



Solid-State Transformers

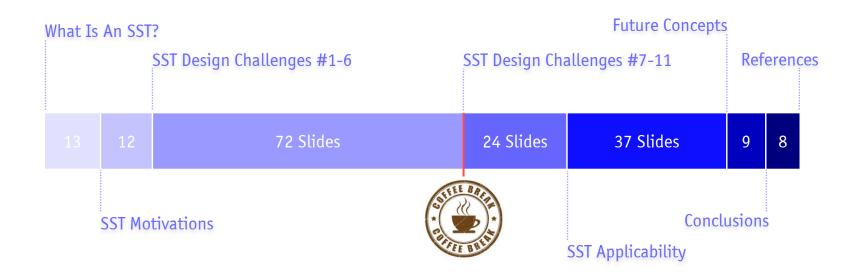
Key Design Challenges, Applicability, and Future Concepts

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Agenda



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ETH Zurich Power Electronic Systems Lab Physikstrasse 3 8092 Zürich Switzerland

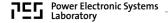


What Is a SST?

Transformer History and Basics *SST Definition*







► Classical Transformer — History (1)

1830	Henry / Far	aday
	_	

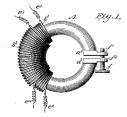
■ 1878 Ganz Company (Hungary)

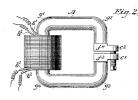
■ 1880 Ferranti

■ 1882 Gaulard & Gibs

■ 1884 Blathy / Zipernowski / Deri

- → Property of Induction
- → Toroidal Transformer (AC Incandescent Syst.)
- → Early Transformer
- → Linear Shape XFMR (1884, 2kV, 40km)
- → Toroidal XFMR (Inverse Type)





W. STANLEY, Jr. INDUCTION COIL.

Patented Sept. 21, 1886.

No. 349,611.







→ Easy Manufact. XFMR (1st Full AC Distr. Syst.)

[Stanley1886]





► Classical Transformer — History (2)



UNITED STATES PATENT OFFICE.

MICHAEL VON DOLIVO-DOBROWOLSKY, OF BERLIN, GERMANY, ASSIGNOR TO THE ALLGEMEINE ELEKTRICITATS-GESELLSCHAFT, OF SAME PLACE.

ELECTRICAL INDUCTION APPARATUS OR TRANSFORMER.

SPECIFICATION forming part of Letters Patent No. 422,746, dated March 4, 1890.

Application filed January 8, 1890. Serial No. 336,290. (No model.)

- 1889 Dobrovolsky → 3-Phase Transformer
- 1891 1st Complete AC System (Gen. + XFMR + Transm. + El. Motor + Lamps, 40Hz, 25kV, 175km)

ELECTRICAL INDUCTION APPARATUS OR TRANSFORMER. Patented Mar. 4, 1890. No. 422,746.

M. VON DOLIVO-DOBROWOLSKY.

[Dobrovolski1890]



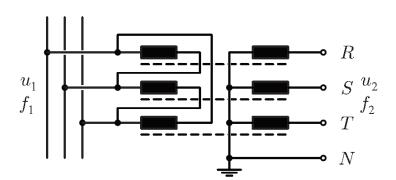


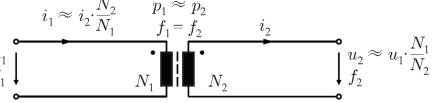
► Classical Transformer — Basics

- Magnetic Core Material
- **■** Winding Material
- Insulation / Cooling
- Operating Frequency
- Operating Voltage

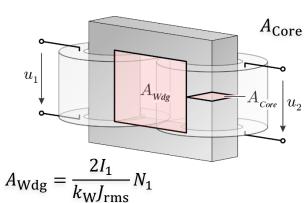
- Silicon Steel / Nanocrystalline / Amorphous / Ferrite
- Copper or Aluminum
- Mineral Oil or Dry-type
- 50/60Hz (El. Grid, Traction) or 16²/₃Hz (Traction)
- 10kV or 20kV (6...35kV)
- 15kV or 20kV (Traction)
- 400V
- **Voltage Transfer Ratio**
- **Current Transfer Ratio**
- Active Power Transfer
- Reactive Power Transfer
- **■** Frequency Ratio

- Fixed
- Fixed
- Fixed $(P_1 \approx P_2)$
- Fixed $(Q_1 \approx Q_2)$
- Fixed $(f_1 = f_2)$
- Magnetic Core $A_{\rm Core} = \frac{1}{\sqrt{2}\pi} \frac{U_1}{\widehat{B}_{\rm max} f} \frac{1}{N_1}$
- Winding Window $A_{\text{Wdg}} = \frac{2I_1}{k_{\text{W}}J_{\text{rms}}}N_1$



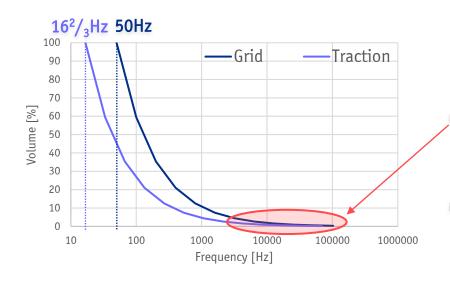


► Transformer Scaling Laws (1)



$$A_{\text{Core}} = \frac{1}{\sqrt{2}\pi} \frac{U_1}{\hat{B}_{\text{max}} f} \frac{1}{N_1}$$

- Area Product: $A_{\text{Core}}A_{\text{Wdg}} = \frac{\sqrt{2}}{\pi} \frac{P_{\text{t}}}{k_{\text{W}}J_{\text{rms}}\hat{B}_{\text{max}}f}$
- Volume: $V \propto (A_{\text{Core}}A_{\text{Wdg}})^{\frac{3}{4}} \propto \frac{1}{f^{3/4}}$



Caution: Too Optimistic!

- Constant Isolation Material Thickness
- Lower Fill Factor (kw) because of Litz Wires
- Gain of Frequency Increase Depends on Grid Frequency



► Transformer Scaling Laws (2)

■ Scaling of Core Losses

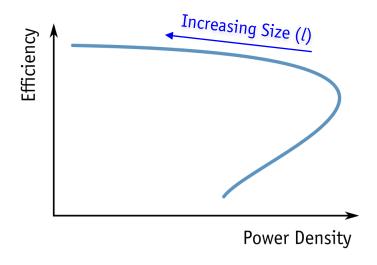
$$P_{\text{Core}} \propto f_{\text{P}} \left(\frac{\Phi}{A}\right)^2 V$$

$$P_{\text{Core}} \propto \left(\frac{1}{l^2}\right)^2 l^3 \propto \frac{1}{l}$$

■ Scaling of Winding Losses

$$P_{\mathrm{Wdg}} \propto I^2 R \propto \frac{I^2 l_{\mathrm{Wdg}}}{\kappa A_{\mathrm{Wdg}}}$$
 $P_{\mathrm{Wdg}} \propto \frac{1}{l}$

$$P_{\mathrm{Wdg}} \propto \frac{1}{l}$$



■ Higher Relative Volumes (Lower kVA/m³) **Allow to Achieve Higher Efficiencies**



► Classical Transformer — Summary (1)

Advantages

- Relatively Inexpensive
- Highly Robust / Reliable
- Highly Efficient (98.5%...99.5% Dep. on Power Rating)
- Short Circuit Current Limitation

■ Weaknesses

- Voltage Drop Under Load
- Losses at No Load
- Sensitivity to Harmonics
- Sensitivity to DC Offset Load Imbalances
- Provides No Overload Protection
- Possible Fire Hazard
- Environmental Concerns
- Low Frequency → Large Weight / Volume







► Classical Transformer — Summary (2)

Advantages

- Relatively Inexpensive
- Highly Robust / Reliable
 Highly Efficient (98.5%...99.5% Dep. on Power Rating)
- Short Circuit Current Limitation













What Is a SST?

Transformer History and Basics **SST Definition**





United States Patent Office

3,517,300

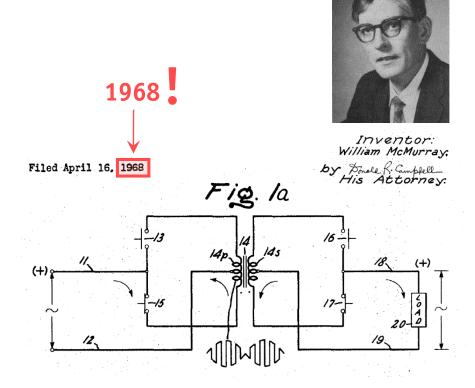
Patented June 23, 1970

1

3,517,300
POWER CONVERTER CIRCUITS HAVING A
HIGH FREQUENCY LINK William McMurray, Schenectady, N.Y., assignor to General Electric Company, a corporation of New York 5 Filed Apr. 16, 1968, Ser. No. 721,817 Int. Cl. H02m 5/16, 5/30 U.S. Cl. 321-60 14 Claims

ABSTRACT OF THE DISCLOSURE

Several single phase solid state power converter circuits have a high frequency transformer link whose windings are connected respectively to the load and to a D-C or low frequency A-C source through inverter configuration switching circuits employing inverse-parallel pairs of controlled turn-off switches (such as transistors or gate turnoff SCR's) as the switching devices. Filter means are connected across the input and output terminals. By synchronously rendering conductive one switching device in each of the primary and secondary side circuits, and alternately rendering conductive another device in each switching circuit, the input potential is converted to a high frequency wave, transformed, and reconstructed at the output terminals. Wide range output voltage control is obtained by phase shifting the turn-on of the switching devices on one side with respect to those on the other side by 0° to 180°, and is used to effect current limiting, current interruption, current regulation, and voltage regulation.



■ Electronic Transformer $(f_1 = f_2)$ ■ AC or DC Voltage Regulation & Current Regulation / Limitation / Interruption

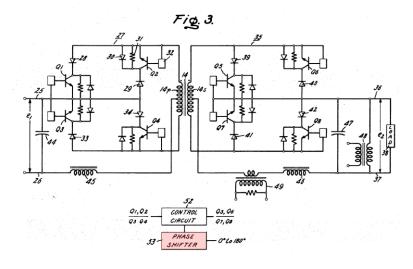
[McMurray1968]





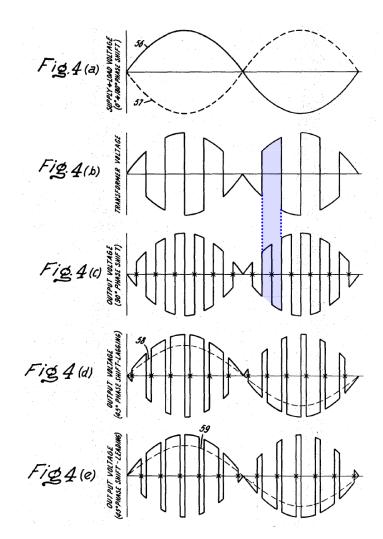
Electronic Transformer

- Inverse-Paralleled Pairs of Turn-off Switches
- 50% Duty Cycle of Input and Output Stage





■ $f_1 = f_2 \rightarrow \text{Not Controllable (!)}$ ■ Voltage Adjustment by Phase Shift Control (!)



[McMurray1968]



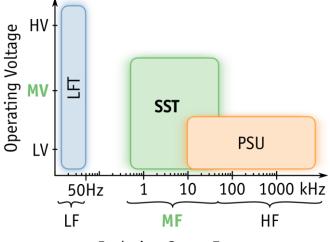
▶ What is a Solid-State Transformer (SST)?

- Power Electronics Interface
- Medium Voltage Connection
- Medium Frequency Isolation Stage
- Communication Link

■ I/O Quantities

- DC/DC
- AC/DC
- AC_{f1}/AC_{f1}
- AC_{f1}/AC_{f2}
- 1ph, 3ph, var. *f*, etc.
- MV/LV, MV/MV

■ Terminology



Isolation Stage Frequency

McMurrayElectronic Transformer (1968)BrooksSolid-State Transformer (SST, 1980)EPRIIntelligent Universal Transformer (IUT)ABBPower Electronics Transformer (PET)BorojevicEnergy Control Center (ECC)WangEnergy Router

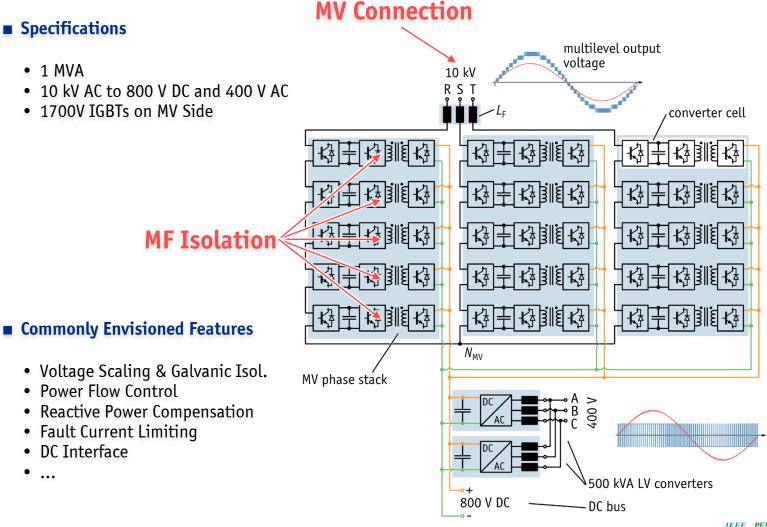
etc.

[Brooks1980]





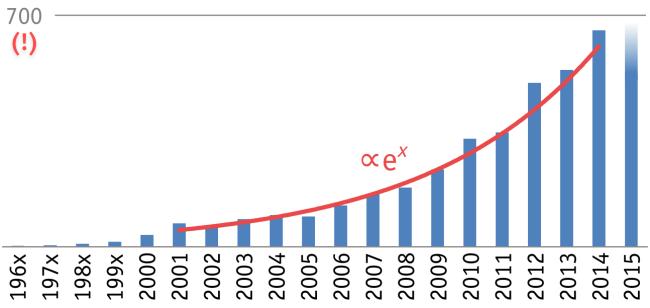
► Example SST System: ETH *MEGAlink* SST Concept





► The Solid-State Transformer Hype

■ Evolution of # of SST Publications Per Year:



Google Scholar Hits for Query: ("solid-state transformer") OR ("electronic transformer") OR ("Intelligent Universal Transformer") OR ("Power Electronic Transformer") OR ("Power Electronics Transformer")

- How To Keep An Overview?
 - Identify Origin and Evolution of Key Concepts
 - Narrow Down Feasible Solutions by Identifying Core Requirements, e.g., Modularity





SST Concept Motivations

Traction → **Weight & Volume** Smart Grid → Controllability DC-DC Conversion





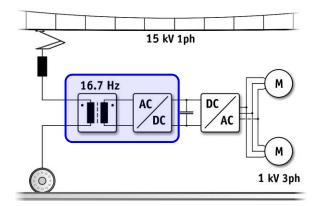
► Classical Locomotives (1)

■ Catenary Voltage 15kV or 25kV

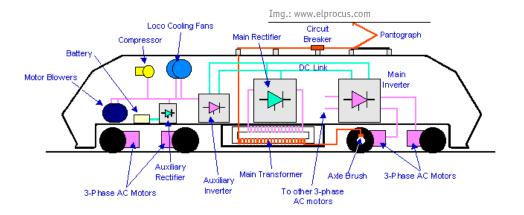
■ Frequency $16^2/_3$ or 50Hz ■ Power Level 1...10MW typ.

■ Isolated **AC/DC** Conversion (!)

■ Volume & Weight Constraints









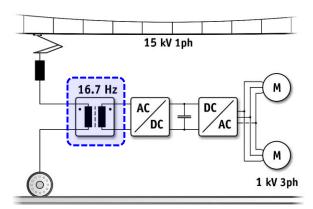


► Classical Locomotives (2)

■ Catenary Voltage 15kV or 25kV

■ Frequency $16^2/_3$ or 50Hz ■ Power Level 1...10MW typ.

- Isolated **AC/DC** Conversion (!)
- Volume & Weight Constraints



■ Traction Transformer
$$A_{\text{Core}}A_{\text{Wdg}} = \frac{\sqrt{2}}{\pi} \frac{P_{\text{t}}}{k_{\text{W}}J_{\text{rms}}\hat{B}_{\text{max}}f}$$



\rightarrow Volume/Weight Reduction By Increasing J_{rms}

Efficiency 90...95% (99% Typ. for Distr. Transf.)
Current Density 6 A/mm² (2A/mm² Typ. for Distr. Transf.)

Power Density 2...4 kg/kVA





▶ Next Generation Traction Systems

■ It's Getting Tougher!

- Distributed Propulsion
- Low-Floor Vehicles
- High-Speed Trains
- Impr. Energy Efficiency
- → Volume Constraints
- → Weight Constraints
- → Weight Constraints
- → Loss Constraints

(Space for Add. Seats)

(Roof Mounting)

(Higher Power at Same Max. Axle Load Limit)

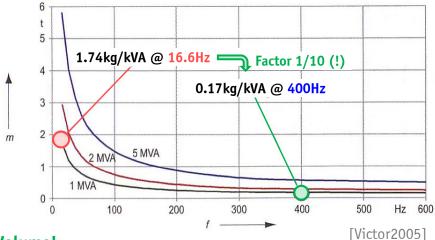
(No Further Increase of J_{rms} , etc.)

■ What Degrees of Freedom Are Left?

$$A_{\text{Core}}A_{\text{Wdg}} = \frac{\sqrt{2}}{\pi} \frac{P_{\text{t}}}{k_{\text{W}}J_{\text{rms}}\hat{B}_{\text{max}}f}$$

$$V \propto \left(A_{\text{Core}}A_{\text{Wdg}}\right)^{\frac{3}{4}} \propto \frac{1}{f^{3/4}}$$





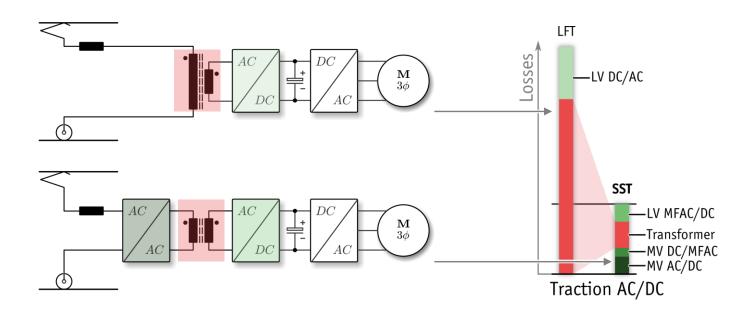
→ Frequency as DOF to Reduce Weight & Volume!

[Hazeltine1923]



▶ Next Generation Locomotives

■ Loss Distribution of Conventional & Next Generation Locomotives



■ Medium Freq. Provides Degree of Freedom → Allows Loss Reduction AND Volume Reduction





SST Concept Motivations

Traction → Weight & Volume

Smart Grid → Controllability

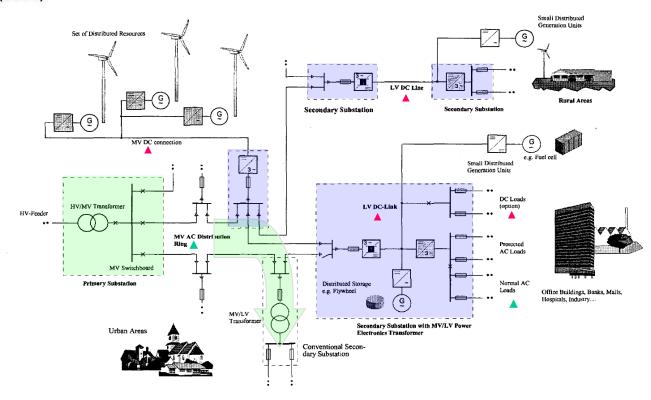
DC-DC Conversion





► Advanced (High Power Quality) Grid Concept

■ Heinemann (2001)



- MV AC Distribution with DC Subsystems (LV and MV) and Large Number of Distributed Resources
- MF AC/AC Conv. with DC Link Coupled to **Energy Storage** provide High Power Qual. for Spec. Customers

[Heinemann2001]



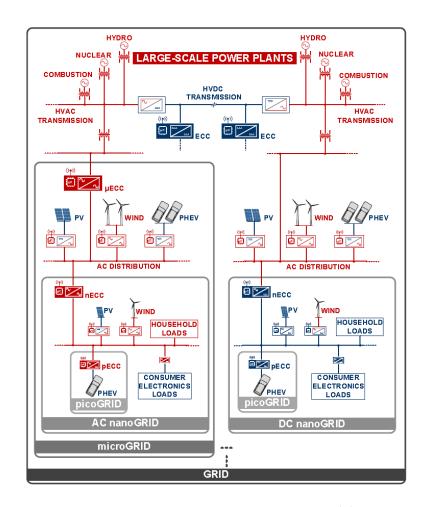


► Smart Grid Concept

- Boroyevich (2010)
- Hierarchically Interconnected Hybrid Mix of AC and DC Sub-Grids
 - Distr. Syst. of Contr. Conv. Interfaces
 - Source / Load / Power Distrib. Conv.
 - Picogrid-Nanogid-Microgrid-Grid Structure
 - Subgrid Seen as Single Electr. Load/Source
 - ECCs provide Dyn. Decoupling
 - Subgrid Dispatchable by Grid Utility Operator
 - Integr. of Ren. Energy Sources

■ ECC = Energy Control Center

- Energy Routers
- Continuous Bidir, Power Flow Control
- Enable Hierarchical Distr. Grid Control
- Load / Source / Data Aggregation
- Up- and Downstream Communic.
- Intentional / Unintentional Islanding for Up- or Downstream Protection
- etc.



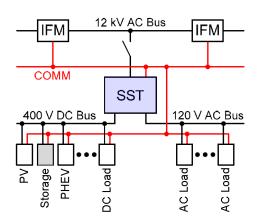
[Boroyevich2010]

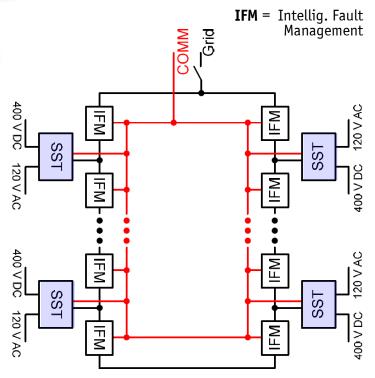




► <u>Future Ren. Electric Energy Delivery & Management (FREEDM) System</u>

- Huang et al. (2008)
- SST as Enabling Technology for the "Energy Internet"
 - Integr. of DER (Distr. Energy Res.)
 - Integr. of DES (Distr. E-Storage) + Intellig. Loads
 - Enables Distrib. Intellig. through COMM
 - Ensure Stability & Opt. Operation





• Bidirectional Flow of Power & Information / High Bandw. Comm. → Distrib. / Local Autonom. Ctrl.

[Huang2009, Huang2011], Figs.: [Falcones2010]





► SST Functionalities

■ Protects Load from Power System Disturbance

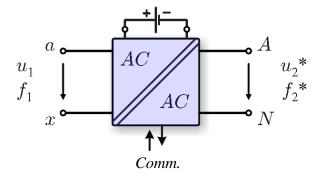
- Voltage Harmonics / Sag Compensation
- Outage Compensation
- Load Voltage Regulation (Load Transients, Harmonics)

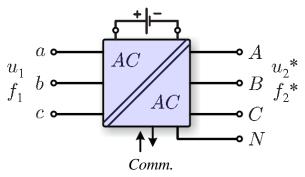
■ Protects Power System from Load Disturbance

- Unity Inp. Power Factor Under Reactive Load
- Sinus. Inp. Curr. for Distorted / Non-Lin. Load
- Symmetrizes Load to the Mains
- Protection against Overload & Output Short Circ.

■ Further Characteristics

- Operates on Distribution Voltage Level (MV-LV)
- Integrates Energy Storage (Energy Buffer)
- DC Port for DER Connection
- Medium Frequency Isolation → Low Weight / Volume
- Definable Output Frequency (1-ph. AC, 3-ph. AC, DC)
- High Efficiency
- No Fire Hazard / Contamination
- Supervisory Control / Status Monitoring Interface

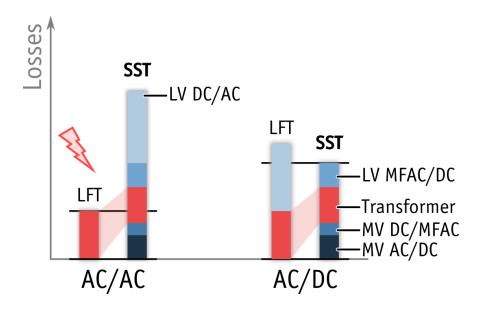








► "Efficiency Challenge" (Qualitative)



■ SSTs in Grid Applications – A Skeptic's View

- Efficiency of LFT for AC/AC Very Hard To Attain
- Weight/Volume Typically Not an Issue In Stationary Grid Applications
- Robustness, Reliability?
- Cost?





SST Concept Motivations

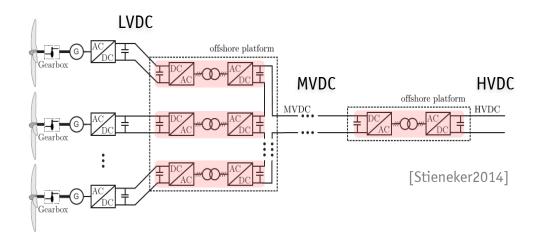
Traction → Weight & Volume Smart Grid → Controllability

DC-DC Conversion





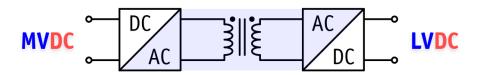
► Isolated DC-DC Applications



■ Examples

- In-Building DC Microgrids
- DC Collection Grids (Wind, PV)
- Future DC Grids in General

- DC Systems With Galvanic Separation Requirements → Isolated DC-DC Conversion = SST!
- Not Limited to MV Connection (Overlap With PSUs)



■ Transformer Operating Frequency Can Be Freely Chosen!





11 Key Challenges of SST Design

- 1. Handling of Medium Voltage
- 2. Topology Selection
- 3. Reliability
- 4. MF Isolated Power Converters
- 5. MF Transformer Design
- 6. Isolation Coordination
- 7. *EMI*
- 8. Protection
- 9. Control
- 10. Construction of Modular Conv.
- 11. Testing of MV Converters





Challenge #1/11 Handling of Medium Voltage

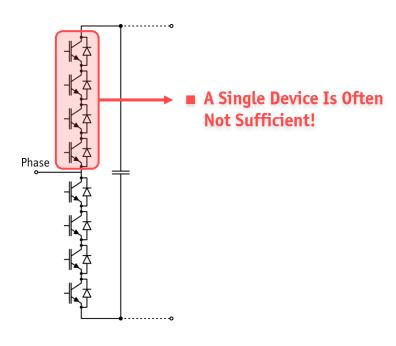
Multi-Cell Approaches
Optimum Blocking Voltage
Single-Cell Approaches
Outlook

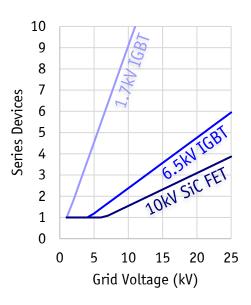




► Interfacing Medium Voltage With Power Electronics

- Limited Blocking Voltages of Available Semiconductors
 - **6.5kV** for Si IGBTs
 - 10-15kV for SiC FETs (Prototype Devices Only)
- Feasible Blocking Voltage Utilization: Only 50-70% (Cosmic Ray Induced Failures)





Mod. Index.: 0.8

Blocking Voltage Utilization: 0.66





United States Patent

[11] 3,581,212

[54] FAST RESPONSE STEPPED-WAVE SWITCHING POWER CONVERTER CIRCUIT

[72] Inventor William McMurray

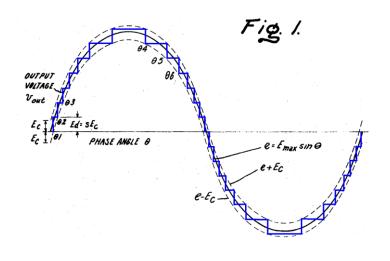
Schenectady, N.Y.
[21] Appl. No. 846,354
[22] Filed 1969

[22] Filed July 31, 1969 (45] Patented May 25, 1971

[45] Patented May 25, 1971 [73] Assignee General Electric Company Inventor: William McMurray, by Finale & Compfell— His Attorney.



- 24n 25n 12n 18n 220n 14n 23n 15n 22n 11n 23n 22n 15n 22n 11n 23n 22n 15n 22n 1
- Cascading of Converter Cells
- Multilevel Output Voltage



[McMurray1969]



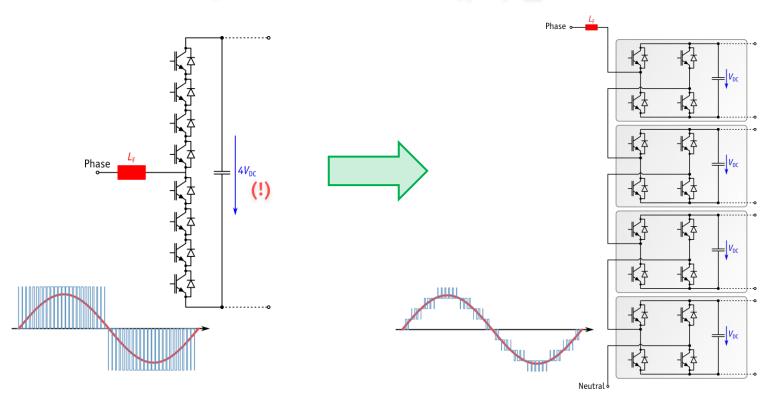


► Cascaded Converter Cells Instead of Direct Series Connection

- Direct Series Connection is Suboptimal
 - Voltage Sharing (Static and Dynamic)
 - Switching Synchronization
 - No Add. Benefit of Multiple Switches

■ Added Value: Multiple Converter *Cells*

- Modularity, Redundancy
- Multilevel Output Voltage Waveform
 - $\rightarrow f_{\rm S} \propto 1/N_{\rm Cell}^2$ for Same Filter Inductor







Challenge #1/11 Handling of Medium Voltage

Multi-Cell Approaches **Optimum Blocking Voltage**Single-Cell Approaches

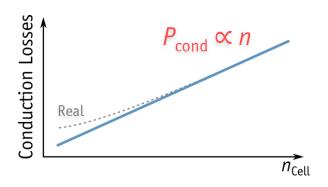
Outlook

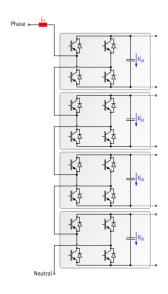




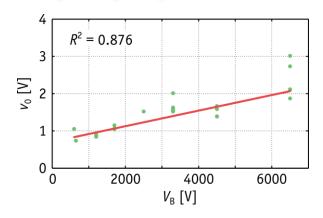
▶ Basic Trade-Offs: Conduction Losses

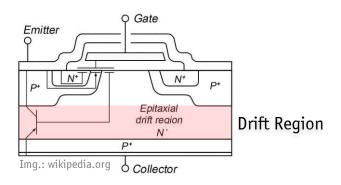
■ More Cells, More Series Voltage Drops (IGBTs):





Reality: Voltage Drop Increases with Blocking Voltage Due to Larger Drift Region









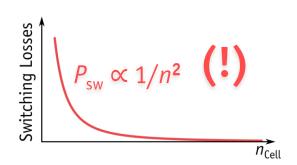
▶ Basic Trade-Offs: Switching Losses

- For Equal Current Ripple in Equal Filter Inductors
 - Switching Frequency (per Cell):
 - Cell DC Voltage:
 - But: Number of Cells:

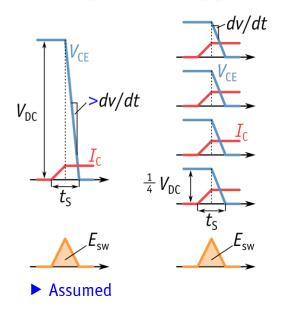
$$f_{\rm S} \propto 1/n^2$$

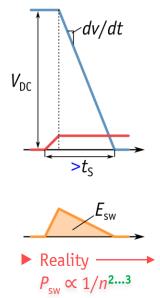
$$V_{\rm DC} \propto 1/n$$

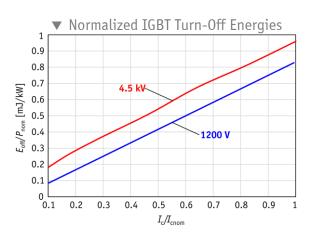
$$\propto n$$



■ Switching Loss Modeling (Qualitative)





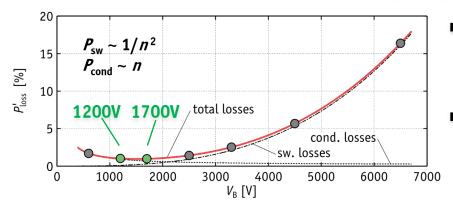






► Loss-Optimal Blocking Voltage Choice

- For Equal Current Ripple in Equal Filter Inductors
 - 10kV Grid Voltage There *Is* an Optimum Blocking Voltage

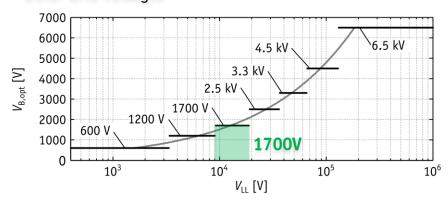


■ Optimum Blocking Voltage



■ Optimum Number of Cascaded Cells

• Other Grid Voltages

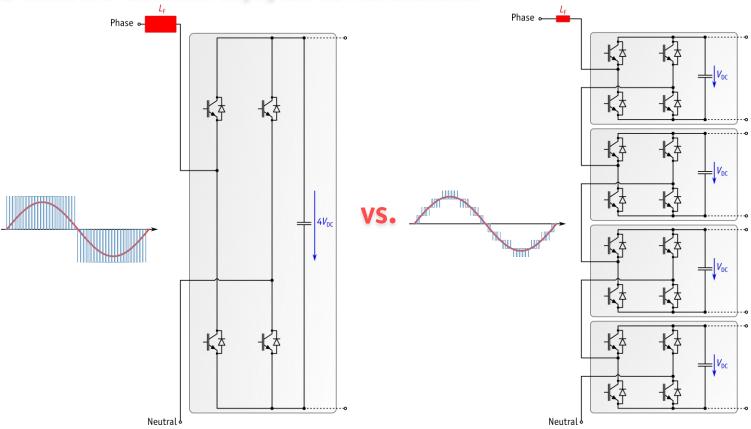






▶ Optimal (Efficiency & Power Density!) Blocking Voltage (1)

■ Volume as 2nd Dimension: Varying Also the Filter Inductance!



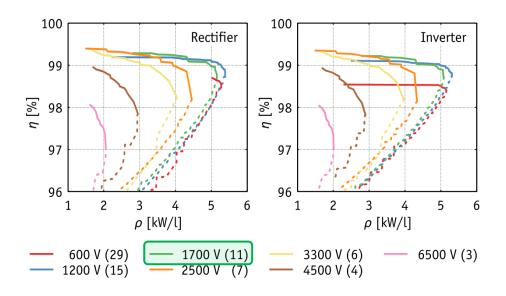
■ Modeling of Component Losses and Volumes (Inductor, Heatsinks, Capacitors, IGBTs, etc.)





▶ Optimal (Efficiency & Power Density!) Blocking Voltage (2)

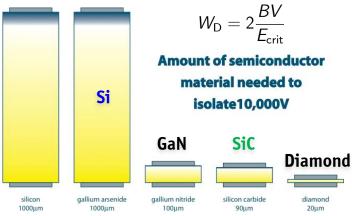
- Volume as 2nd Dimension: Varying Also the Filter Inductance!
 - Component Losses and Volumes (Inductor, Heatsinks, Capacitors, IGBTs, etc.)



■ Caution: Minimum Filter Inductance Might be Defined By Application-Dependent Protection Considerations



► Enter Silicon Carbide: Si vs. WBG (SiC/GaN) Semiconductors

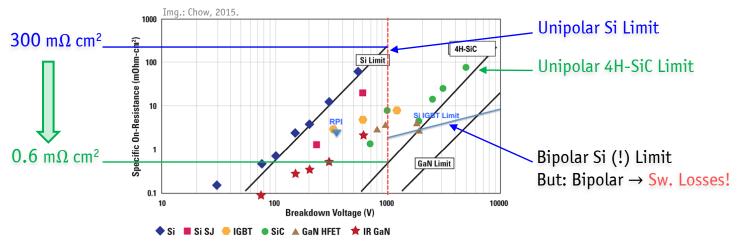


Imq.: http://www.evincetechnology.com/whydiamond.html

■ Specific On-State Resistance

$$R_{
m on,sp} = rac{4BV^2}{\epsilon \mu_{
m n} E_{
m C}^3} rac{
m Blocking \, Voltage}{
m Critical \, Electric \, Field}$$

- E_{C} in SiC ca. 9x Larger Than in Si
- Lower R_{on,sp} For Given Blocking Voltage







► Example: All-SiC Traction Inverter

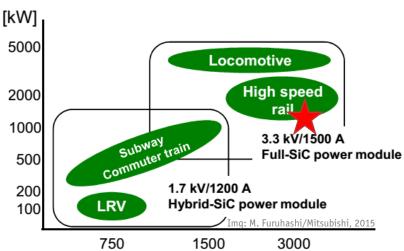
- Mitsubishi All-SiC Traction Inverter (2014)
 - 3.3kV/1.5kA SiC Modules in All-SiC Traction Inverter



- 65% Reduction of Size and Weight
- 55% Loss Reduction







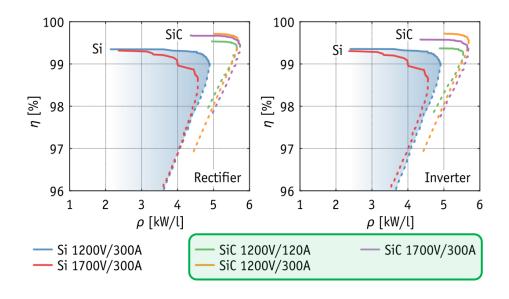
Rated voltage for power device [V]





▶ Optimal (Efficiency & Power Density!) Blocking Voltage with SiC

■ 1200V and 1700V SiC FET Power Modules for Comparison



Wolfspeed 1200V/5mΩ ▼



- Caution: Minimum Filter Inductance Might be Defined By Application-Dependent Protection Considerations
- Si IGBT → SiC Transition Yields Significant Benefits!

Further Reading: ETH / [Huber2016b]





Challenge #1/11 Handling of Medium Voltage

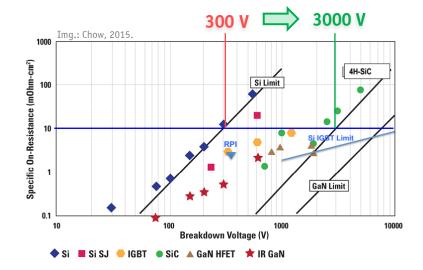
Multi-Cell Approaches
Optimum Blocking Voltage
Single-Cell Approaches
Outlook





► Enter HV SiC Power Semiconductors

- $E_{\rm C}$ in SiC ca. 9x Larger Than in Si
- Lower $R_{on,sp}$ For Given Blocking Voltage
- **or:** Higher Blocking Voltage for Given $R_{on,sp}$



■ 10...15kV Prototype Devices Are Available



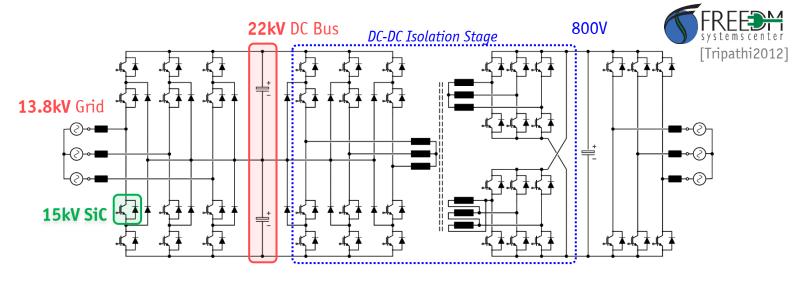
■ Challenging HV Packaging



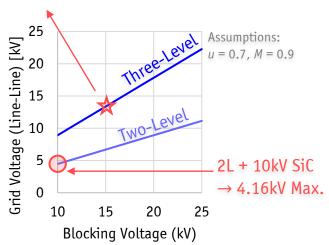




► Single-Cell Approach: The Positive Aspects



- Standard Inverter Topologies Can Be Employed (Two-Level, Three-Level)
- **■** Comparably Low System Complexity
- Three-Phase Inverter Stage
 → Constant Power Flow In Isolation Stage (!)

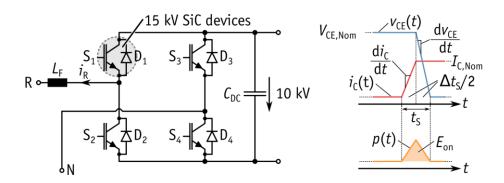




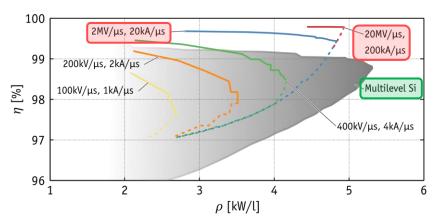


► Single-Cell Approach: The Challenging Aspects

- Low Number of Levels \rightarrow Remember: $f_{\varsigma} \propto 1/n^2$
- High Switching Frequency and/or Large Filter Inductor



- "Virtual" Devices By Adapting t_S (and thus di/dt and dv/dt)
- Pareto Optimization for Two-Level, Single-Phase (!) System



Very Fast Switching Transitions Required

- High $dv/dt \rightarrow CM$ Disturbances
- High $di/dt \rightarrow 0$ vervoltages

Further Reading: ETH / [Huber2016b]

■ Implementation of Redundancy?





Challenge #1/11 Handling of Medium Voltage

Multi-Cell Approaches
Optimum Blocking Voltage
Single-Cell Approaches
Outlook





▶ Outlook: Single-Cell vs. Multi-Cell

■ Strategies for Handling Medium Voltage Connection

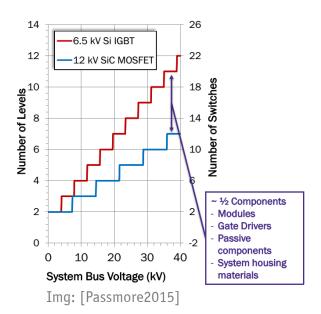
- Multi-Cell Approach
- LV Devices, Multilevel Waveforms, Redundancy, "Divide et Impera"
- Complexity, Phase-Modular Topologies
- Single-Cell Approach
- Simplification of Converter Structure, Three-Phase Topologies
- Max. Grid Volt. Limited, 2L/3L w. Fast Switching Trans.

■ The Best of Both Worlds?

• FEWER-Cells Approach

Higher DC Voltage per Cell Less Cells, Lower Complexity Multilevel Waveforms Redundancy

- Suitable Choice Depends on Application Voltage and Power Levels
- Careful Choice/Optimization of Blocking Voltage for Multi-Cell Systems







Challenge #2/11 Topology Selection

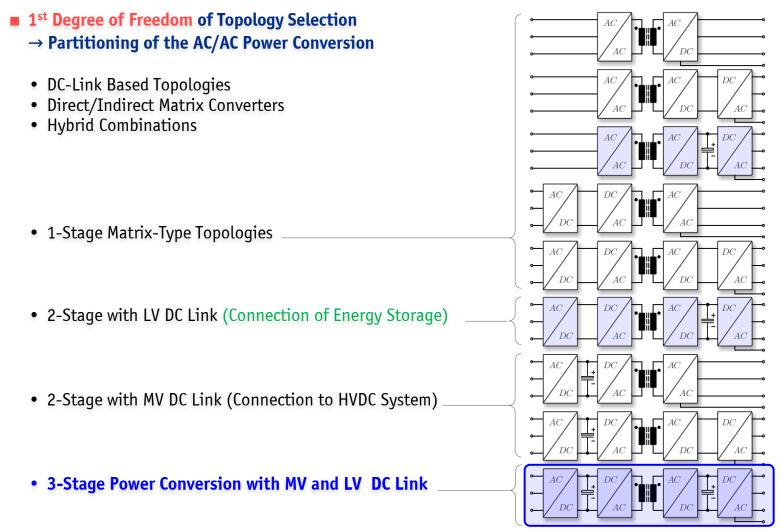
Partitioning of AC/AC Power Conv.
Partial or Full Phase Modularity
Classification of SST Topologies

Conclusion: Main SST Topologies





► Partitioning of the AC/AC Power Conversion





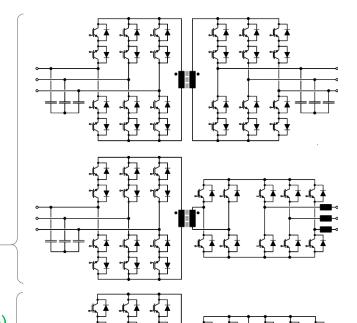


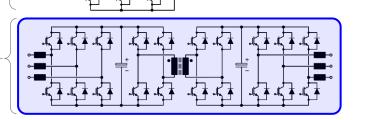
▶ Partitioning of the AC/AC Power Conversion

- 1st Degree of Freedom of Topology Selection
 - → Partitioning of the AC/AC Power Conversion
 - DC-Link Based Topologies
 - Direct/Indirect Matrix Converters
 - Hybrid Combinations

- 1-Stage Matrix-Type Topologies
- 2-Stage with LV DC Link (Connection of Energy Storage)

- 3-Stage Power Conversion with MV and LV DC Link
 - → Requires HV Devices (!)









Challenge #2/11 Topology Selection

Partitioning of AC/AC Power Conv.

Partial or Full Phase Modularity

Classification of SST Topologies

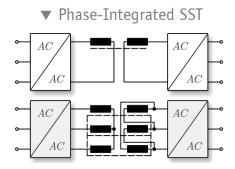
Conclusion: Main SST Topologies

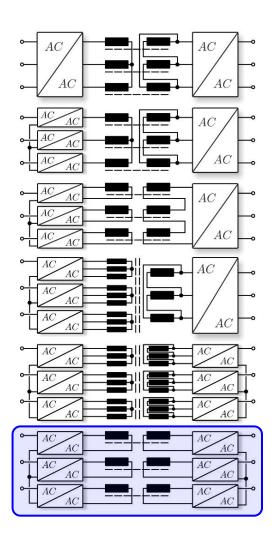




▶ Partial or Full Phase Modularity

- 2nd Degree of Freedom of Topology Selection
 - → Partial or Full Phase Modularity
 - Phase-Modularity of **Electric** Circuit
 - Phase-Modularity of Magnetic Circuit



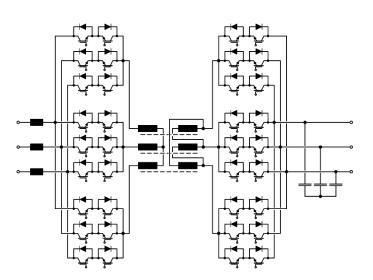






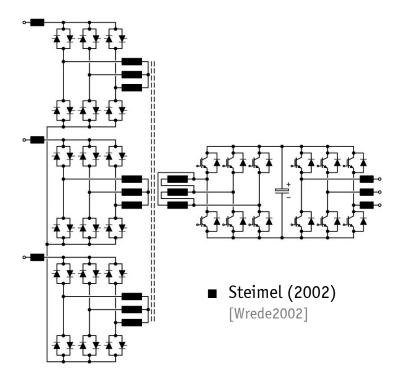
▶ Partial or Full Phase Modularity: Examples

- 2nd Degree of Freedom of Topology Selection
 - → Partial or Full Phase Modularity
 - Example of Three-Phase Integrated (Matrix) Converter & Magn. Phase-Modular Transf.



■ Enjeti (1997)
[Kang1999]

• Example of Partly Phase-Modular SST



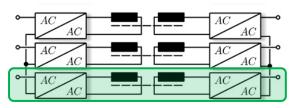




▶ Partitioning of Single-Phase AC/DC PFC Functionality

■ Required Functionality

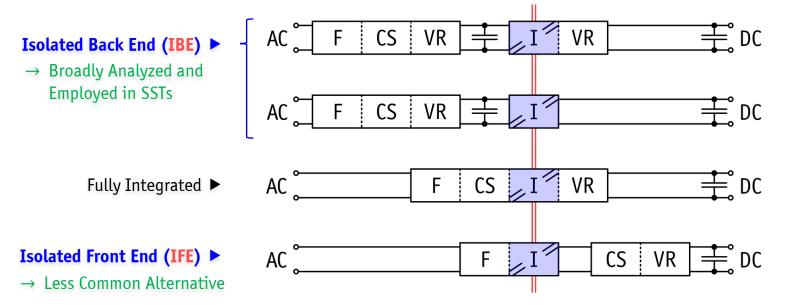
- F: Folding of the AC Voltage Into a | AC | Voltage
- CS: Input Current Shaping
- I: Galvanic Isolation & Voltage Scaling
- VR: Output Voltage Regulation



One Phase of Phase-Modular 3ph-SST

→ Single-Phase System!

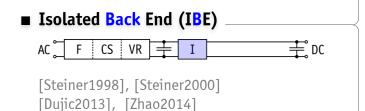
■ Isolated PFC Task Partitioning Variants

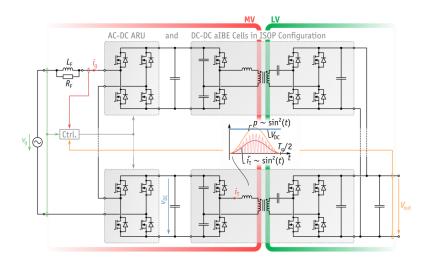




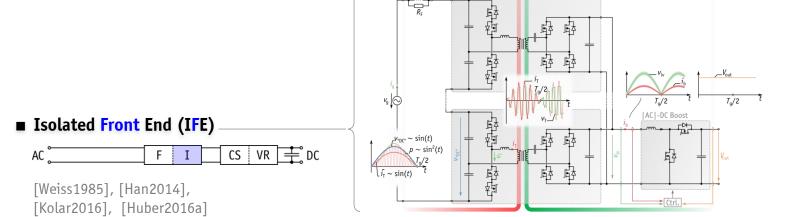


► Examples of Multi-Cell AC/DC SST Topologies





AC-|AC| aIFE Cells in ISOP Configuration







Challenge #2/11 Topology Selection

Partitioning of AC/AC Power Conv. Partial or Full Phase Modularity

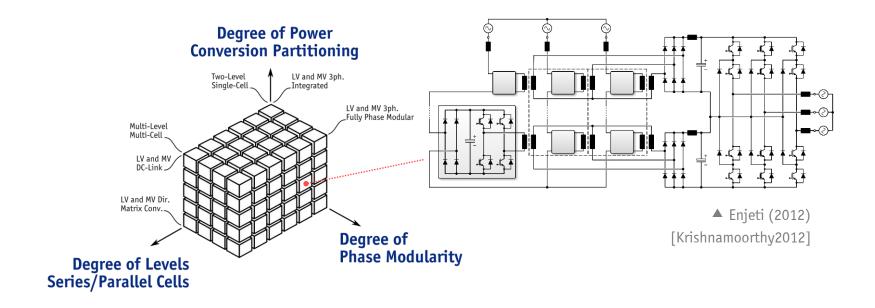
Classification of SST Topologies

Conclusion: Main SST Topologies





► Classification of SST Topologies



■ Very (!) Large Number of Possible Topologies

- Partitioning of Power Conversion
- Splitting of 3ph. System into Individual Phases
- Splitting of Medium Voltage into Lower Partial Voltages

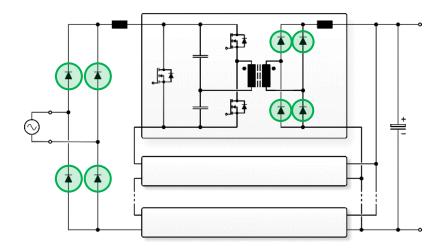
- → Matrix & DC-Link Topologies
- → Phase Modularity
- → Multi-Level/Cell Approaches





► Side Note: Unidirectional SSTs

- Simplification of Topologies for Unidirectional Power Flow
- SST As MV-Connected Power Supply



Example Topology:Unidirectional Multi-CellBoost Topology

■ Example Applications

- Direct Supply of 400V/48V DC System from 6.6kV AC
- Direct PV Energy Regeneration from 1kV DC into 6.6kV AC

[VanDerMerwe2009a] [VanDerMerwe2009b] ETH / [Rothmund2014]





Challenge #2/11 Topology Selection

Partitioning of AC/AC Power Conv. Partial or Full Phase Modularity Classification of SST Topologies

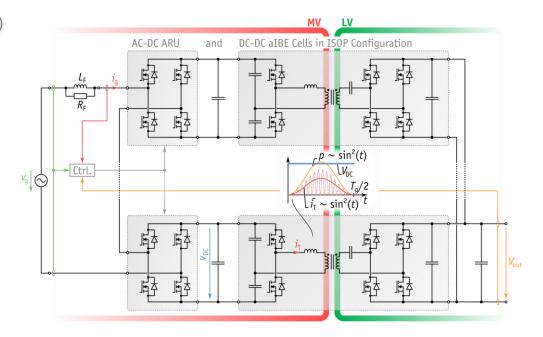
Conclusion: Main SST Topologies





► Main SST Topologies (1)

- Multi-Cell Topologies
 - Isolated Back End
 - Isolated Front End
 - Matrix-Type (AC/AC)
 - Modular-Multi-Level (M2LC)
- Single-Cell Topologies



■ Note: Specific Realizations May Vary (e.g., 3-Phase Configurations, AC/AC Conversion, NPC Cells, DC-DC Converter Type, Unidirectionality, etc.)

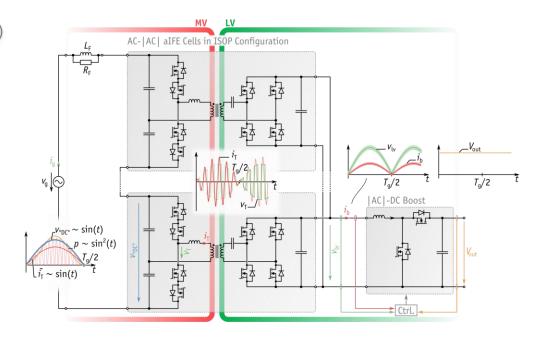
[Steiner1998] [Steiner2000] [Dujic2013] [Zhao2014]





► Main SST Topologies (2)

- Multi-Cell Topologies
 - Isolated Back End
 - Isolated Front End
 - Matrix-Type (AC/AC)
 - Modular-Multi-Level (M2LC)
- Single-Cell Topologies



■ Note: Specific Realizations May Vary (e.g., 3-Phase Configurations, AC/AC Conversion, NPC Cells, Unidirectionality, etc.)

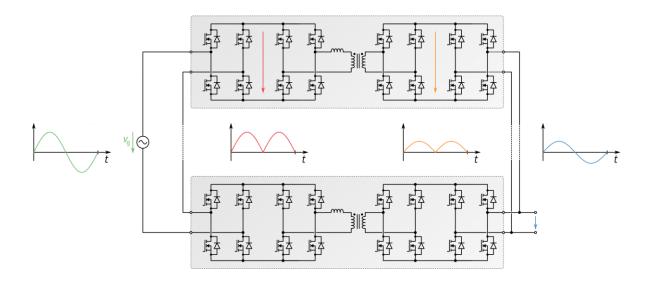
[Weiss1985] [Han2014] [Kolar2016] [Huber2016a]





► Main SST Topologies (3)

- Multi-Cell Topologies
 - Isolated Back End
 - Isolated Front End
 - Matrix-Type (AC/AC)
 - Modular-Multi-Level (M2LC)
- Single-Cell Topologies



■ Note: Specific Realizations May Vary (e.g., 3-Phase Configurations, NPC Cells, Unidirectionality, etc.)

[Das2011]

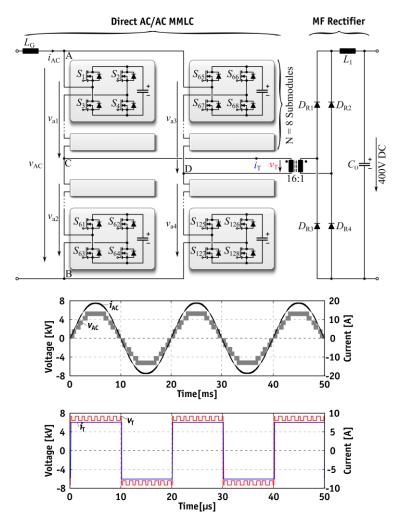




► Main SST Topologies (4)

- Multi-Cell Topologies
 - Isolated Back End
 - Isolated Front End
 - Matrix-Type (AC/AC)
 - Modular-Multi-Level (M2LC)
- Single-Cell Topologies

■ Note: Specific Realizations May Vary (e.g., 3-Phase Configurations, AC/AC Conversion, Bidirectionality, etc.)



[Glinka2003], Img.: ETH / [Rothmund2014]



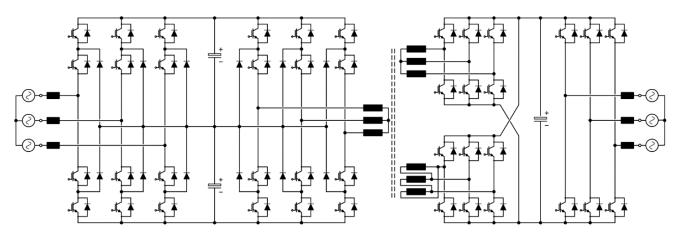


► Main SST Topologies (5)

- Multi-Cell Topologies
 - Isolated Back End
 - Isolated Front End
 - Matrix-Type (AC/AC)
 - Modular-Multi-Level (M2LC)

■ Single-Cell Topologies





■ Note: Specific Realizations May Vary (e.g., DC-DC Converter Type, Unidirectionality, etc.)

[Tripathi2012]

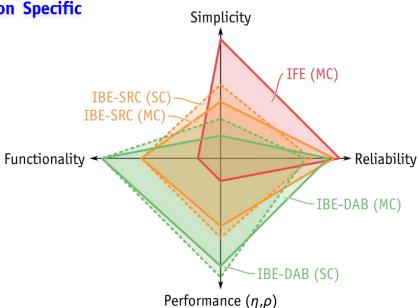




► SST Topologies Summary & Outlook

■ High Number of Possible SST Topologies

→ Optimum Topology Choice Depends on Specific Application Requirements!



■ Trends And Outlook

- LV SiC Devices
- HV SiC Devices / Single-Stage SSTs
- Reliability Considerations Are Highly Important





Challenge #3/11 Reliability

Basics of Reliability Modeling Cell-Level Redundancy "Reliability Bottlenecks"

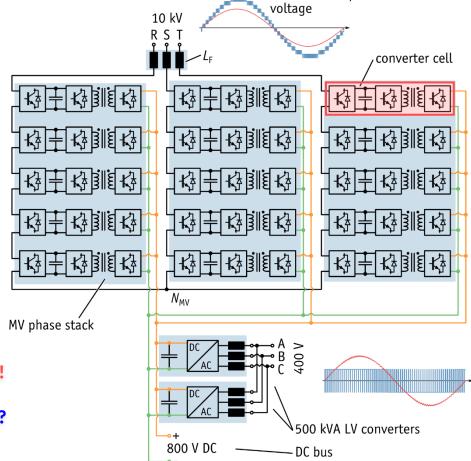




► Example System: ETH *MEGAlink* Distribution SST

Specifications

- 1 MVA
- 10 kV AC to 800 V DC and 400 V AC
- 1700V IGBTs on MV Side



multilevel output

- Modular System → MANY Components!
 - → Can Such a System Still Be Reliable?





► Reliability Considerations for SST Design

■ Remember:

Conventional Transformers are Highly Reliable and Robust

Copper, Iron and Oil

VS.

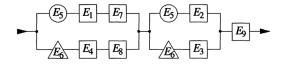
 High # of Semiconductors, Gate Drives, Measurement and Control Electronics, Cooling Systems, ... (!)



Source: http://www.africancrisis.org

■ Very High Reliability Requirements for Grid and Traction Equipment

■ Include Reliability Considerations Early in the SST Design Process



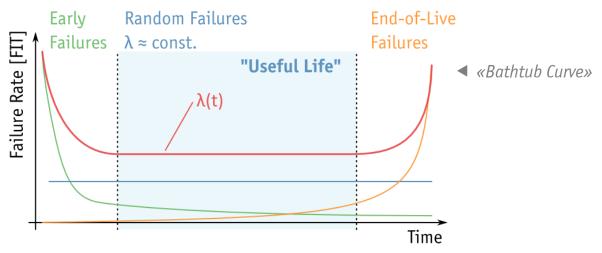
Textbook: [Birolini1997]

- Reliability Block Diagrams
- Design for Reliability Approach [Wang2013]
- Etc.

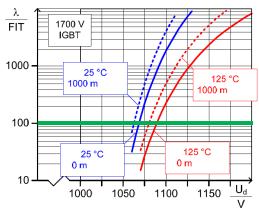




► Modeling Reliability: The Failure Rate



- In General, the Failure Rate $\lambda(t)$ is a Function of Time
- Here, Only Useful Life is Considered
 - Dominated by Random Failure Distribution
 - Constant Failure Rate λ
 - $[\lambda] = 1$ FIT (1 Fail. in 10⁹ h) Typ. Value for an IGBT Mod.: 100 FIT \triangleright
- **Example Sources for Empirical Component Failure Rate Data**
 - MIL-HDBK-217F, "Reliability Prediction of Electronic Equipment," 1995
 - IEC Standard 62380:2004(E), "Reliability Data Handbook," IEC, 2004.
 - Stds. Define Base Failure Rates for Comp. and Factors to Account for Stress Levels (e.g., Temperature)





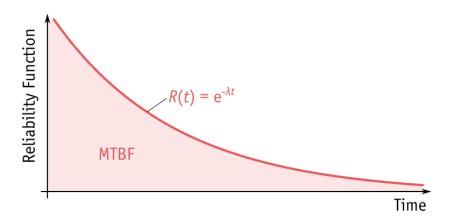


► Modeling Reliability: The Reliability Function

- **■** Expresses **Probability of System Being Operational After** *t* **Hours**
- General Definition:

$$R(t) = e^{-\int_0^t \lambda(x) dx}$$

■ During Useful Life: $\lambda(t) = \text{const.} = \lambda$:



■ Mean Time Between Failures

$$extit{MTBF} = \int_0^\infty R(t) dt = \int_0^\infty \mathsf{e}^{-\lambda t} dt = rac{1}{\lambda}$$

Caution: MTBF is Not the Time Before Which No Failure Occurs – It's All Statistics!

■ Average Availability:

$$A = \frac{MTBF}{MTBF + MTTR}$$

Textbook: [Birolini1997]



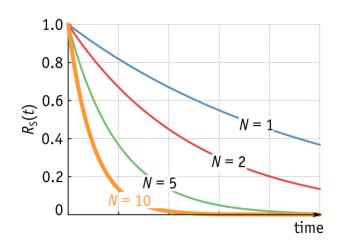


► Modeling Reliability: Basic Multi-Element Considerations

■ Series Structure

(e.g. Components of a Single Converter Cell)

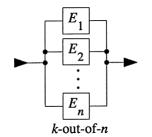
(General Assumption: Independent Elements with Equal Failure Rate.)

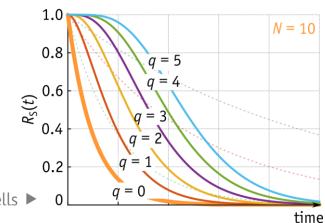


■ k-out-of-n Redundancy

(e.g., Redundancy of Cells in a Phase Stack)

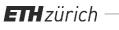
 System is Operational as Long as At Least k out of n Subsystems (Cells) Are Operational





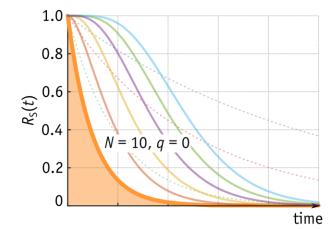
Effect of *q* Additional Redundant Cells ▶

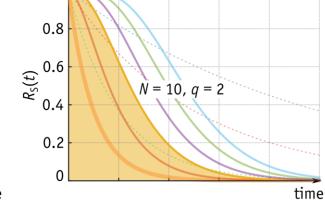
Textbook: [Birolini1997]





► The "Power of Redundancy" (1)



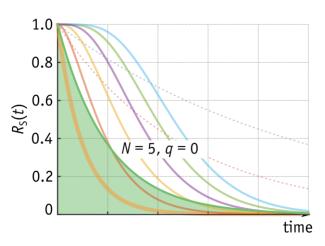


1.0

- Remember: $MTBF = \int_0^\infty R(t)dt$
 - Area Below Reliability Function!



• 10 Elements + 2 Redundant: Reliability Higher than for 5 Elements!



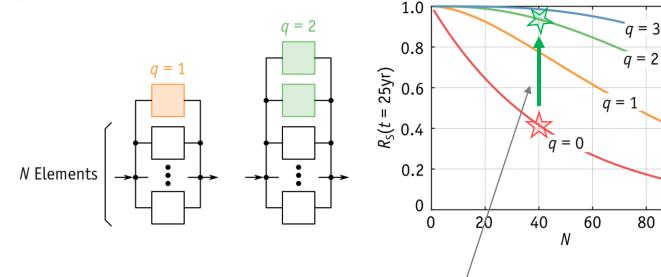


► The "Power of Redundancy" (2)

■ Value of Reliability Function at t = 25 Years

(Probability That System Is Operational After 25 Years)

- N Elements
- q Additional Redundant Elements



- Redundancy Can Significantly Improve System Level Reliability
 - E.g., for N = 40: from 40% to > 90% with 2 Additional Redundant Cells

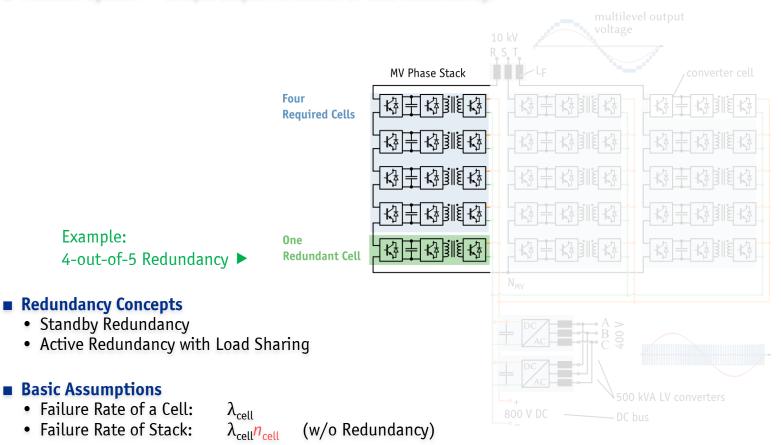




100

► Example System: Cell Redundancy

■ Modular System → Simple Implementation of Cell Redundancy!

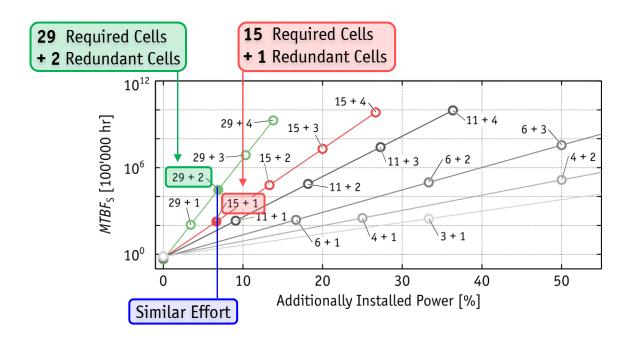






► Example System: Cell Redundancy and Reparability

- Reparability: Faulty Cell Can Be Replaced On-Site; Possibly Even In a Hot-Swap Operation
 - Example: Mean Time To Repair (MTTR) of One Week Assumed



- Multi-Cell Designs Can Be Made Highly Reliable By Adding Redundancy!
- Preventive Maintenance Can Further Improve System Availability

Note 1: 50% Of Cell FIT Rate Is Assumed To Be Proportional To Blocking Voltage **Note 2:** Absolute MTBFS Values Depend on FIT Rate Assumptions; Relative Results Stay The Same

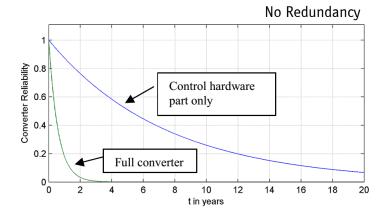
Further Reading: ETH / [Huber2016b]





► Reliability "Bottlenecks"

- Reliability Improvement by Means of Cell-Level Redundancy Is
 - Very Effective

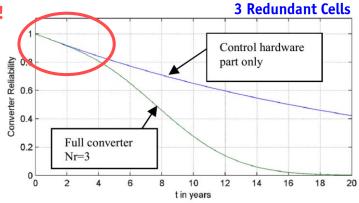


Control Hardware Becomes Limiting Factor!

 But Limited by Other Parts of the Converter System

- Control
- Auxiliary Supplies
- Communication
- Bypass Devices

- ...



[Grinberg2013]

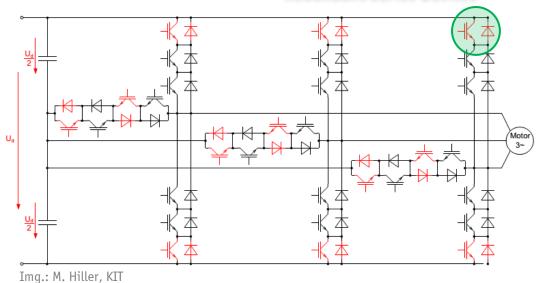




▶ Redundancy In Single-Cell Systems

■ Example: MV Motor Drive

Redundant Series Devices





▲ Press-Pack NPC Phase Module (Converteam GmbH)







- **Fail-To-Short Behavior Required!**
- Only Feasible With IGBT Press Pack Modules

[Hiller2016]





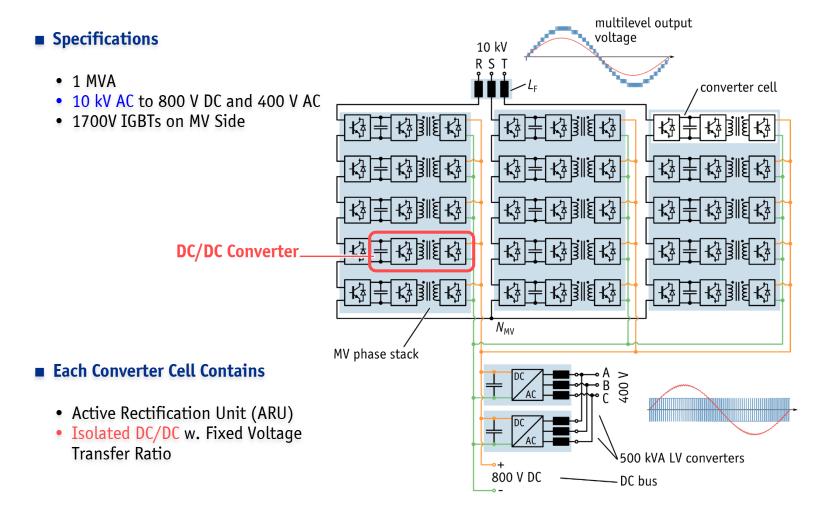
Challenge #4/11 MF Isolated Power Converters

Dual Active Bridge HC-DCM Series Resonant Converter





► Example System: ETH *MEGAlink* Distribution SST



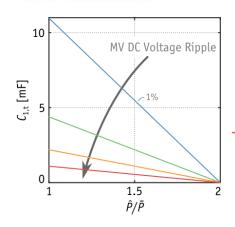


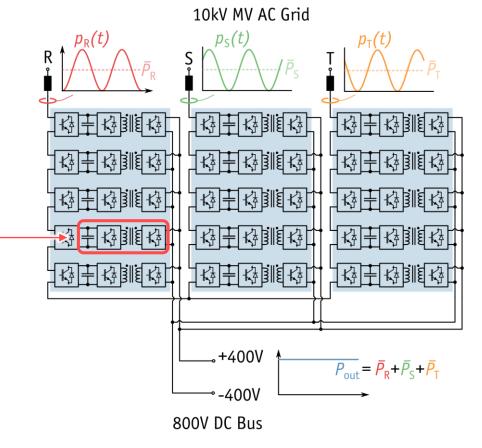


▶ Power Flows in Phase-Modular Solid-State Transformers

■ MV: 100 Hz Power Fluctuation in Single-Phase Systems

■ DC/DC Converter Power Flow How To Handle The Single-Phase Power Fluctuation?





■ LV: Constant Power Behavior of Three-Phase Systems





Challenge #4/11 MF Isolated Power Converters

Dual Active Bridge

HC-DCM Series Resonant Converter





1991

United States Patent [19]

[11] Patent Number:

5,027,264

DeDoncker et al.

[45] Date of Patent:

Jun. 25, 1991

[54] POWER CONVERSION APPARATUS FOR DC/DC CONVERSION USING DUAL ACTIVE BRIDGES

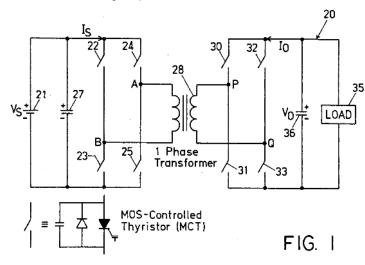
[75] Inventors: Rik W. DeDoncker, Niskayuna, N.Y.;

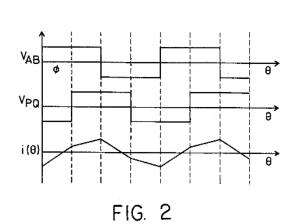
Mustansir H. Kheraluwala; Deepakraj M. Divan, both of

Madison, Wis.

[22] Filed:

Sep. 29, 1989





- Soft Switching in a Certain Load Range
- Power Flow Control by Phase Shift between Primary & Secondary Voltage

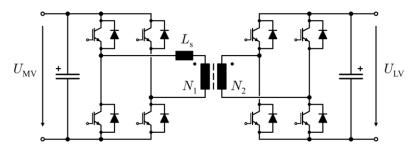
[DeDoncker1989]





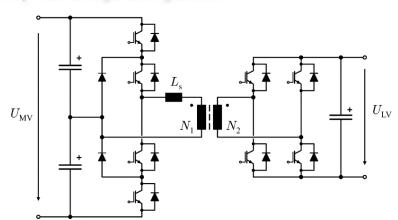
► Common Bridge Configurations

■ Full-Bridge



• Three Voltage Levels on Each Side

■ NPC / Full-Bridge Configuration



• Suitable for Higher MV/LV Ratios

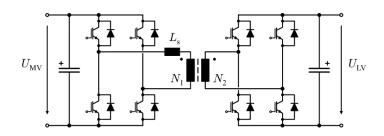
Other Configurations Possible (Half-Bridge / Half-Bridge, etc.)

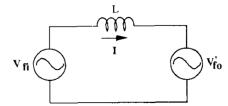




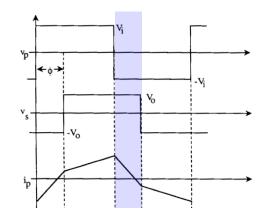
► Phase-Shift Modulation (1)

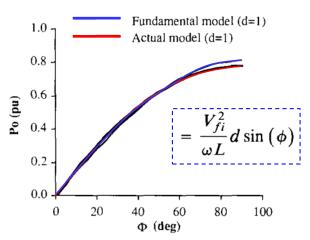
■ Power Transfer Controlled Through Phase Shift Between MV and LV Bridges





Fundamental model of the dual bridge dc/dc converter.





Comparison of the output power versus ϕ , at d = 1, from the fundamental model and actual model.

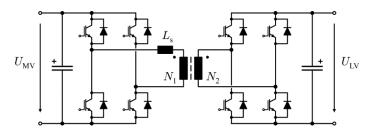
[DeDoncker1989]





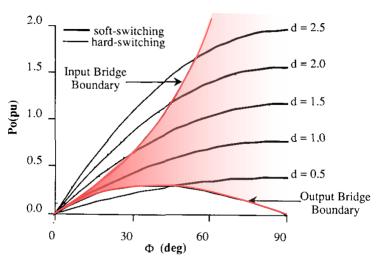
► Phase-Shift Modulation (2)

■ All Switching Transitions done in **ZVS** Conditions (within a Certain Operating **Range**)



v_{p} v_{q} v_{q

▶ Soft Switching Range

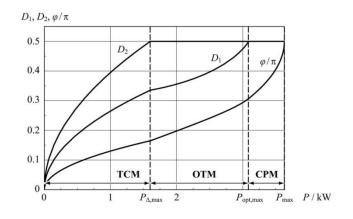


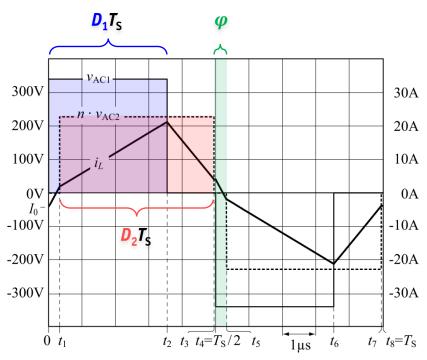




▶ Phase-Shift / Duty Cycle Modulation

- Additional Degrees of Freedom Can Be Utilized for Optimization
- For Example: Minimization of the RMS Currents through the Transformer





Not Possible in Half-Bridge Configurations (No Zero Voltage Intervals)

[Krismer2012]

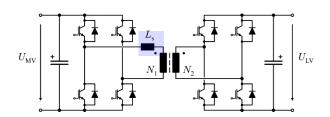


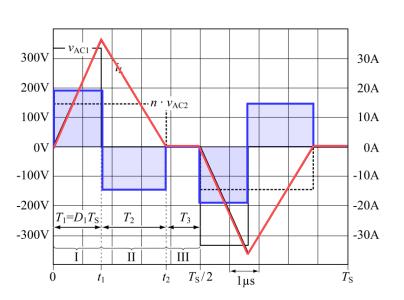


► Triangular Current Modulation

■ Duty Cycles and Phase Shift Utilized to Perform **Zero Current Switching (ZCS)**

► HV IGBT Switching Loss Reduction





ZCS on **ZCS on MV ZVS** on **MV Side** and LV Sides LV Side 300V 30A 200V 20A 100V 10A 0V0A-100V -10A -200V -20A $T_1 = D_1 T_S$ T_2 -300V -30A ĬÌ III

 $T_{\rm S}/2$

► ZCS on MV Side (!)





Challenge #4/11 MF Isolated Power Converters

Dual Active Bridge

HC-DCM Series Resonant Converter

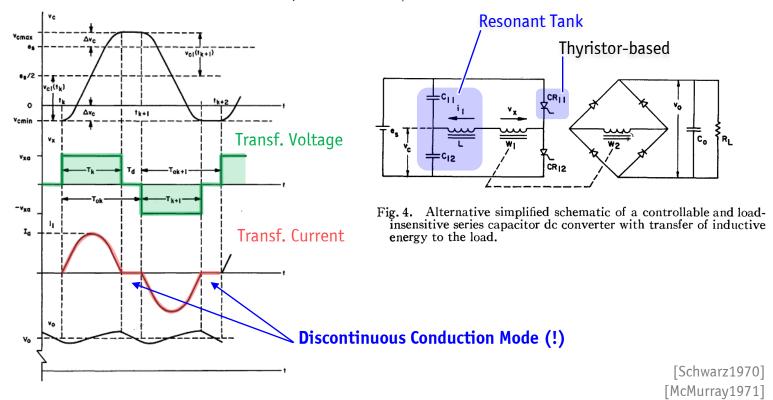




IEEE TRANSACTIONS ON INDUSTRIAL ELECTRONICS AND CONTROL INSTRUMENTATION VOL. IECI-17, NO. 3, MAY 1970 (!)

A Method of Resonant Current Pulse Modulation for Power Converters

FRANCIS C. SCHWARZ, SENIOR MEMBER, IEEE

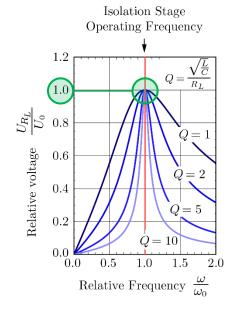




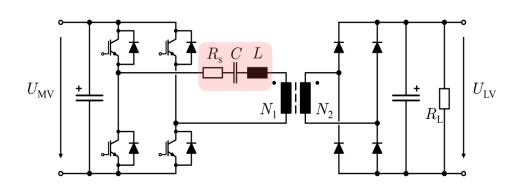


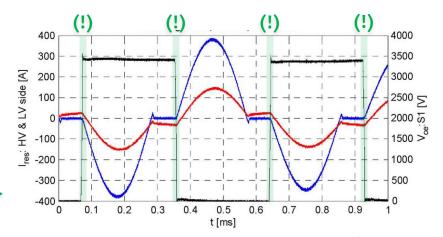
► <u>Half-Cycle Discont.-Cond.-Mode Series-Res.-Conv.</u> (HC-DCM SRC)

■ Operating Principle: Resonance Frequency ≈ Switching Frequency → Unity Gain



■ The Input/Output Voltage Ratio is Close to Unity, Independent of Power Transfer





ZCS of All Devices ▶

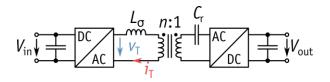


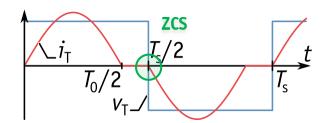




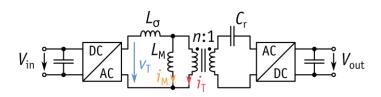
► HC-DCM SRC Switching Transitions

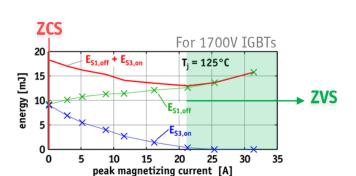
■ Zero Current Switching (ZCS) For All Transitions

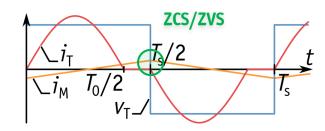




■ Load-Independent Zero Voltage Switching (ZVS)
Using The Magnetizing Current







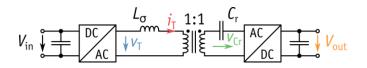
- Loss Optimization With Magnetizing Current and Interlock Time
- Example: 1700V IGBT

Further Reading: ETH / [Huber2013a] ETH / [Ortiz2013a]





HC-DCM SRC: "DC Transformer" Behavior



Source Bridge → Actively Switched Only
 Sink Bridge → Passive Operation (Diodes)

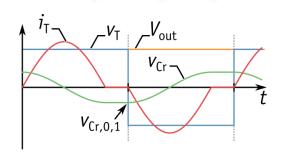
- **Ideal** (Lossless Components)
 - \rightarrow Steady State: $V_{\text{out}} = V_{\text{in}}$
- Real
 - \rightarrow Steady State: $V_{\text{out}} \approx V_{\text{in}}$ (Deviation Due to Losses)
 - → Tight Coupling of DC Input and Output Voltages

- ► Acts as "DC Transformer" with **Certain Dynamics!**
- ► No Control Possible/Required!

■ Steady State 1 $\hat{\imath}_{T,1} = \frac{\hat{v}_{\text{Cr,0,1}}}{Z_0}$

$$V_{\text{out}} = V_{\text{in}}^{Z_0}$$

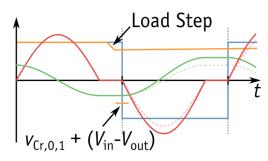
$$V_{\rm out} = V_{\rm in}$$



■ Disturbance

$$V_{\rm out} \neq V_{\rm in}$$

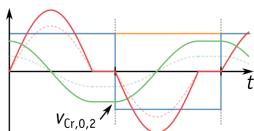
→ Add. Excit. Volt.



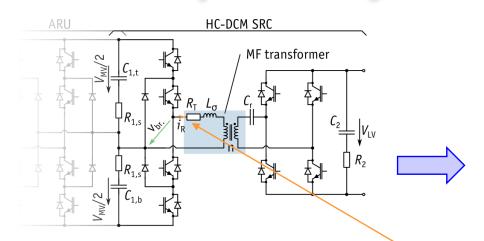
■ Steady State 2

$$\hat{\imath}_{T,\mathbf{2}} = \frac{\hat{v}_{\text{Cr},0,\mathbf{2}}}{Z_0}$$

$$V_{\rm out} = V_{\rm in}^{Z_0}$$

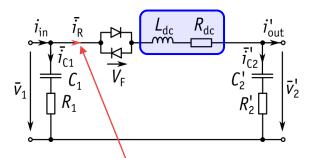


► HC-DCM SRC Dynamic Modeling of Terminal Behavior



■ Dynamic Equivalent Circuit

- Modeling of Terminal Behavior
- Based on Local Average Current, in



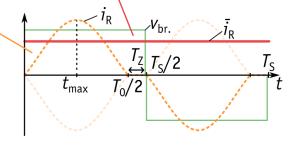
■ How to Choose Eq. Circ. Element Values?

• **R**_{dc} (Equal RMS Losses):

$$\vec{i}_R^2 R_{dc} \stackrel{!}{=} \vec{i}_R^2 R_{total} \quad \Rightarrow R_{dc} = \frac{\vec{i}_R^2}{\vec{i}_R^2} R_{total} = \beta^2 R_{total}$$

• **L**_{dc} (Equal Stored Energy):

$$\vec{i}_{R}^{2}L_{dc} \stackrel{!}{=} \hat{i}_{R}^{2}L_{\sigma} \quad \Rightarrow \quad L_{dc} = \frac{\hat{i}_{R}^{2}}{\hat{i}_{R}^{2}}L_{\sigma} = \alpha^{2}L_{\sigma}$$



• For Piecewise Sinusoidal Current:

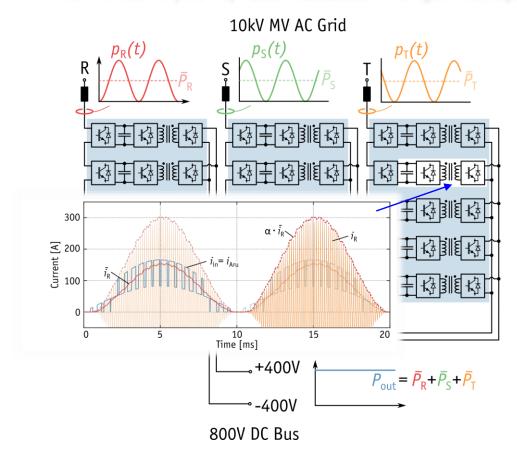
$$\alpha = \frac{\pi}{2} \cdot \frac{f_0}{f_s} \qquad \beta^2 = \frac{\pi^2}{8} \cdot \frac{f_0}{f_s}$$

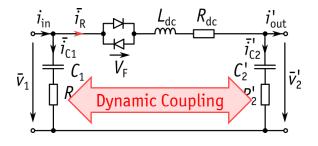
Further Reading: [Esser1991], [Steiner2000], ETH / [Huber2015]



► Again: Power Flows in Phase-Modular SSTs

■ MV: 100 Hz (120 Hz) Power Fluctuation in Single-Phase Systems





■ HC-DCM SRC Dynamics

• MV DC Volt.: 100 Hz Fluct.

• LV DC Volt.: Constant

→ Transmission of Full Single-Phase Power Fluctuation!

- Higher RMS Current (23%) in Transformer and DC-DC Switches
- Appropriate Dimensioning

■ LV: Constant Power Behavior of Three-Phase Systems

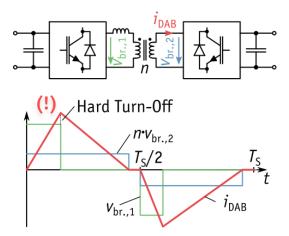
Further Reading: ETH / [Huber2015]





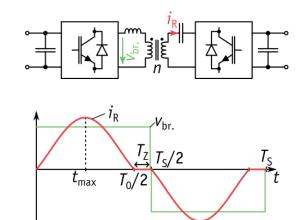
► Realization Options for DC/DC Converters in SST Cells

Dual Active Bridge (DAB)



- Can (Must!) Be Fully Controlled
 - Arbitrary Choice in Losses ← Capacitor Volume Trade-Off
 - Potentially Lower RMS Currents

■ Half-Cycle Discont.-Conduction-Mode SRC (HC-DCM SRC)



- Does Not Have To (Can Not!) Be Controlled (!)
 - Reduces Complexity in Multi-Cell Systems
 - · Ensures MV Side Voltage Balancing
- ► Predominant Solution in Multi-Cell SSTs!







Challenge #5/11 MF Transformer Design

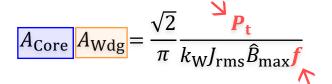
Transformer Types Litz Wire Issues

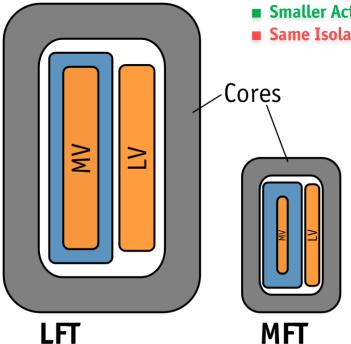




▶ General Challenge of MF Transformers

- Higher Operating Frequency
- Lower Unit Power Rating







Same Isolation Voltage (!)

MV Winding Cooling Through Isolators

■ Solid Isolators → Bad Thermal Conductors

Prim.

Core

Sec. Iso. Prim.

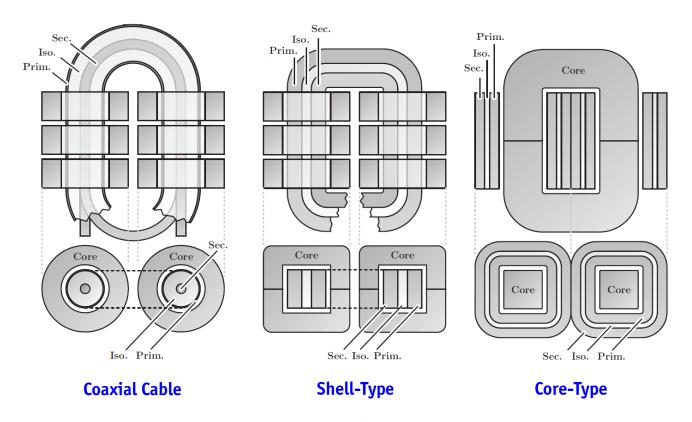
- Isolation vs. Cooling Trade-Off
- Oil = Coolant And Isolator (!)





▶ MF Transformer Design – Transformer Types

■ Main Transformer Types as Found in Literature



- Transformer Construction Types Very Limited by Available Core Shapes in this Dimension Range
- Shell-Type has Been Favored Given Its Construction Flexibility and Reduced Parasitic Components





► MF Transformer Examples (1)

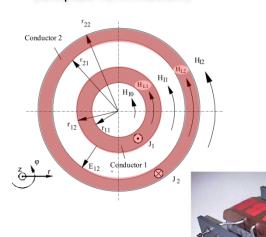
■ Coaxial Cable Winding

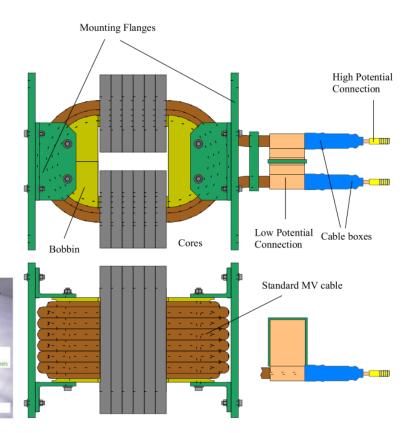
• Extremely Low Leakage Inductance

• Reliable Isolation due to Homog. E-Field

• Low Flexibility on Turns Ratio (1:1)

• Complex Terminations





• Heinemann (ABB, 2002) [Heinemann2002]

Cores (amorphous material)





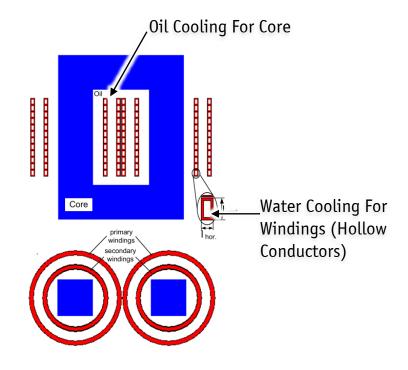
► MF Transformer Examples (2)

■ Coaxial Windings – Core Type

- Tunable Leakage Inductance
- More Complex Isolation
- Total Flexibility on Turns Ratio
- Simple Terminations



Hoffmann (2011) [Hoffmann2011]



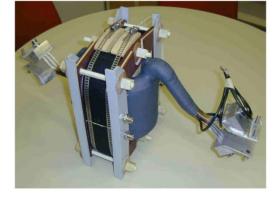




► MF Transformer Examples (3)

■ Coaxial Windings - Shell Type

- Tunable Leakage Inductance
- More Complex Isolation
- Total Flexibility on Turns Ratio
- Simple Terminations



- 8kHz, 350kW
- Water Cooling (Hollow Conductors)
- Isolation for 33kV

• Steiner (2007)
[Steiner2007]



- 8kHz, 450kW, 50kg
- Efficiency: 99.7%
- Dry-Type / Liquid Isol. (34.5kV)

• STS (2014) www.sts-trafo.com





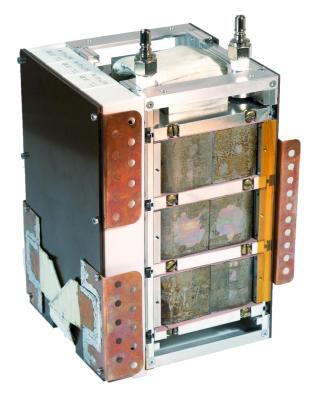
► ETH *MEGACube:* Water-Cooled Nanocrystalline Core Transformer

■ Power Rating 166 kW ■ Losses 0.88 kW

■ Efficiency 99.5 % (Meas.) ■ Power Density 32.7 kW/dm³

■ ETH / Ortiz, Leibl (2013)

166kW / 20kHz Water-Cooled Nanocrystalline Core Transformer ▶



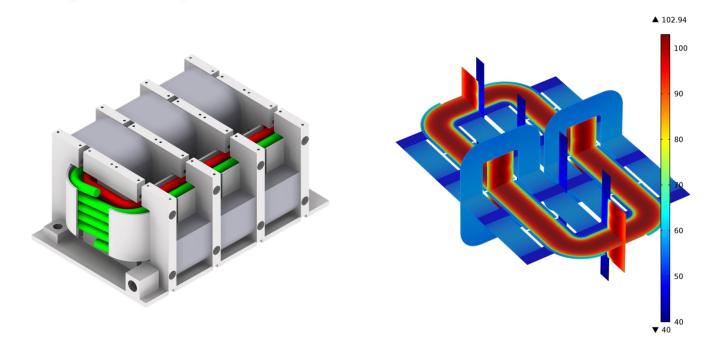






► ETH *MEGACube*: MF Transformer Design – Cold Plates / Water Cooling

■ Nanocrystalline 166kW/20kHz Transformer



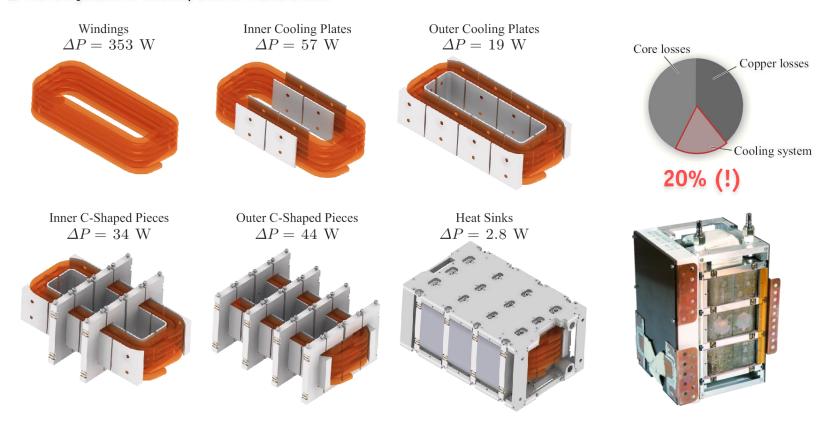
- Combination of **Heat Conducting Plates** and Top/Bottom **Water-Cooled Cold Plates**
- FEM Simulation Comprising Anisotropic Effects of Litz Wire and Tape-Wound Core





► ETH MEGACube: MF Transformer Design - Cold Plates / Water Cooling

■ Nanocrystalline 166kW/20kHz Transformer



■ Losses Generated in Internal Cooling System Amount to ca. 20% of Total Transformer Losses

ETH / [Ortiz2013b]



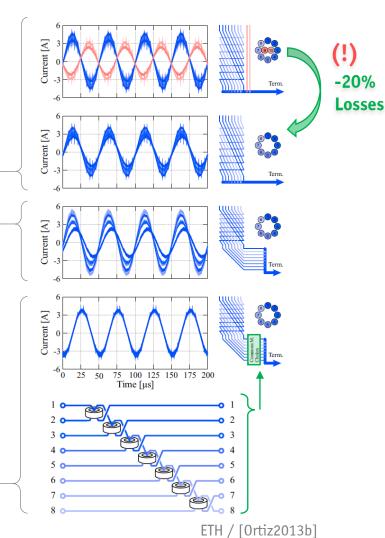


► Anecdote: Litz Wire Issues

- Case Study: Litz Wire with 10 Sub Bundles and 9500 x 71µm Strands in Total
- Unequal Current Sharing Between Sub Bundles
 - Flawed Interchanging Strategy
 - Influence of Terminations



■ Common-Mode Chokes for Forcing Equal Current Sharing







Challenge #6/11 Isolation Coordination

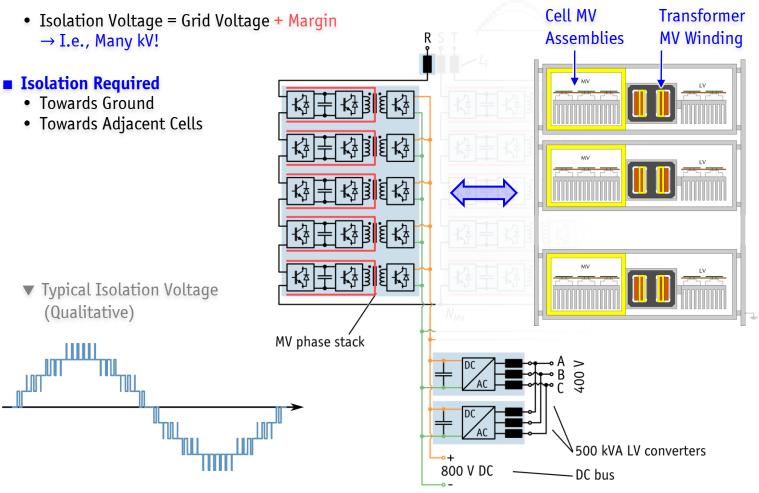
Isolation Barrier Positioning
Mixed-Frequency Stress





► Isolation Barriers In A Multi-Cell SST

■ Cascaded Cells Are On Floating Potentials

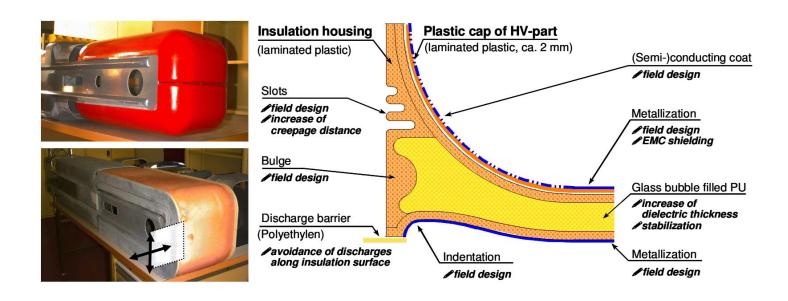






► Example: Isolation Coordination of Cascaded Cells' MV Part

- Components on MV Potential (e.g., Heat Sink)
- Isolation Towards Cabinet Required
- Field Grading to Avoid Partial Discharges, etc.









Challenge #6/11 Isolation Coordination

Isolation Barrier Positioning
Mixed-Frequency Stress

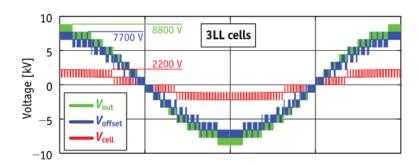


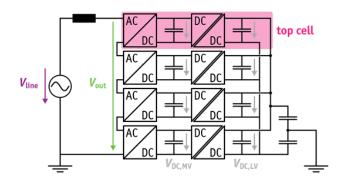


► Mixed-Frequency Electrical Field Stress

■ Combined Electrical Field Stress

- Large DC or Low-Frequency Component
- Smaller Medium-Frequency Component





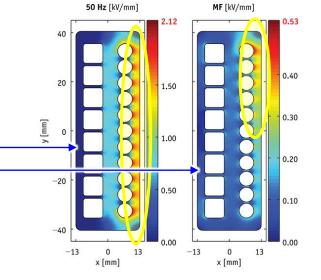
- Known From Machine Isolation Systems
- Physical Breakdown & Ageing Mechanisms Are Unclear

■ 50Hz Stress Common-Mode ______

■ MF Stress Differential-Mode (Mostly)

→ Degree of Freedom To Optimize Isolation System!







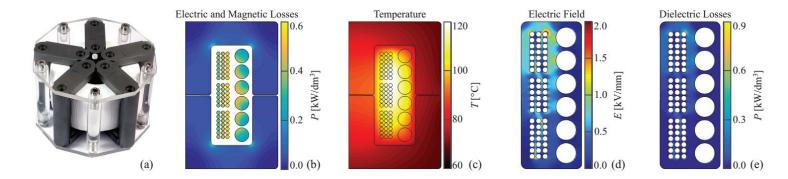
► Mixed-Frequency Electrical Field Stress: Dielectric Losses

■ Dielectric Losses Depend on the Frequency

$$P(\vec{x}) \propto f \cdot E(\vec{x})^2$$

Danger of Local Hotspots

- Example: HV-SiC DC/DC Converter:
- 25kW
- 8kV
- 50kHz ← (;)



- Dielectric Losses In Epoxy Isolation: 16% of Total Transformer Losses
 - → Reduced Efficiency
 - → Increased Hot-Spot Temperature
 - → Accelerated Aging (?)
- Careful Choice of Isolation Material is Essential (Field Strength/Thermal Cond./Dielectric Losses)

Further Reading: Upcoming ETH Pub. by T. Guillod.





Challenge #7/11 EMT

Common-Mode Ground Currents *EMI Limits*

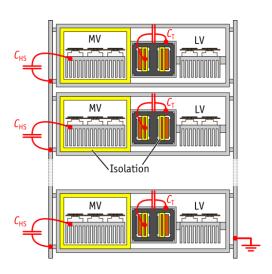




► CM Ground Currents: Basic Problem Description

■ Considering One Phase Stack Including the DC/DC Converters

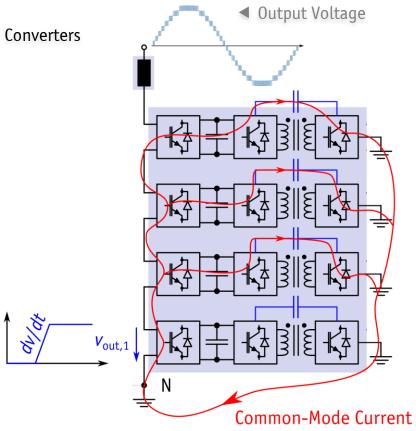
Parasitic Capacitances Between Cells and Ground



■ Switching Action in One Cell Moves All Cells At Higher Stack Positions In Potential

■ Charging Currents: $i = C \frac{dv}{dt}$

■ CM Oscillations With Parasitic Inductances!

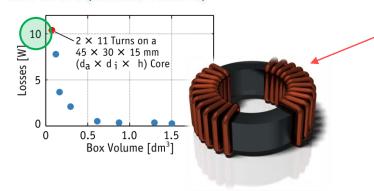


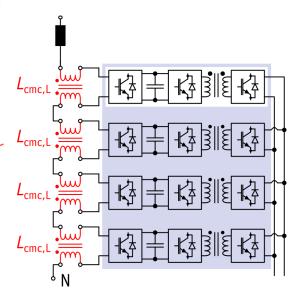




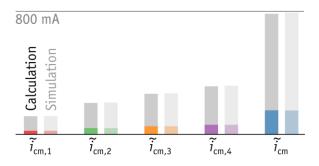
► CM Ground Currents: Countermeasure

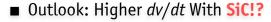
- Placing Common-Mode Chokes At Cells' AC Inputs
 - Low Effort (Losses, Volume)

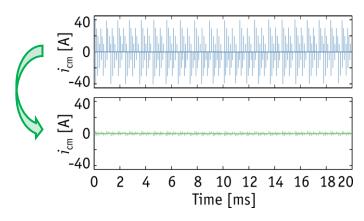




■ Simulations With/Without CM Chockes







Further Reading: ETH / [Huber2014a]





Challenge #7/11 EMI

Common-Mode Ground Currents **EMI Limits**





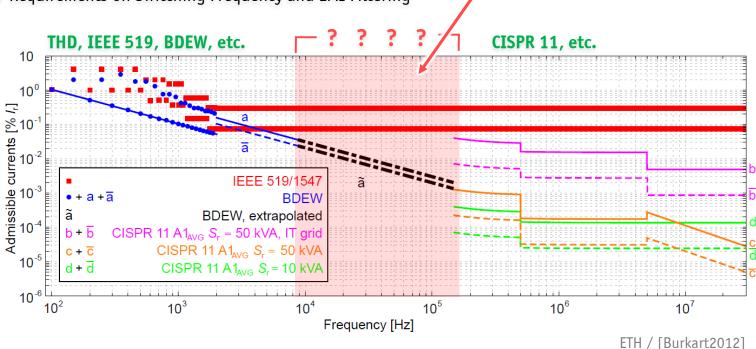
Grid Harmonics and EMI Standards

- Medium Voltage Grid Considered Standards
 - IEEE 519/1547
 - BDEW
 - CISPR (?)
- Requirements on Switching Frequency and EMI Filtering

■ Limits for CM Ground Currents?

Unclear Limits!

■ Limits for HF Noise?







Challenge #8/11 Protection

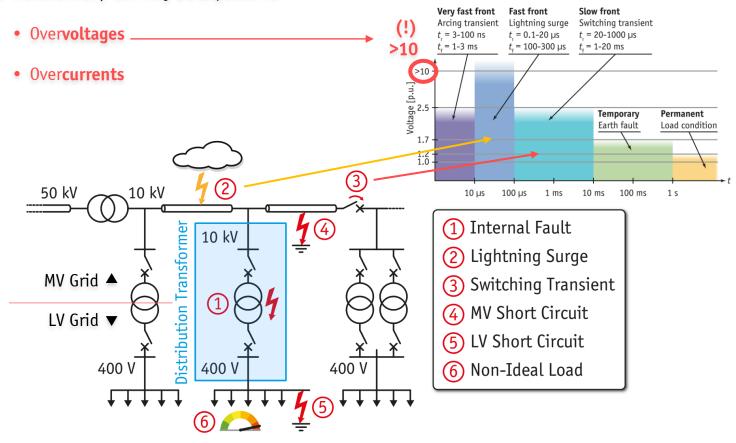
Protection of the SST





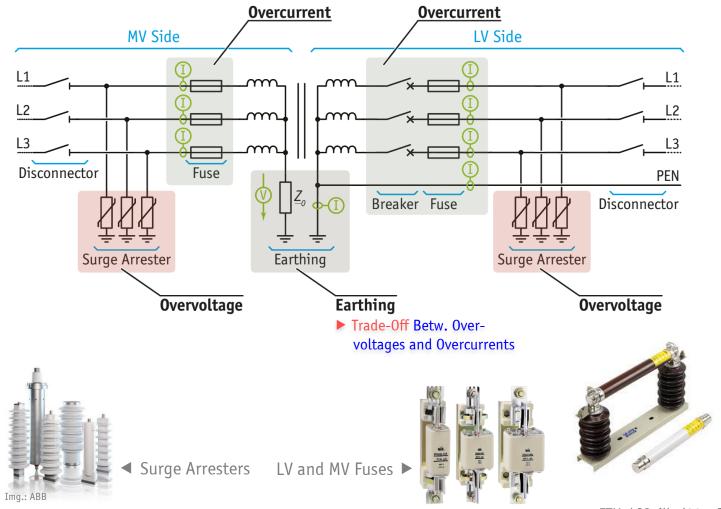
▶ Possible Fault Situations

■ Transformer / SST May Be Exposed To





► Typical LFT Protection Scheme



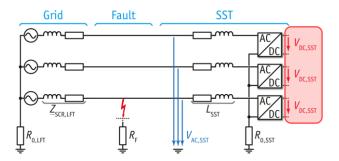






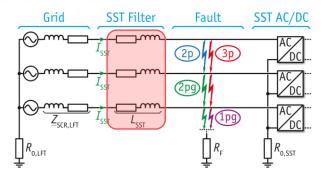
► MV Side SST Protection (1)

■ Grid Short Circuit



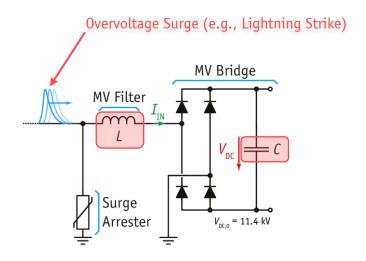
 Phase-To-Phase Voltage (!) Must Be Blocked → DC Capacitor Volt. Ratings!

■ SST Short circuit



 Current Limiting: (SCR > 8%) → Filter Inductor > 8%

■ Overvoltage Protection



- Arrester Clamping Voltage Is Still High
- Grounding Scheme: Lower Stress if Unearthed
- Current Limiting → Filter Inductor > 8%
- Energy Absorption in DC Link Capacitors
 - → DC Capacitance Requirement



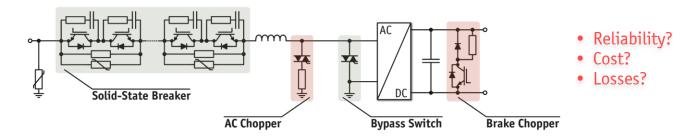


► MV Side SST Protection (2)

- Protection Considerations Affect SST Design & Limit Performance
- Example: Boost/Filter Inductor → Low Frequency Magnetic Component (!)
 - Min. 8% pu (SCR > 8%) • Critical for Low Power SSTs: $L_{\rm F}=8\%\cdot\frac{V_{\rm B}^2}{2\pi f\cdot P_{\rm N}}$ • Creation of "Safe" Environments to Protect Several SSTs at Once \rightarrow "Swarm Protection"
 - Limits Control Bandwidth (e.g., Act. Filtering, etc.)
 - Volume Reductions Due to Higher Switching Frequencies Might be Limited By Protection Considerations

Outlook: Advanced Protection Concepts

• E. g., Solid-State Protection



Further Reading: ETH / [Guillod2015]





Challenge #9/11 Control

It's Not Just Passives!

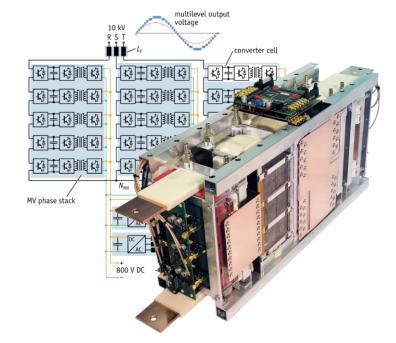




► A SST is Not Just Passives!



Source: http://www.africancrisis.org



■ **High Complexity** of SST Control System Compared to Passive Low Frequency Transformers





► SST Control System Partitioning

■ Very Different Timing Requirements

• IGBT Protection: us

• Grid Transients: ms to s

■ Feasible Approach: Several Hierarchical Layers

■ How To Test?



External Ctrl.

- Smart Grid Integration
- Power Flows (P, Q)
- ...

Internal Ctrl.

- Current/Voltage Control
- Redundancy Mgmt.
- ...

(Cell) Internal Ctrl.

- Modulation, Protection
- ...

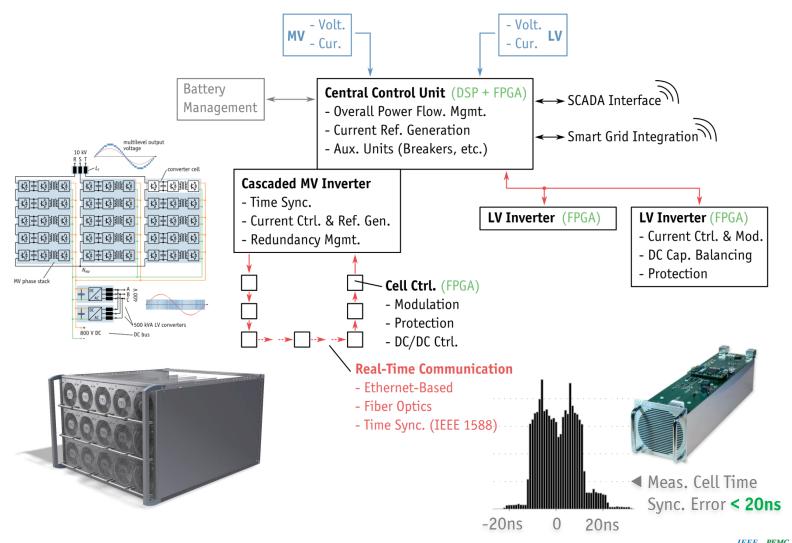
SST Power Hardware

■ The miniLINK Lab-Scale Full SST Demonstrator $15 \text{kVA}, 400 \text{V}_{AC} \leftrightarrow 800 \text{V}_{DC} \leftrightarrow 400 \text{V}_{AC}$





► Example of SST Control System Partitioning





Challenge #10/11 Construction of Modular Converter Systems

From Conceptualization to Realization





► From Conceptualization to Realization (1)

■ Actual Realization of a Modular MV Converter Systems → Complex Task

PCIM Europe 2015, 19 - 21 May 2015, Nuremberg, Germany

- Isolation Coordination
- Cooling
- Control & Communication

Phase Right

Hot-Swap

- Auxiliary Supply
- Mechanical Assembly
- etc., etc.

Integration Technologies for a Fully Modular and Hot-Swappable MV Multi-Level Concept Converter

Didier Cottet, Wim van der Merwe, Francesco Agostini, Gernot Riedel, Nikolaos Oikonomou, Andrea Rüetschi, Tobias Geyer, Thomas Gradinger, Rudi Velthuis, Bernhard Wunsch, David Baumann, Willi Gerig, Franz Wildner, Vinoth Sundaramoorthy, Enea Bianda, Franz Zurfluh, Richard Bloch, Daniele Angelosante, Dacfey Dzung ABB Switzerland Ltd., Corporate Research, 5405 Baden-Dättwil, Switzerland

Tormod Wien, Anne Elisabeth Vallestad, Dalimir Orfanus, Reidar Indergaard, Harald Vefling, Arne Heggelund, ABB Norway Ltd., Corporate Research, 1375 Billingstad, Norway

Jonathan Bradshaw, DPS Ltd., Auckland 1010, New Zealand

Contact: didier.cottet@ch.abb.com

> 25 Authors (!)

[Cottet2015a] [Cottet2015b]



Imgs.: W. van der Merwe





► From Conceptualization to Realization (2)

■ Actual Realization of a Modular MV Converter Systems → Complex Task

PCIM Europe 2015, 19 – 21 May 2015, Nuremberg, Germany

- Isolation Coordination
- Cooling
- Control & Communication
- Hot-Swap

- Auxiliary Supply
- Mechanical Assembly
- etc., etc.

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Tormod Wien, Anne Elisabeth Vallestad, Dalimir Orfanus, Reidar Indergaard, Harald Vefling, Arne Heggelund, ABB Norway Ltd., Corporate Research, 1375 Billingstad, Norway

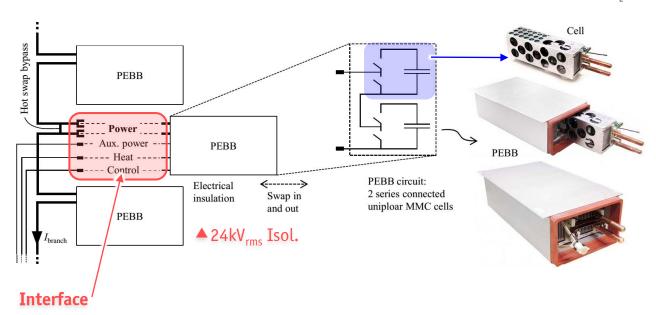
Jonathan Bradshaw, DPS Ltd., Auckland 1010, New Zealand

Contact: didier.cottet@ch.abb.com

> 25 Authors (!)

[Cottet2015a] [Cottet2015b]

■ Example: MV Modular Multilevel Converter Presented by ▲ (2015)



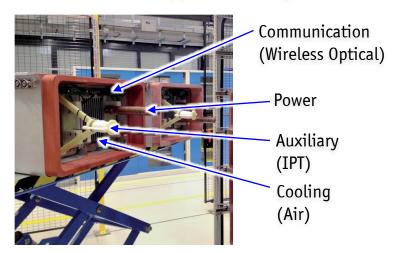


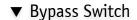


► Modularity: Hot-Swapping at 24kV

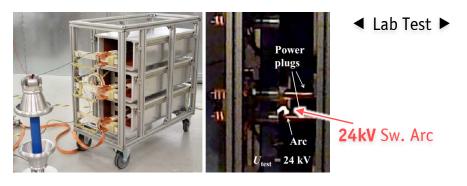
■ Example: MV Modular Multilevel Converter Presented by (2015) [Cottet2015a], [Cottet2015b]

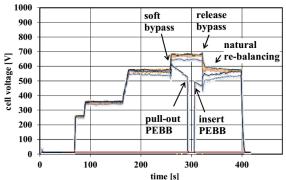
■ All Interfaces Must Support Modularity



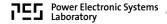








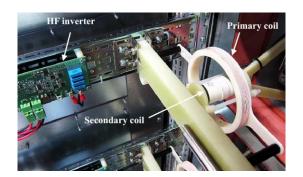




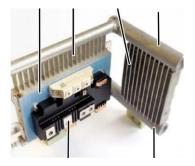
► Advanced Integration Technologies

■ Example: MV Modular Multilevel Converter Presented by (2015) [Cottet2015a], [Cottet2015b]

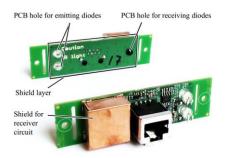
■ IPT for Auxiliary Power Supply



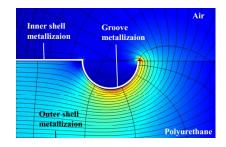
■ Two-Phase Cooling



■ Wireless Optical EtherCAT Comm.



■ Solid Isolation of PEBBs





→ Actually Building an SST is a Multi-Disciplinary, Highly Complex Task!





Challenge #11/11 Testing of MV Converters





► Infrastructure

- Significant Planning and Realization Effort
- Power Supply / Cooling / Control / Simulation (Integrated)





Img.:Center for Advanced Power Systems / Florida State University

■ Large Space Requirement / Considerable Investment (!)





► Infrastructure Examples

■ Medium-Voltage and High-Voltage Testing Facilities & Experience





Img.: High Voltage Lab, ETH Zurich]

Imgs.: [Cottet2015b]

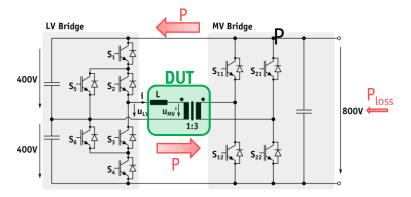
60kV Flashover

■ Source/Sink for 100s of kW



Img.: electrical-engineering-portal.com

■ Or Back-To-Back Testing Concepts → Complexity

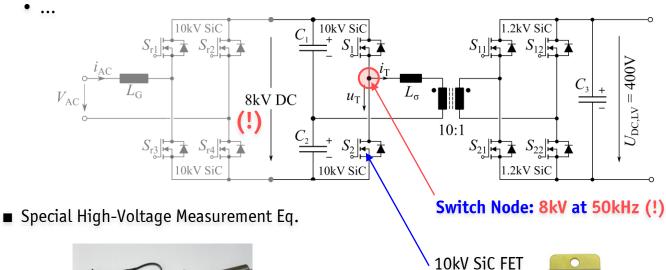






Measurement Equipment

- E.g., Switching Loss Measurements of HV SiC Devices
 - Voltage Range vs. Accuracy/Resolution
 - Skew
 - Disturbances





Img.: www.Tektronix.com



Img.: Cree Inc.

Circuit: ETH / [Rothmund2015]





11 Key Challenges Core Competencies

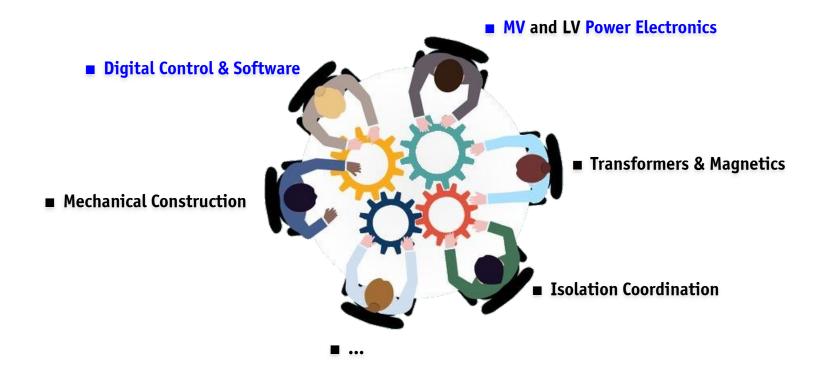
- 1. Handling of Medium Voltage
- 2. Topology Selection
- 3. Reliability
- 4. MF Isolated Power Converters
- 5. MF Transformer Design
- 6. Isolation Coordination
- 7. *EMI*
- 8. Protection
- 9. Control
- 10. Construction of Modular Conv.
- 11. Testing of MV Converters





▶ Core Competencies for SST Design

■ The 11+ Challenges Need to be Addressed by a TEAM



▶ Developing and Actually Building an SST is a Multi-Disciplinary, Complex Task!



SST Applicability In Grid Applications

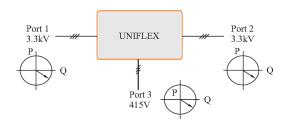
Grid SST Examples
Competing Approaches
Compatibility w. Existing Infrastructure

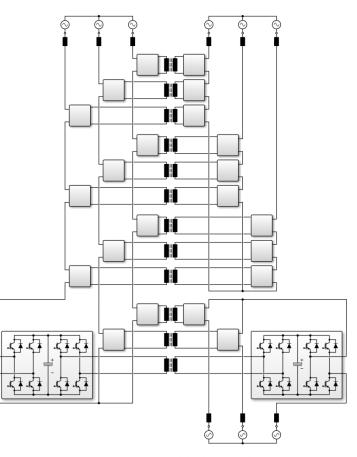




▶ UNIFLEX Project (1)

■ EU Project (2009)





- Advanced Power Conv. for <u>Universal</u> and <u>Flexible Power Management (UNIFLEX)</u> in Future Grids
- Cellular 300kVA Demonstrator of 3-Port Topology for 3.3kV Distr. System & 415V LV Grid Connection

[Watson2009]

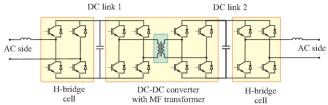




▶ UNIFLEX Project (2)

■ EU Project (2009)





■ AC/DC-DC//DC-DC/AC Module (MF Isolation, 1350V DC Link) and Prototype @ Univ. of Nottingham

[Watson2009]



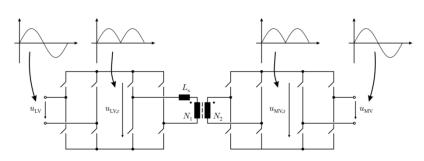


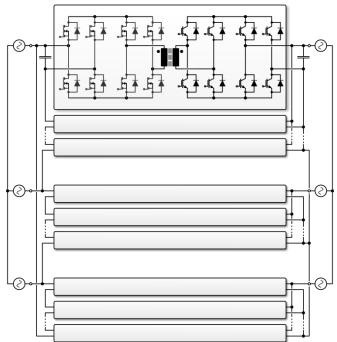
► SiC-Enabled 1MVA/20kHz Solid State Power Substation (1)

■ Das (2011)



- Fully Phase Modular System
- Indirect Matrix Converter Modules $(f_1 = f_2)$
- MV ∆-Connection (13.8kV_{l-l}, 4 Modules in Series)
- LV Y-Connection (465V/ $\sqrt{3}$, Modules in Parallel)





■ Comp. to 60Hz: 25% Weight / 50% Volume Reduction @ 97% Efficiency

IEEE PEMC

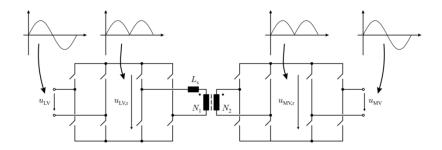


► SiC-Enabled 1MVA/20kHz Solid State Power Substation (2)

■ Das (2011)



- Fully Phase Modular System
- Indirect Matrix Converter Modules $(f_1 = f_2)$
- MV ∆-Connection (13.8kV_{l-l}, 4 Modules in Series)
- LV Y-Connection (465V/ $\sqrt{3}$, Modules in Parallel)





■ Comp. to 60Hz: 25% Weight / 50% Volume Reduction @ 97% Efficiency

IEEE PEMC

INDIRATES ACADEMIA

ACADEMIA

TECHNOLOGY BRIDGE



Applicability Grid Applications

Grid SST Examples

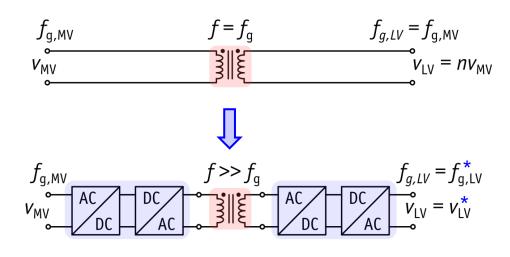
Competing Approaches: Isolation
Compatibility w. Existing Infrastructure

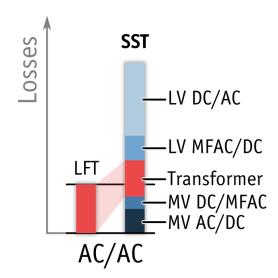




► Grid Application Task No. 1: Isolation & Voltage Scaling

- Typical Grid Application: MVAC // LVAC
- Low Frequency Transformer → SST
 - No Significant Efficiency Gain of Magnetic Transformer
 - Additional Conversion Stages Generate Additional Losses





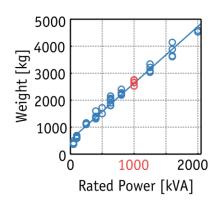
→ Remember "Efficiency Challenge"

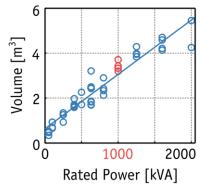




► Task: Isolation & Voltage Scaling

- The Competitor: **1000kVA LF Distribution Transformer**
 - Standard Off-the-Shelve Products
 - Typically Liquid Filled (Oil): Isolation, Cooling







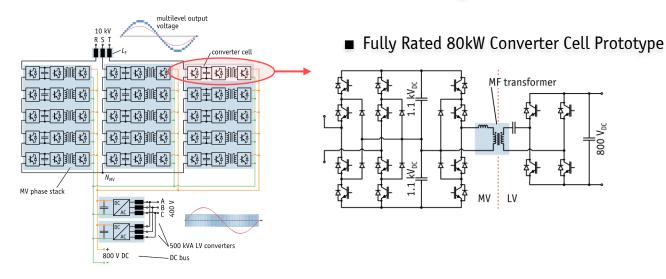
■ Averaged Data from Different Manufacturers

	LFT	
Efficiency	98.7	%
Volume	3.43	m^3
Weight	2590	kg
Material Cost	11.3	kUSD

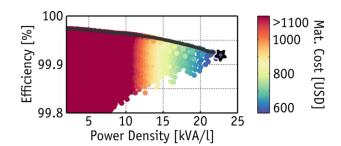




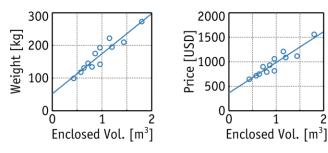
► SST vs. LFT Quantified - MV Side Modeling



■ Filter Inductor Pareto Optimization



■ Cabinet Modeling Based on Empirical Data



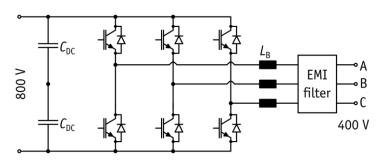
■ Material Costs: High-Volume Component Cost Models [Burkart2012]



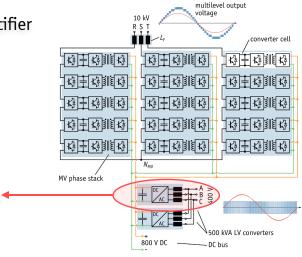


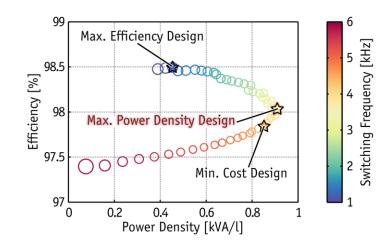
► SST vs. LFT Quantified - LV Side Modeling

■ Pareto Optimization of Standard 500kVA Inverter/Rectifier



- Calculated Results (Losses, Volumes)
- Good Agreement with Specs of Commercially Available Active Frontend Converter





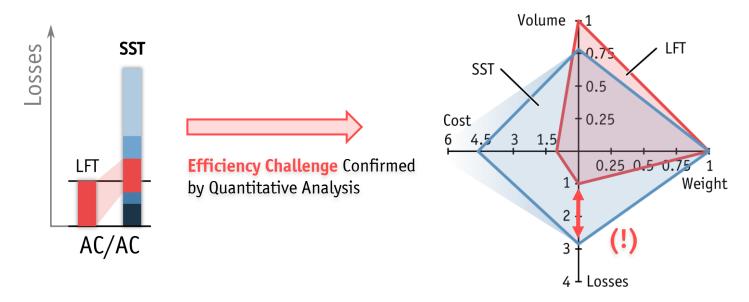




► SST vs. LFT Quantified – AC/AC Conversion

■ AC/AC SST = SST MV + 2 SST LV

	LFT	AC/AC SST
Efficiency	98.7	96.3 %
Volume	3.4	2.6 m ³
Weight	2590	2600 kg
Material Cost	11.3	> 52.7 kUSD

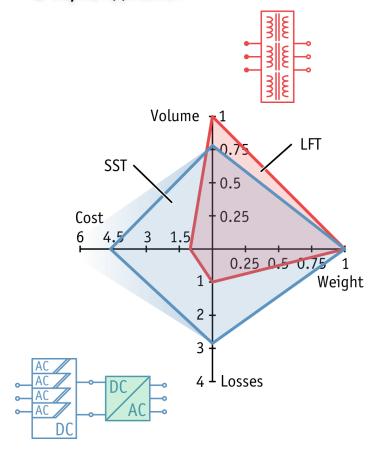




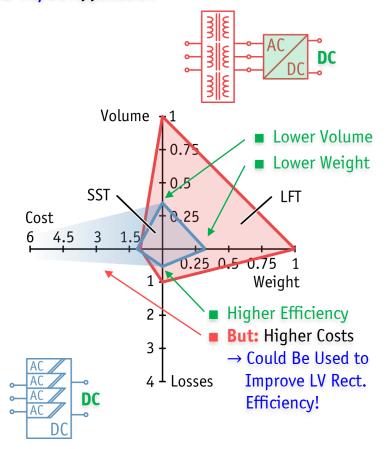


► SST vs. LFT Quantified – AC/AC and AC/DC Conversion

■ AC/AC Application



AC/DC Application



Further Reading: ETH / [Huber2014b]





Applicability Grid Applications

Grid SST Examples

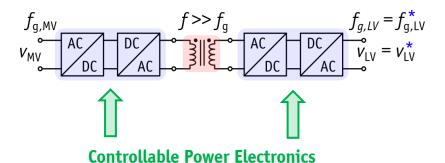
Competing Approaches: Control
Compatibility w. Existing Infrastructure





► Controllability As Unique SST Selling Point?

- SST Is Not Competitive If Only Isolation & Voltage Scaling Are Required!
- Added Value: Commonly Envisioned SST Features



- Reactive Power Compensation
- Voltage Regulation
- Active Filtering
- Power Flow Control
- Fault Current Limiting
- DC Interface (e.g., Energy Storage)
- ..

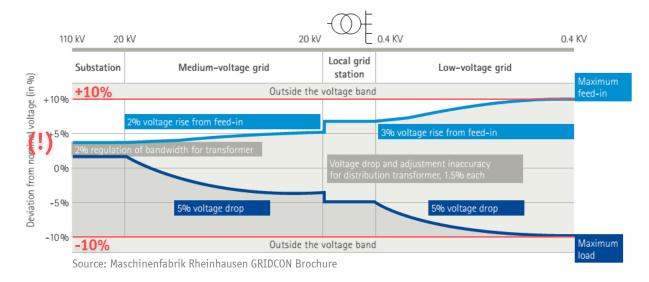
- Alternative Approaches To Provide These Features? → Several Examples In The Following!
- Is It Necessary To Process The *Full* Power Flow With The Controllable (Less Efficient) Stage?





► Voltage Band Violations in the Distribution System

- Voltage Band Specified by EN 50160: ±10%
- Limits Renewable Power Infeed on LV and MV Level
 - Max. 3% Voltage Increase on LV Level
 - Max. 2% Voltage Increase on LV Level



- Grid Expansion Becomes Necessary Even Though Equipment Capacities Are Not Exhausted
- SST Can Control Voltages But So Can Voltage Regulation Distribution Transformer (VRDT), etc.



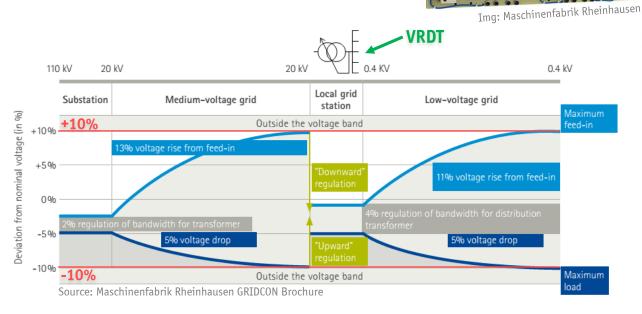


▶ Voltage Regulation Distribution Transformer

■ LFT Extended By A Controlled Automatic On-Load Tap Changer

- Up to 9 Positions, e.g., ±4 x 2.5%
- Up to 700'000 Switching Transitions
- LFT Efficiency & Robustness!







Imq: ABB

- Max. 11% Voltage Increase on LV Level
- Max. 13% Voltage Increase on MV Level

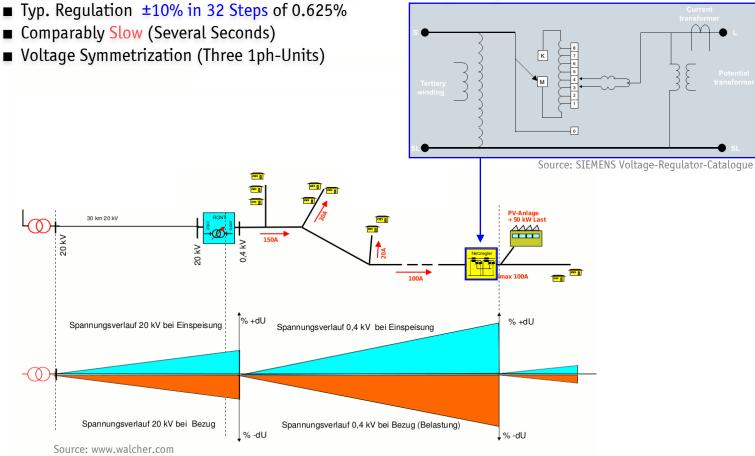




Distribution Voltage Regulators

- Available for MV or LV Systems
- Easy **Retrofit** (No Modification of Existing LFT)
- Typ. Regulation ±10% in 32 Steps of 0.625%

■ Mechanical Solution: Auto-Transformer With Tap Changer

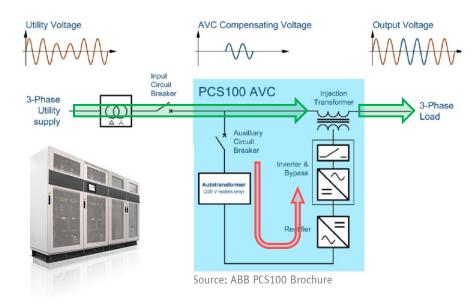






► Active Series Voltage Regulators

- Protection of Sensitive Industrial and Commercial Loads from Voltage Disturbances
- Power Electronic Solution: Converter With Injection Transformer
 - Continuous & Fast Voltage Regulation
 - Correction of Voltage Sags, Unbalances, Surges, and Phase Angle Errors
 - Harmonic Filtering
 - Reactive Power Compensation / Power Factor Correction
- Typical Features Envisioned For SSTs (!)
- But: Power Electronics Do Not Process The Full Power Flow



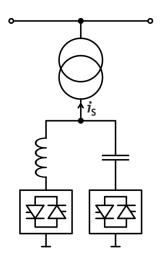


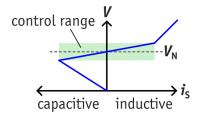


▶ Reactive Power Compensation

■ Static VAr Compensation

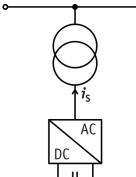
Switched Capacitor or Reactor Banks





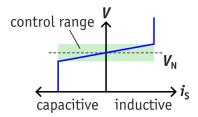
STATCOM

Power Electronic Converter



Additional Features

- Improved Power/Voltage Quality
- Voltage Regulation
- Compensation of Harmonics, Flicker, etc.

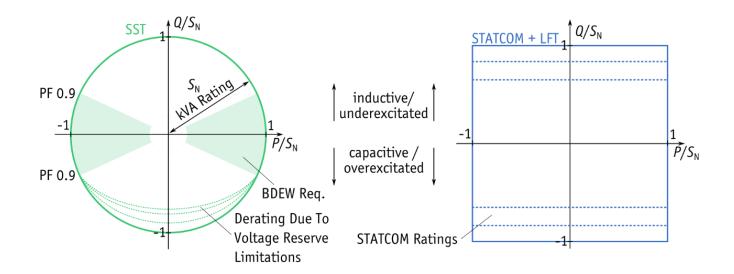






► SST vs. LFT + STATCOM

- SST's VAr Capability Depends on Active Power Flow!
- Or: SST Max. Reactive Power Capability Is Limited By Active Power Demand



- SST Provides Complete **Decoupling of Reactive Power Flow** of MV and LV Grid
 - No Propagation of Disturbances
 - Different STATCOM OPs in MV and LV Grid



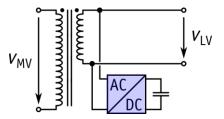


► Hybrid Transformers: Combinations of LFT and SST

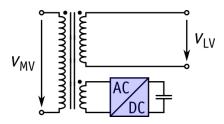
■ Shunt

Reactive Current Injection

- Power Factor Correction
- Harmonic Filtering
- Flicker Control



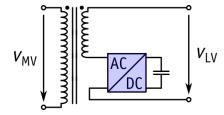
Isolated DC Port



■ Series

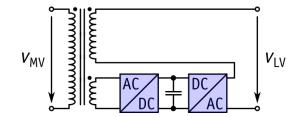
Reactive Voltage Injection

- · Phase Shifting
- Voltage injection



■ Combined

- Power Factor Correction
- Harmonic Filtering
- Flicker Control
- AC Regulation
- Phase Shifting



► Fractional Power Processing

→ Power Electronics Processes Only A Fraction Of The Power And/Or Voltage

[Bala2012], [Burkard2015]





Applicability Grid Applications

Grid SST Examples Competing Approaches

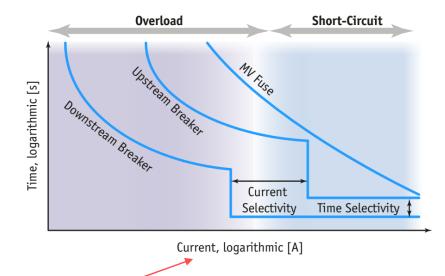
Compatibility w. Existing Infrastructure



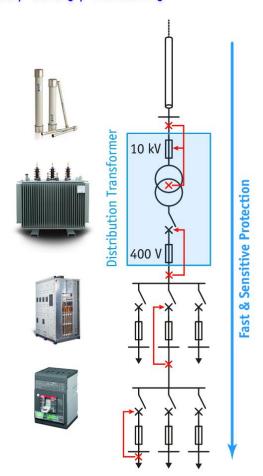


▶ Grid Protection Schemes

- Protection Scheme Needs to Consider: Selectivity / Sensitivity / Speed / Safety / Reliability
 - Selectivity: Only Closest Upstream Breaker/Fuse Should Trip to Isolate Faults Quickly
 - Different Trip Current Levels
 - Different Time Delays



■ Certain Overcurrents Required To Trip Fuses And/Or Breakers



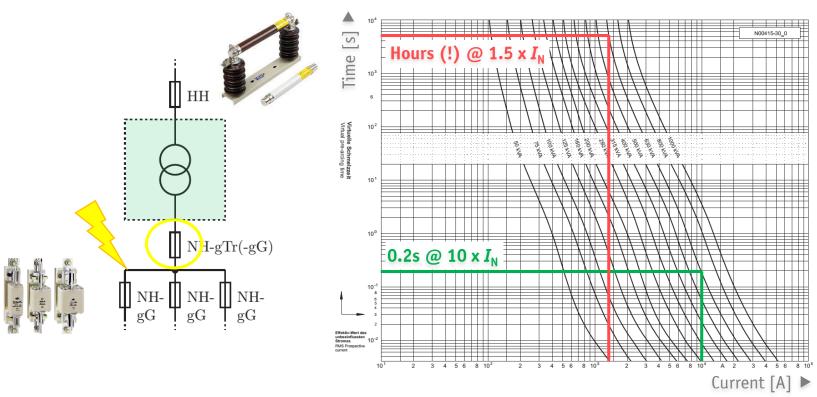
Imgs.: ETH / [Guillod2015]





► Tripping of LV Side Fuses

■ Example: 400V Fuse for 630kVA Transformer



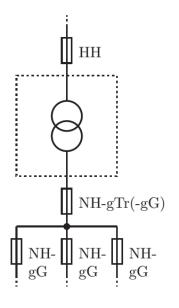
- Very High Short-Circuit Currents Required To Trip Fuses → No Problem for LFT!
- But Not Possible With Power Electronic Converter (Semiconductors!)

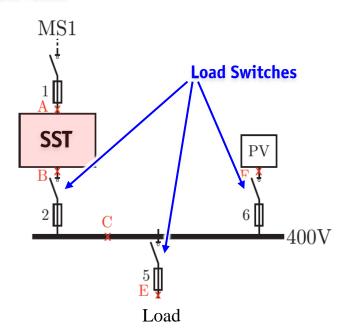




► Alternative Protection Schemes

- SST Can Limit Its Short-Circuit Current
- **Load Switches** (≠ Breakers!) Could Be Used To Isolate Faults





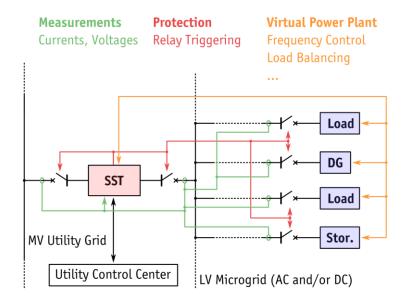
- Integration of SST in Existing LV Distribution System Remains Challenging
- Communication Between (Protection) Devices Becomes Essential
- SST Requires a "Smart Grid" → Coordination of Protection Relays





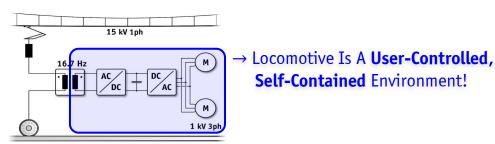
► SST Grid Integration

- SST Requires A **Controlled Environment** On Its LV Side
- SST Is Thus **Not a Direct Replacement** For A Distribution LFT!



- Novel Protection Schemes
- Micro Grid Can Act as a "Virtual Power Plant"
- DC Distribution
- Etc.

■ Comparison: **Traction Application**







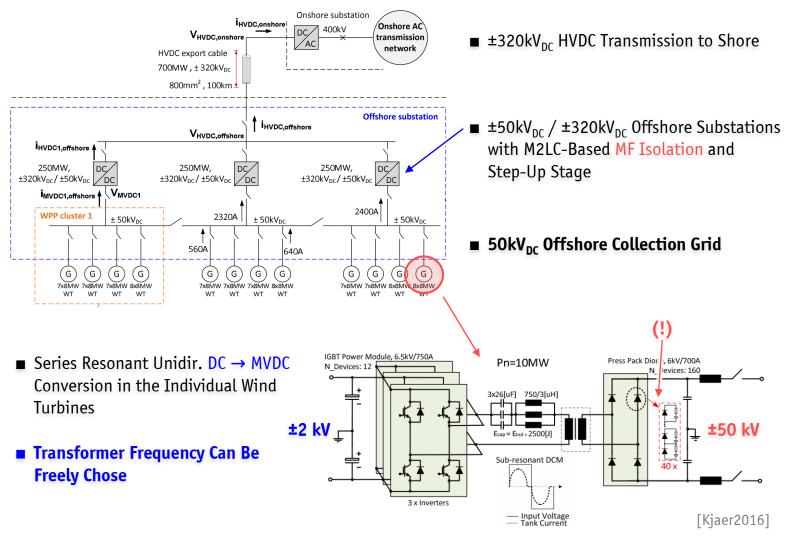
Applicability DC-DC Applications

No Alternatives!





► Example: DC Collection Grids for Offshore Wind Parks





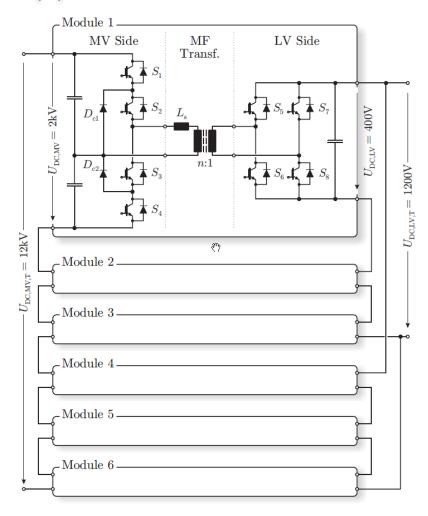


► Example: *MEGACube* @ ETH Zurich (1)

■ Total Power 1 MW ■ Frequency 20 kHz

■ Efficiency Goal 97 %

■ MV Level 12.0 kV ■ LV Level 1.2 kV



[Ortiz2010], [Ortiz2013c]





► Example: *MEGACube* @ ETH Zurich (2)

■ **Dual Active Bridge** DC-DC Converter Stage

■ Module Power

166 kW

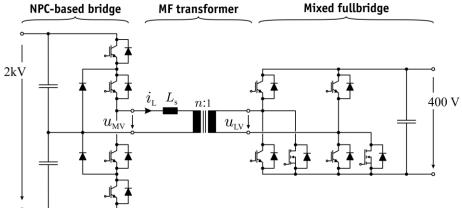
Frequency

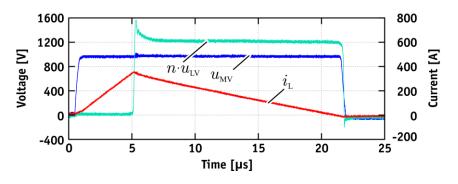
20 kHz

■ Triangular Current Mode Modulation



▲ 166kW / 20kHz TCM DC-DC Converter (Ortiz, 2013)



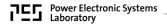


▲ Structure of the 166kW Module and MV Side Waveforms

[0rtiz2013c]



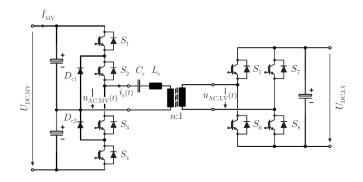


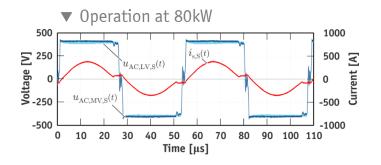


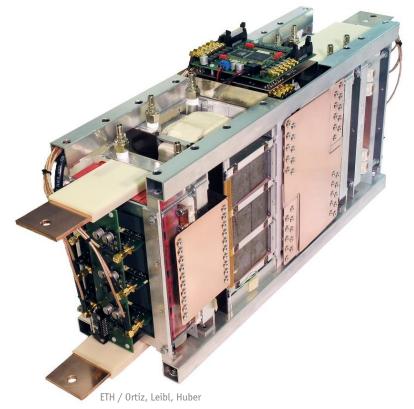
► Example: *MEGACube* @ ETH Zurich (3)

■ HC-DCM SRC DC-DC Converter Stage

■ Module Power
■ Frequency
■ Medium Voltage Side
■ Low Voltage Side
400 V











SST Applicability In Traction Applications

Traction SST Example



Img.: www.futuretimeline.net





► Cascaded H-Bridges and Resonant LLC DC-DC Stages (1)



- Dujic et al. (2011)
- Steiner (1996)
- Heinemann (2002)

P = 1.2MVA, 1.8MVA pk. 9 Cells (Modular)

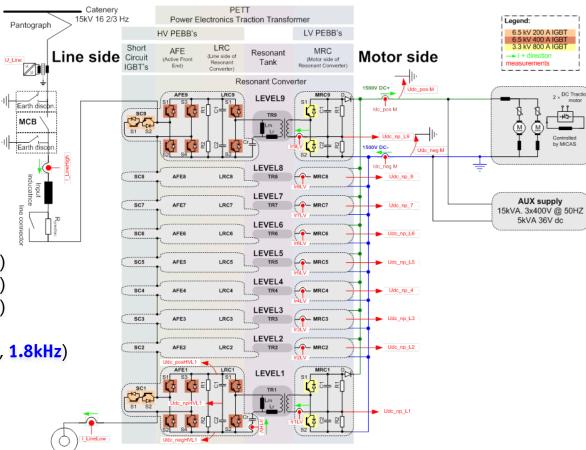
54 x (6.5kV, 400A IGBTs)

18 x (6.5kV, 200A IGBTs)

18 x (3.3kV, 800A IGBTs)

9 x MF Transf. (150kVA, 1.8kHz)

1 x Input Choke



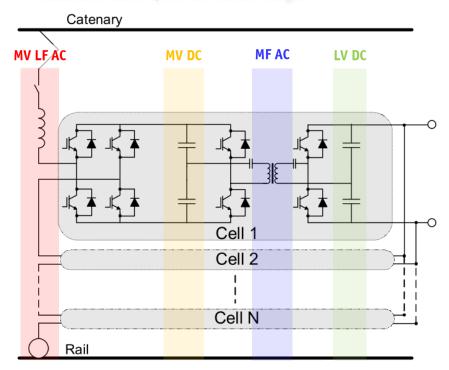






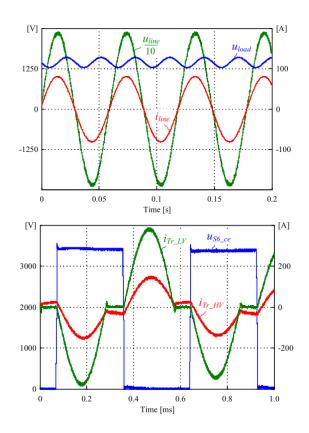
► Cascaded H-Bridges and Resonant LLC DC-DC Stages (2)

- 1.2MVA, 15kV, 16 ²/₃ Hz, 1ph. AC/DC Power Electronic Transformer (PETT)
 - Cascaded H-Bridge 9 Cells
 - Resonant LLC DC/DC Converter Stages



PET topology with cascaded H-bridges and resonant (LLC)DC-DC stages.

Img.: [Dujic2011]



[Dujic2013] & [Zhao2014]

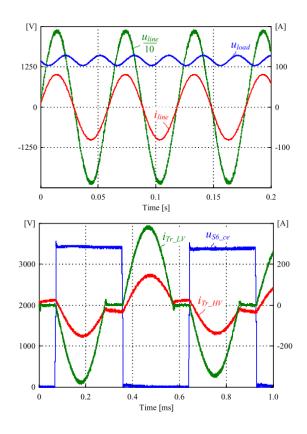


IEEE PEMC

► Cascaded H-Bridges and Resonant LLC DC-DC Stages (3)

- 1.2MVA, 15kV, 16 ²/₃ Hz, 1ph. AC/DC Power Electronic Transformer (PETT)
 - Cascaded H-Bridge 9 Cells
 - Resonant LLC DC/DC Converter Stages

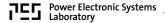




[Dujic2013] & [Zhao2014]





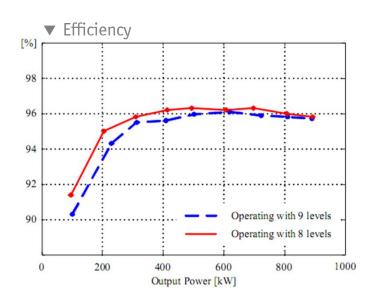


► Cascaded H-Bridges and Resonant LLC DC-DC Stages (4)

- 1.2MVA, 15kV, 16 ²/₃ Hz, 1ph. AC/DC Power Electronic Transformer (PETT)
 - Cascaded H-Bridge 9 Cells
 - Resonant LLC DC/DC Converter Stages







[Dujic2013] & [Zhao2014]





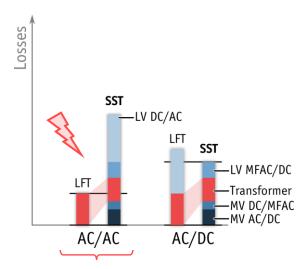
SST Applicability Summary





▶ "Efficiency Challenge" (Qualitative)

■ No Weight/Volume Constraints

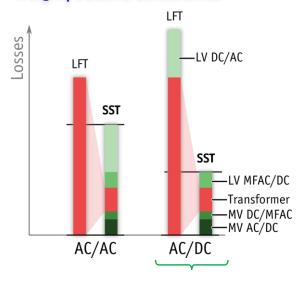


Typical **Grid** Application

■ SSTs in Grid Applications – A Skeptic's View

- **Efficiency** of LFT for AC/AC Very Hard To Attain
- Weight/Volume Typically Not an Issue In Stationary Grid Applications
- Robustness, Reliability?
- Cost?

■ Weight/Volume Constraints



Typical **Traction** Application

SSTs in Traction Applications

 SST Shows Efficiency Benefits for Applications with Volume/Weight Constraints!





► SST Applicability: The Road Ahead

■ Grid AC-AC



■ Efficiency Challenge

- Controllability Can Be Provided By Alternative Approaches
 - More Efficient (e.g., Tap Changers)
 - Partial Power Processing
- Compatibility Issues With Existing Infrastructure (e.g., Protection)
- Cost, Robustness, Reliability Issues

■ DC-DC Applications



- Isolation Stage Frequency Is A Free Parameter
- Future Applications, e.g. MV DC Collection Grids for Wind/PV

■ Grid AC-DC



- Efficiency Challenge More Balanced
- Self-Contained Applications (e.g., Datacenter DC Distr.)
- Cost, Robustness, Reliability

■ Weight/Space Limited Appl.



- Medium Frequency Systems Offer
 - Weight/Volume Reduction
 AND
 - Efficiency Improvement
- Typically Self-Contained Environments On One Side Of The SST
- Several Industrial Prototypes, But So Far No Products





ieee transactions on industry and general applications, vol. iga-7 no. 4, july/august 1971 \longleftarrow 1971

451

The Thyristor Electronic Transformer: a Power Converter Using a High-Frequency Link

WILLIAM McMURRAY, SENIOR MEMBER, IEEE

"Initial Use May be Found in Special Applications where Cost and Efficiency are Secondary to Size and Weight."

W. McMurray, 1971

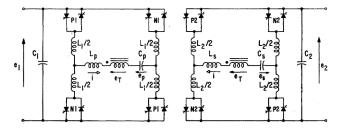


Fig. 5. Double-bridge electronic transformer; arrows define positive polarity of voltages and currents.

Conclusions

thyristors. Thus practical application of the electronic transformer is dependent upon further circuit development and component improvements. Initial use may be found in special applications where cost and efficiency are secondary to size and weight.





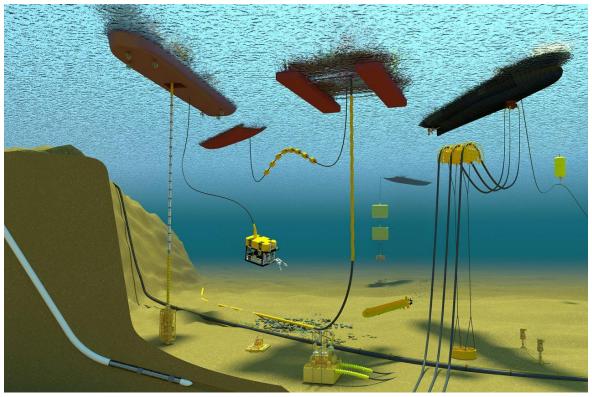
Future SST Applications







► Subsea Applications: Oil & Gas Processing (1)



Img.: matrixengineered.com

■ ABB's Future Subsea Power Grid → "Develop all Elements for a Subsea Factory"



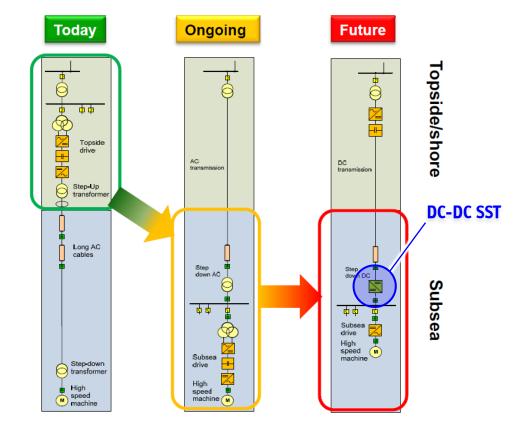


► Subsea Applications: Oil & Gas Processing (2)

■ Future Subsea Distribution Network (Devold, ABB, 2012)



- Transmission Over DC, No Platforms/Floaters
- Longer Distances Possible
- Subsea 0&G Processing
- **Weight Optimized Power Electronics**

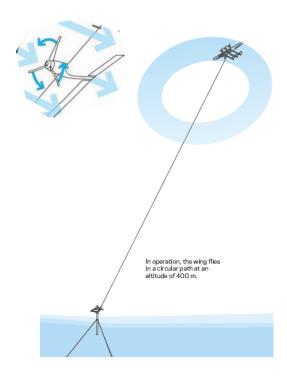






► Airborne Wind Turbines

- Power Kite Equipped with Turbine / Generator / Power Electronics
- Power Transmitted to Ground Electrically
- Minimum of Mechanically Supporting Parts













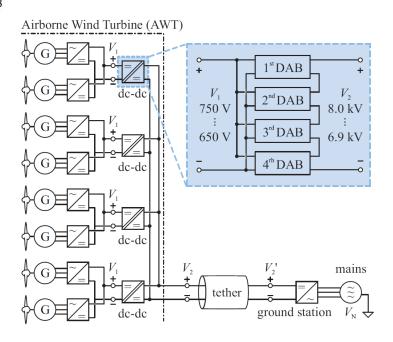
▶ 100kW Airborne Wind Turbine (1)

■ Ultra-Light Weight Multi-Cell All-SiC Solid-State Transformer – $8kV_{DC} \rightarrow 700V_{DC}$

Medium Voltage Port
 Switching Frequency
 Low Voltage Port
 Cell Rated Power
 Power Density
 1750 ... 2000 VDC
 650 ... 750 VDC
 6.25 kW
 5.2 kW/dm³

• Specific Weight 4.4 kW/kg





ETH / [Gammeter2015]





► 100kW Airborne Wind Turbine (2)

■ Ultra-Light Weight Multi-Cell All-SiC Solid-State Transformer – $8kV_{DC} \rightarrow 700V_{DC}$

• Medium Voltage Port 1750 ...

Switching Frequency

Low Voltage Port

Cell Rated Power

Power Density

Specific Weight

1750 ... 2000 VDC

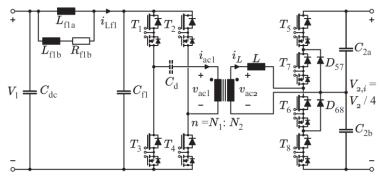
100 kHz

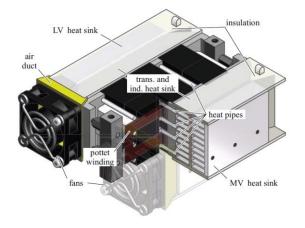
650 ... 750 VDC

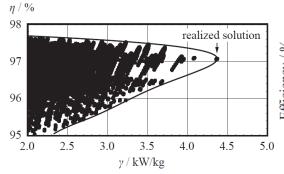
6.25 kW

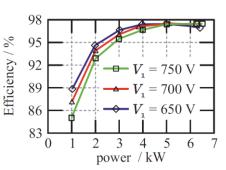
 5.2 kW/dm^3

4.4 kW/kg









ETH / [Gammeter2015]





► Future Hybrid or All-Electric Aircraft

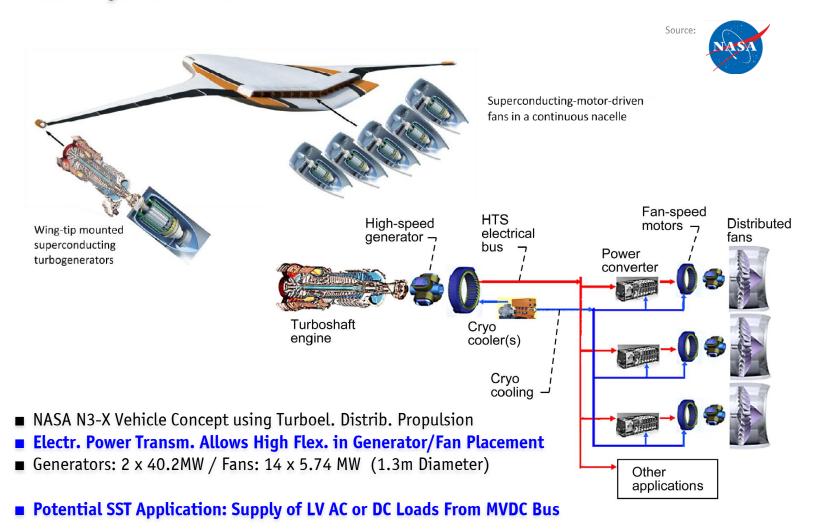


- Source:
- Powered by Thermal Efficiency Optimized Gas Turbine and/or Future Batteries (1000 Wh/kg)
- Highly Efficient Superconducting Motors Driving Distributed Fans (E-Thrust)
- Until 2050: Cut CO2 Emissions by 75%, NO_x by 90%, Noise Level by 65%





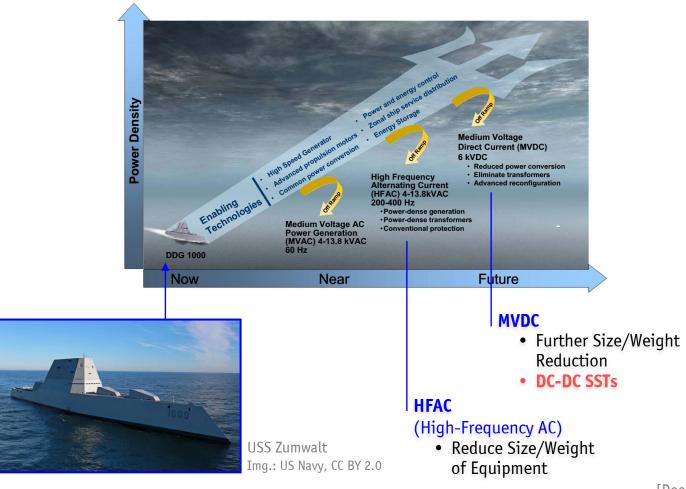
► Future Hybrid Aircraft







► Future Naval Applications (1)

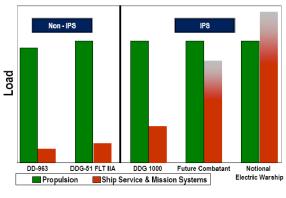


[Doerry2009]

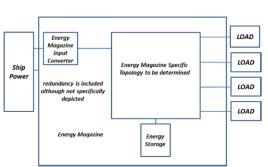


► Future Naval Applications (2)

■ Cellular MV DC Power Distribution on Future Combat Ships, etc.



[Doerry2009]





- "Energy Magazine" as Extension of Electric Power System / Individual Load Power Conditioning
- Bidirectional Power Flow for Advanced Weapon Load Demand
- **Extreme Energy and Power Density Requirements**





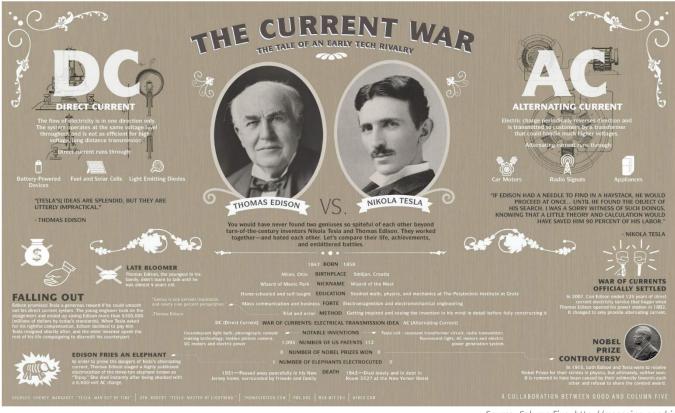
Conclusion & Outlook

SST Evaluation / Application Areas
Future Research Areas





➤ SST Ends the "War of Currents"



Source: Column Five, http://magazine.good.is

■ No "Revenge" of T.A. Edison, but Future "Synergy" of AC and DC Systems!





► Key Messages #1/3

Basic SST Limitations

- Efficiency (Rel. High Losses of 2-4%)
- **High Costs** (Cost-Performance Adv. still to be Clarified)
- Limited Weight/ Volume Reduction vs. Conv. Transf. (Factor 2-3)
- Limited Overload Capability
- Limited Overvoltage Tolerance
- (Reliability)

■ Potential Application Areas

- ► MV Grid/Load-Connected AC/DC and DC/DC Converter Systems
- ▶ Volume/Weight Limited Systems where 2-4% of Losses Could be Tolerated
 - Traction Vehicles
 - MV Distribution Grid Interface
 - * DC Micgrogrids (e.g., Datacenters)
 - * Renewable Energy (e.g., DC Collecting Grid for PV, Wind; Power-to-Gas)
 - * High Power Battery Charging (E-Mobility)
 - * More Electric Ships
 - * etc.
 - Parallel Connection of LF Transformer and SST (SST Current Limit SC Power does not Change)
 - Temporary Replacement of Conv. Distribution Transformer
 - Military Applications









► Key Messages #2/3

Advantageous Circuit Approaches

► Fully Modular Concepts

- Resonant Isolated Back End Topology (ABB)
- Resonant Isolated Front End Topology (Swiss SST)



"It is not the strongest of the species that survives, nor the most intelligent that survives. It is the one that is the most adaptable to change."

Charles Darwin

- Redundancy (!)
- Scalability (Voltage / Power)
- Natural Voltage / Current Balancing
- Economy of Scale

► Alternatives

- Single Transformer Solutions (MMLC-Based)
- HV-SiC Based Solutions (SiC NPC-MV-Interface)





► Key Messages #3/3

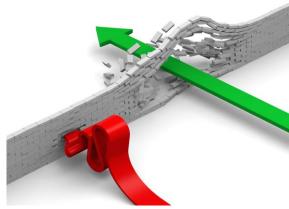
■ Main Research Challenges

- Multi-Level vs. Two-Level Topologies with HV SiC Switches
- Low-Inductance MV Power Semiconductor Package
- Mixed-Frequ./Voltage Stress on Insul. Materials
- Low-Loss High-Current MF Interconnections / Terminals
- Thermal Management (Air and H₂O Cooling, avoiding Oil)
- SST Protection
- SST Monitoring
- SST Redundancy (Power & (!) Control Circuit)
- SST vs. FACTS (Flexible AC Transmission Systems)
- System-Oriented Analysis → Clarify System-Level Benefits (Balancing the Low Eff. Drawback)

■ SST Design for Production → Multi-Disciplinary Challenge

► Required Competences

- MV (High) Power Electronics incl. Testing
- Digital Signal Processing (DSP & FPGA)
- MF High Power Magnetics
- Isolation Coordination / Materials
- Power Systems
- etc.
- ▶ 50/60Hz XFRM Design Knowledge is NOT (!) Sufficient

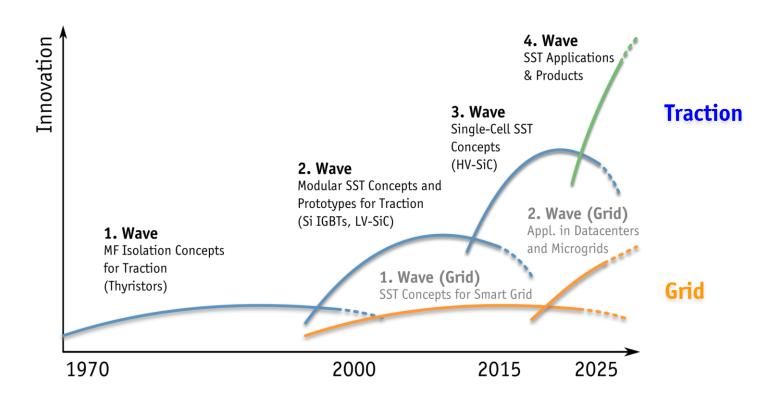








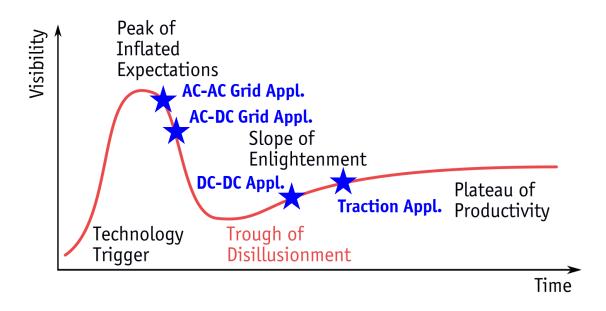
▶ Waves of SST Innovations







► SST Technology Hype Cycle



- Different State of Development of SSTs for
- → Traction Applications
- → Hybrid / Smart Grid Applications





► SST for Future Grid Applications



■ Huge Multi-Disciplinary Challenges / Opportunities (!)





Thank You!

Questions?



Source: Saddington Baynes / tmar.com

Acknowledgement

The authors would like to thank

- Dr. Gabriel Ortiz
- Thomas Guillod
- Daniel Rothmund

for their contributions.



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43,755 °M

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► ETH Zurich: Recent Key Publications (1)

- **J. E. Huber and J. W. Kolar**, "Solid-state transformers: on the origins and evolution of key concepts", *IEEE Ind. Electron. Mag.*, to be published, 2016.
- **J. E. Huber and J. W. Kolar**, "Optimum number of cascaded cells for high-power medium-voltage AC-DC converters," *IEEE Trans. Emerg. Sel. Topics Power Electron.*, to be published, 2016.
- **J. E. Huber, D. Rothmund, L. Wang, and J. W. Kolar**, "Full-ZVS modulation for all-SiC ISOP-type isolated front end (IFE) solid-state transformer," in *Proc. IEEE Energy Conversion Congr. and Expo. (ECCE)*, Milwaukee, WI, USA, Sep. 2016.
- **T. Guillod, R. Färber, F. Krismer, C. M. Frank, and J. W. Kolar**, "Computation and Analysis of Dielectric Losses in MV Power Electronic Converter Insulation," in *Proc. IEEE Energy Conversion Congr. and Expo. (ECCE)*, Milwaukee, WI, USA, Sep. 2016.
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- **J. E. Huber and J. W. Kolar**, "Common-mode currents in multi-cell solid-state transformers," in *Proc. Int. Power Electronics Conf. (IPEC) and ECCE Asia*, Hiroshima, Japan, May 2014. → Download
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