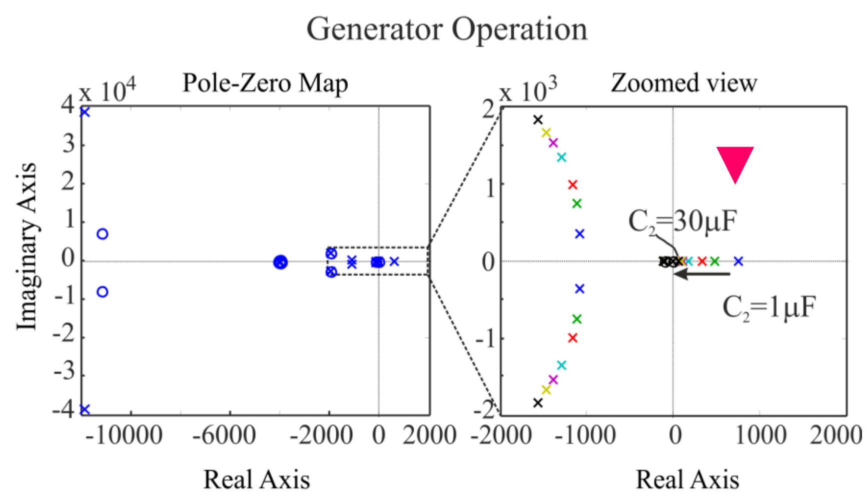
Tether Voltage Control Plant

$$G_{\mathrm{vTh2,Ruout}} = \left.\frac{v_{\mathrm{Th,2}}}{R_{\mathrm{uout}}}\right|_{v_{\mathrm{Nd}}=0,\, i_{\mathrm{L,eq}}=0}$$

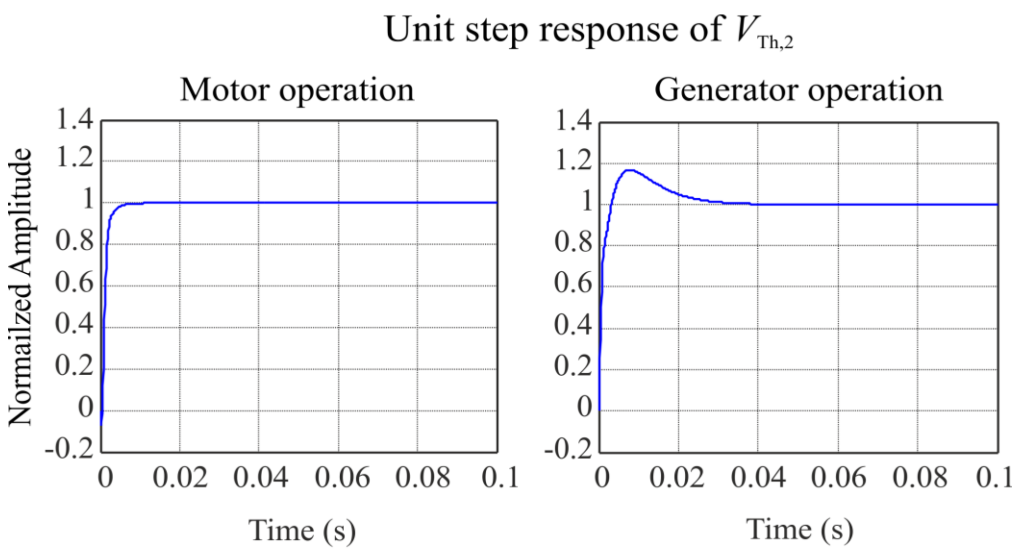
Motor Operation (100kW)





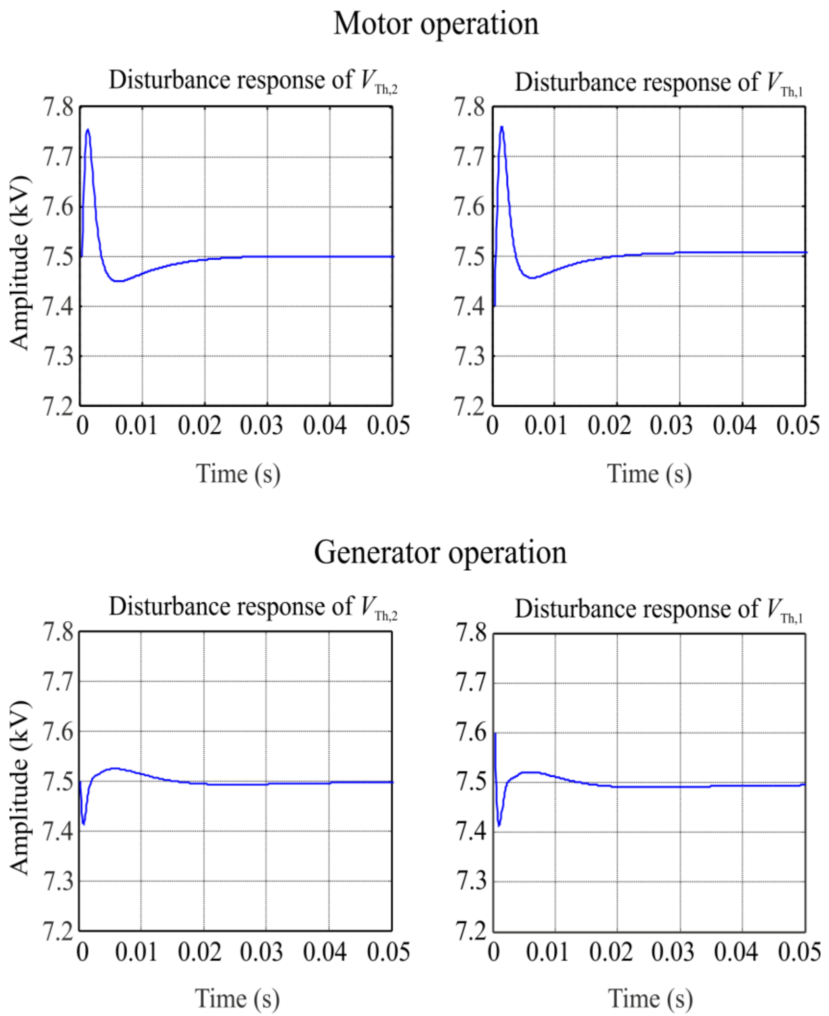


Voltage Control Reference Step Response



- **Overshoot Could be Avoided with Reference Form Filter**

Voltage Control
Disturbance Response



- Motor Operation 100kW → 0
- Gen. Operation —100kW → 0

Conclusions

- AWTs are Basically Technically Feasible
- AWTs Realization Combines Numerous Challenges
  - Aircraft Design
  - MVDC Transmission
  - MV/HF Power Electronics
  - etc.
- AWTs are a Highly Interesting Example for η-γ Trade-off Studies
- AWTs are Examples for Smart Pico Grids or MEA Power System Analysis
- AWTs is a Clear Example of Thinking "Out-of-the-Box" !


thinking
THE BOX

Questions ?